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HOOP/COLUMN ANTENNA  
RF VERIFICATION MODEL  
VOLUME I: TEST RESULTS

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HOOP/COLUMN ANTENNA  
RF VERIFICATION MODEL  
ANALYSIS AND TEST

BY  
HARRIS CORPORATION  
GOVERNMENT ELECTRONIC SYSTEMS DIVISION

PREPARED FOR: LANGLEY RESEARCH CENTER  
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# TABLE OF CONTENTS

## VOLUME I

<u>Paragraph</u>	<u>Title</u>	<u>Page</u>
	LIST OF FIGURES .....	2
	INTRODUCTION .....	3
	DESCRIPTION OF TEST ARTICLES AND ALIGNMENT .....	4
	DESCRIPTION OF THE TEST RANGE AND EQUIPMENT.....	5
	DESCRIPTION OF EXPERIMENT AND CALIBRATION.....	6
	SUMMARY OF ANALOG PATTERN MEASUREMENTS.....	8
	HARDWARE DESCRIPTION AND ANALOG PATTERNS LOGS.....	8
LSST I	PRIMARY PATTERN LOG.....	24
LSST II	PRELIMINARY FOCUS DATA, SECONDARY PATTERN LOG.....	31
LSST III	RASTER SCAN LOG.....	58
LSST IV	SECONDARY PATTERN LOG, 6 dB HORN.....	119
LSST V	SECONDARY PATTERN LOG, 6 dB HORN.....	150
LSST VI	SECONDARY PATTERN LOG, 6 dB HORN, QUARTZ WIRES.....	185
LSST VII	SECONDARY PATTERN LOG, 14 dB HORN.....	214
LSST VIII	SECONDARY PATTERN LOG, 14 dB HORN.....	245
LSST IX	SECONDARY PATTERN LOG, 14 dB HORN, QUARTZ WIRES.....	278
LSST X	SECONDARY PATTERN LOG, 14 dB HORN, QUARTZ WIRES .....	307

### NOTE:

ANALYSIS AND CORRELATION DATA FOR HOOP/COLUMN ANTENNA  
RF VERIFICATION MODEL FINAL REPORT COMPRISE VOLUME II.

## LIST OF FIGURES

- Figure 1. Top view of the RF verification model.
- Figure 2. Front view of the RF verification model.
- Figure 3. Side view of the RF verification model.
- Figure 4. Isometric view of the RF verification model.
- Figure 5. Photograph of the reflector and backup structure and assembly during fabrication.
- Figure 6. Photograph of the reflector structure being lifted on the antenna range.
- Figure 7. Photograph of the feed alignment structure being used on the antenna range.
- Figure 8. Photograph of RF verification model located on antenna range showing the alignment scope, transmitting antenna and tower.
- Figure 9. RF verification model showing quartz cords, front view.
- Figure 10. RF verification model showing quartz cords, side view.
- Figure 11. Antenna range equipment diagram.
- Figure 12. Range geometry and link calculations.
- Figure 13. Transmit antenna patterns, E plane - azimuth cut.
- Figure 14. Transmit antenna patterns, H plane - azimuth cut.
- Figure 15. Feed horns.



## HOOP/COLUMN ANTENNA RF VERIFICATION MODEL ANALYSIS AND TEST

### INTRODUCTION

The purpose of this report is to present the results of an experimental and theoretical study of the RF characteristics of the Hoop/Column quad aperture antenna. The primary purposes of the RF Verification Model in the LSST Program were twofold.

- 1) To provide experimental pattern data for the quad aperture configuration at different reflector edge illumination levels from which the geometry and edge effects can be assessed. Also, to provide experimental data which can be compared with calculations using various theoretical reflector scattering formulations.
- 2) To experimentally determine the effects of scale model quartz cables, to be used in the hoop column design, upon secondary patterns in order to assess the importance of developing a scattering theory to predict such effects.

In addition to the description of experimental procedures and the presentation of extensive experimental results, a comprehensive theoretical study of how to feed the quad aperture configuration is described. Firstly, an outline of the physical optics formulation used for subsequent calculations is given. Secondly, the experimental feed horns were modeled, using a Huygen's source approximation. From these feed horn patterns, calculations for various experimental aperture configurations were made, and compared with experimental patterns. Using these data and measured raster scan contour plots, a fundamental effect of parasitic side lobes is discussed, including location in space, and reasons for the approximate amplitude.

Based upon these results, a comprehensive theoretical study was conducted in order to design a feed for use in the quad aperture configuration resulting in good pattern characteristics. The first feed studied was the corrugated horn, where contiguous cross track coverage suitable for a radiometric mission was considered. Next, the effect of feed aperture distributions upon the secondary gain and pattern characteristics was determined for a wide variety of typical low side lobe aperture distributions. Then, related to communications missions, a brief study was made of multimode horn feeds suitable for clusters. Finally, a discussion of feed designs suitable for the quad aperture is given, along with a brief summary of conclusions from the study.

#### DESCRIPTION OF TEST ARTICLES AND ALIGNMENT

A top-view drawing of the basic pie-shaped reflectors, support fixtures, and feed support plates are given in Figure 1. Notice that the center of rotation is located behind the vertex of the parabolas in order to balance the overall structure on the azimuth-elevation antenna mount. Front and side views of the structure are given in Figures 2, 3, and 4 where scale model quartz cables are shown attached to the antenna. It can be noted from these figures that the feed support and fixtures are located well below the primary apertures; the feed horn itself provides the only blockage area. Detailed sketches showing specific dimensions and angles are given in Figures 16 through 19. (See Volume II)

The reflectors, as shown in Figure 5, were fabricated on a mold with an accuracy of 0.002 inch. The surface was made conductive with a flame spray aluminum process. The final reflectors were checked on the backup structure with a swept template and shown to be accurate to within 0.008 inch rms.

The reflector and feed support assembly were hoisted in sections as shown in Figure 6 and assembled on the pedestal. A special alignment tool was

manufactured to check feed alignment. Three known points located by holes were placed in each sector during manufacture. With these holes and an alignment fixture the distance to the feed on focus can be set to an accuracy of 0.03 inch. By placing fine cross hairs in the feed horn aperture, and the input waveguide to the feed horn, angular alignment was obtained. The exact offset angle of 21.6 degrees was marked on the reflector surface. The feed horn alignment was determined by observing the input waveguide, with the mixer removed.

The transmitting antenna, and an alignment scope, are shown in Figure 8. The transmitting antenna, which is located at the top of the tower, was aligned by the double cross hair method used on the feed horn. This alignment permitted bore sighting within a distance of  $\pm 1.0$  foot of the center axis of the two sectors as observed from the transmitting tower. The bore sight scope, as shown in Figure 8, permits the setting of the test antenna axis with errors of less than 0.004 degrees.

The quartz wires were mounted as required during the test program, using the fiberglass support fixture on the feed support structure, and special tabs attached around the edge of the dish, as shown in Figures 9 and 10. Also visible in Figure 10 are the standard gain horn, mounted on the feed support structure, and the white parabolic reflector used to obtain the phase reference for the two channel phase lock receiver.

#### DESCRIPTION OF THE TEST RANGE AND EQUIPMENT

The antenna test range equipment is illustrated in Figure 11. Most of the equipment is standard Scientific Atlanta and Hewlett Packard off-the-shelf instrumentation. Using analog-to-digital devices, the output of the synchros was digitized and recorded on floppy disks along with phase-amplitude data using a Vector computer. The data on the floppy disks were then transferred

off-line to the Harris H-80 and H-800 computers and stored. All of the subsequent raster scan data shown in this report were obtained in this manner. The basic pedestal gear and synchro accuracy was checked; hence the recorded data from the synchros can be repeated by rotating the pedestal in the same direction for each line of the raster scan run. The absolute accuracy of any angular number recorded was better than 0.05 degrees. It was noted that the stability of the amplitude recording system was better than 0.1 dB from day to day, as was the drift during any one 8 hour measurement day.

The geometrical arrangement of the antenna range, along with a conservative link budget, is given in Figure 12. It was noted during the course of measurement that receiver noise began to be noticeable about 70 dB down in dynamic range, although repeatable lobes were measured at lower values. The multipath signal levels for the test antenna were determined using the geometry of Figure 12, and the measured transmitting antenna pattern given in Figures 13 and 14. The cross-polarization levels from the transmitter were generally below -40 dB in the multipath reflection Fresnel zone. The direct polarization pattern level in the same region will be -26 dB to -30 dB down. The above mentioned measurements, along with the multipath zone being 13 to 16 degrees away from any measurement elevation angle, indicate that the multipath had minimal effect upon the detailed measurements reported.

#### DESCRIPTION OF EXPERIMENT AND CALIBRATION

The receiving feed antennas were specified to have -6 dB and -14 dB edge tapers at the bisector of a pie reflector. The feed horns designed for use in this experiment are depicted in Figure 15. A detailed set of primary patterns were measured and recorded in both analog and digital form, as listed in the pattern log, LSST-I, page 24. The analog patterns are shown on the pages as

listed in LSST-I. The feed horns were set at an angle of 21.6 degrees corresponding to bisector of the angle between the focal point and the outer edge of the pie sector. For convenience, the following are the summary parameters used in this experiment:

FOCAL LENGTH	137.7 inches
OFFSET ANGLE	21.6 degrees
RADIUS OF PIE SECTOR	110.8 inches
DIAMETER FROM FOCUS TO PIE EDGE	105.3 inches
OPERATING FREQUENCY	15.0 GHz
PHASE CENTER DISTANCE BEHIND HORN APERTURE	
-6 dB	0.30 inches
-14 dB	0.99 inches

The antenna range was chosen to minimize multipath signals. The distance between the towers was approximately  $D^2/\lambda$  or about one-half the conventional range distance. In order to correct for quadratic phase error, due to a fore-shortened range, the feed was displaced along the offset angle. Several calculations were run for symmetrical offset reflectors and compared with measurements where the axial feed displacement was varied. From these data, and gain measurements, it was determined that an axial defocus (movement along the offset angle of 21.6 degrees) of about 1.2 inches gave optimum gain. All of the data taken are given in the log, LSST-II, page 31, with the subsequent pages of patterns listed for indexing.

It should be noted that great care was taken to ensure calibration between pattern sets that were taken over a period of nearly five weeks. As a routine procedure, the pedestal was always rotated in the same direction during pattern taking. This tended to maintain gear wear errors in the same direction. Also, the systems were left on continuously to minimize warmup

errors, and there was a gain measurement taken by the substitution method before and after each measurement sequence. The only significant measurement error noted was the resetting of synchros to precise increments. This error, on an absolute basis, was less than 0.05 degree and was observable for only a few significant pattern locations. It was noticeable as an amplitude change on secondary peaks at wide angles. There was little chance of improving on the accuracy without a complete redesign and rebuild of the pedestal and synchro system.

Data were also taken for both no scan and scanned cases. For the scan cases the horn was mounted in a plane perpendicular to the offset angle of 21.6 degrees. The horns were scanned in the horizontal plane and toward the direction of the other pie sector. Data are presented in a three-dimensional azimuth-elevation-amplitude plot, followed by an azimuth-amplitude plot, and an elevation-amplitude plot for detailed review. The data presented allow for a detailed comparison of the aperture coupling problem between two pie-shaped sectors.

#### SUMMARY OF ANALOG PATTERN MEASUREMENTS

The purpose of presenting these results is to give an expanded pattern description of the aperture coupling and quartz wire effects over wide angular sectors. It should be noted that the quartz wires produced few noticable pattern changes, and hence no detailed raster scans were obtained. The secondary pattern log is given in LSST-IV through LSST-IX, pages 119-306. In order to compare one pattern set with another in absolute amplitude, the measured gain for that pattern set is available in the recorded floppy disk data.

#### HARDWARE DESCRIPTION AND ANALOG PATTERNS LOGS

The remainder of Volume I consists of photographs, hardware descriptions, and antenna patterns.

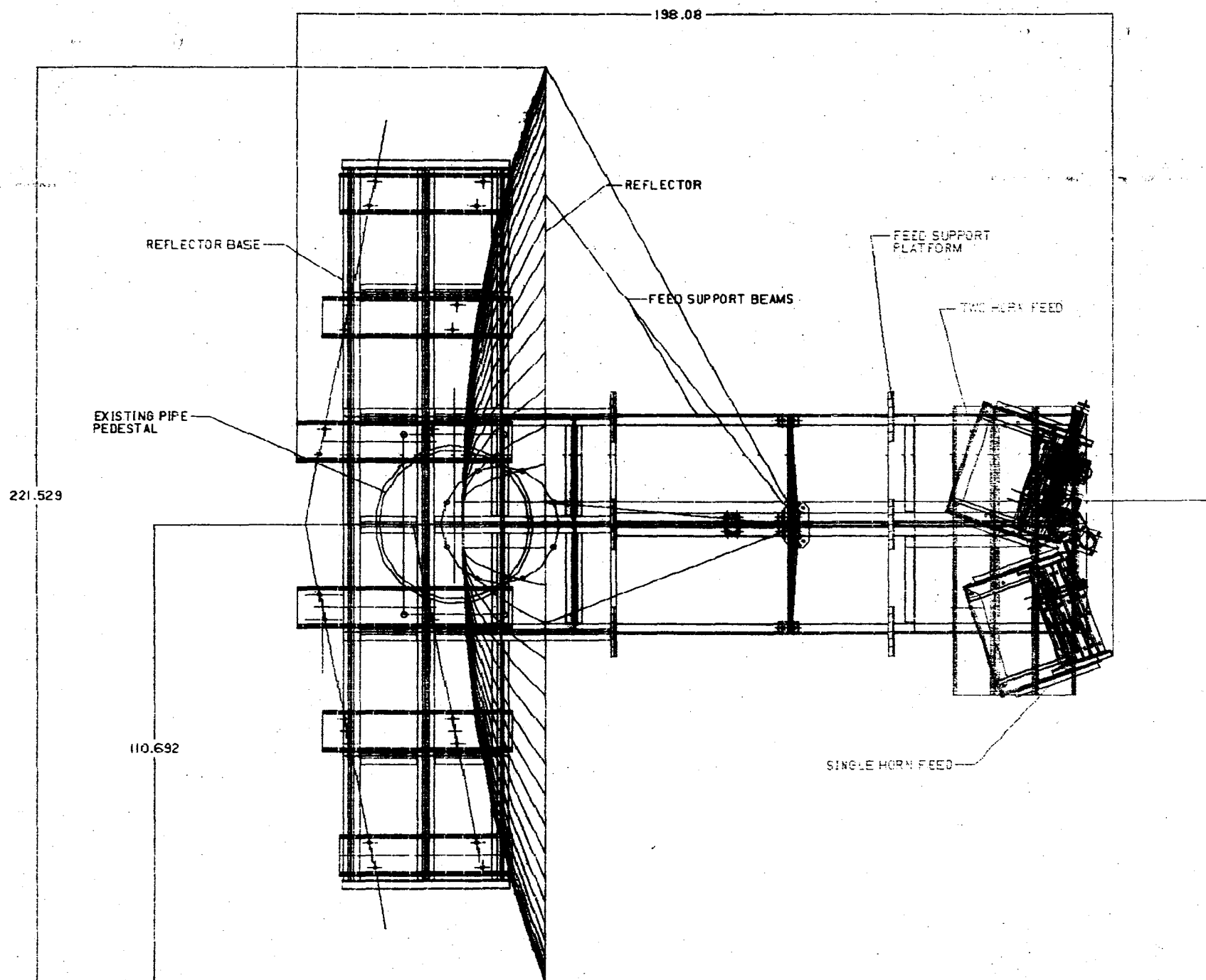


Figure 1. TOP VIEW OF THE RF VERIFICATION MODEL

Figure 2. FRONT VIEW OF THE RF VERIFICATION MODEL

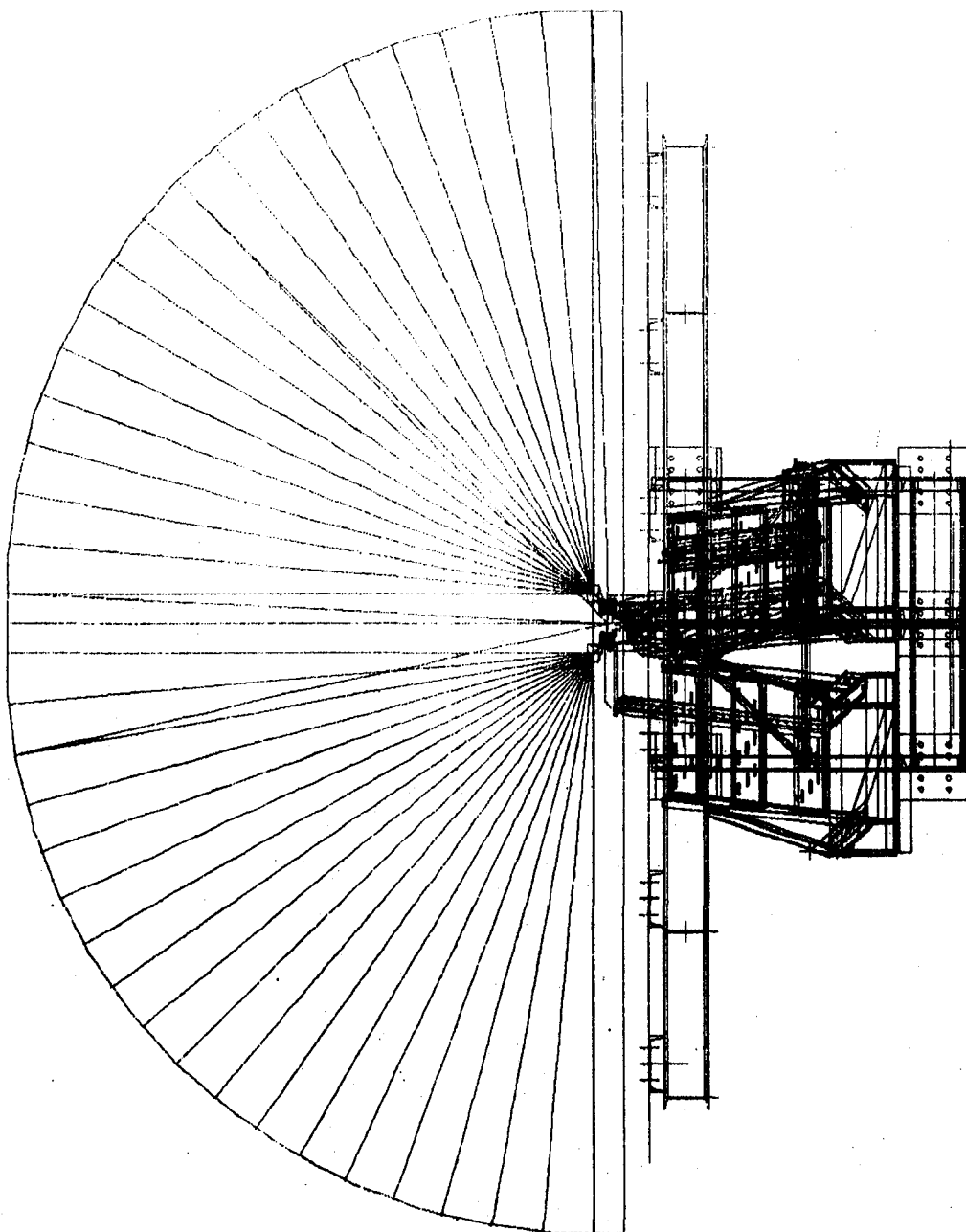




Figure 3. SIDE VIEW OF THE RF VERIFICATION MODEL

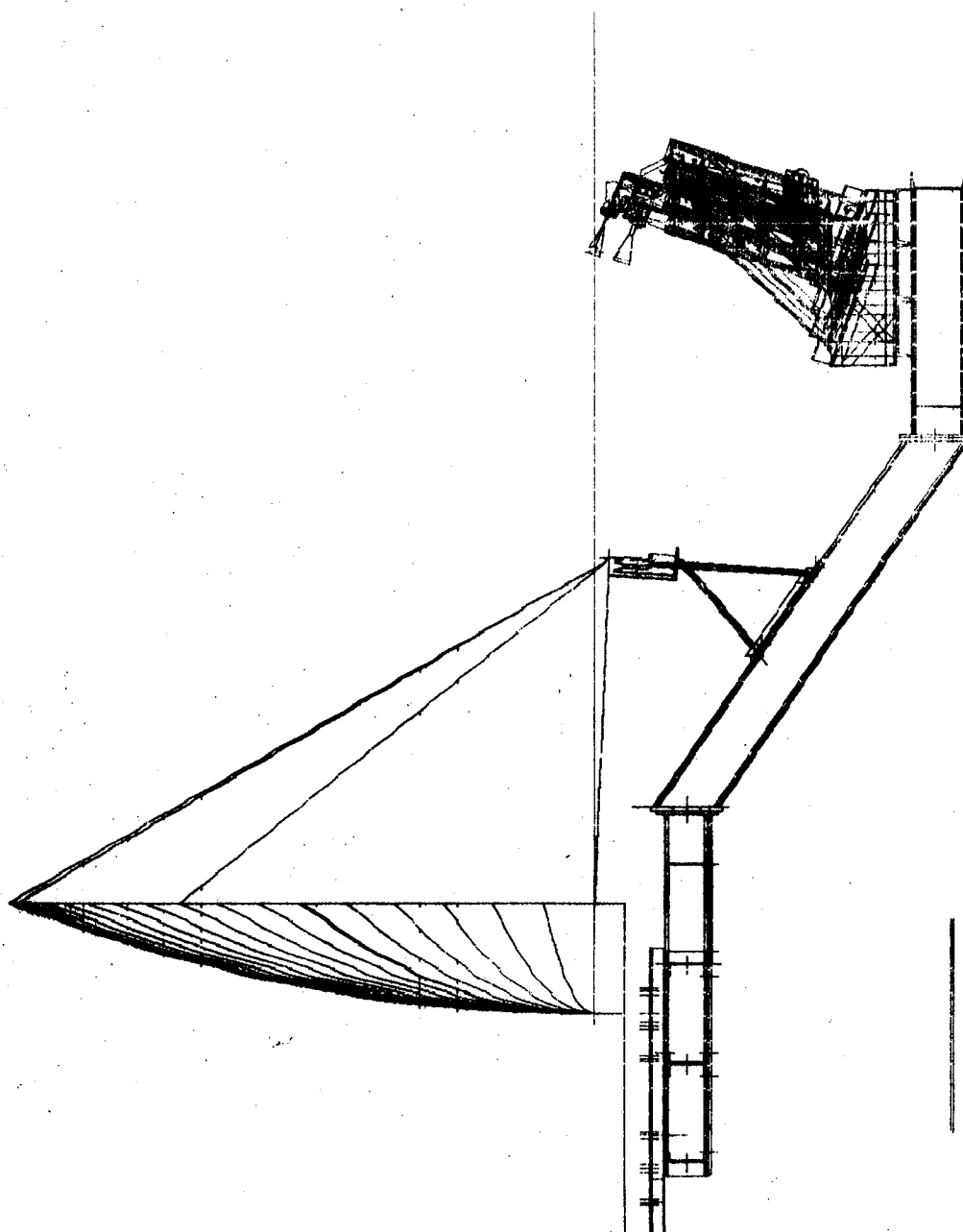
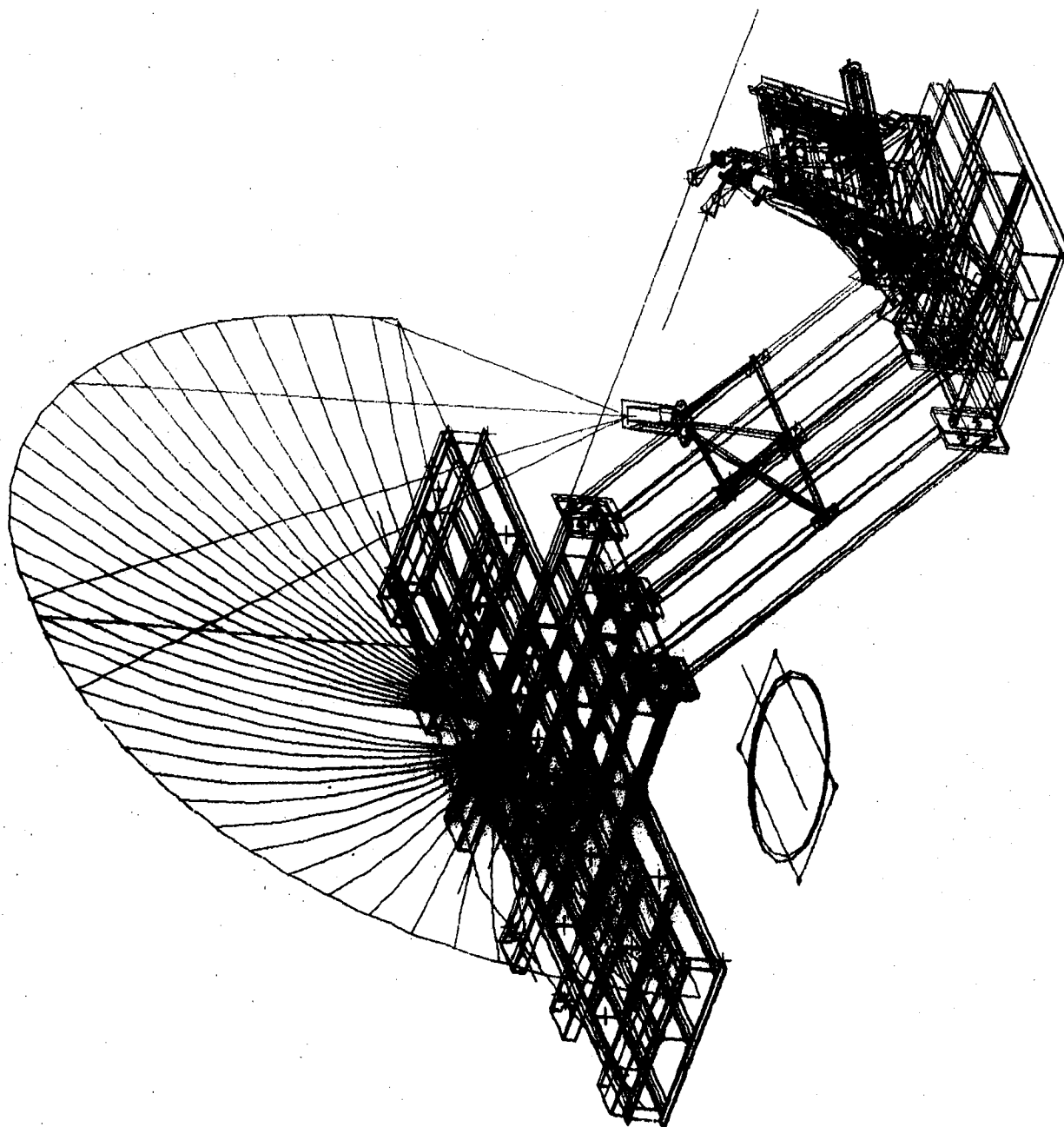
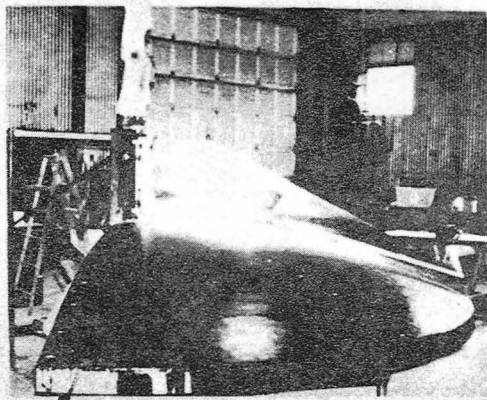


Figure 4. ISOMETRIC VIEW OF THE RF VERIFICATION MODEL

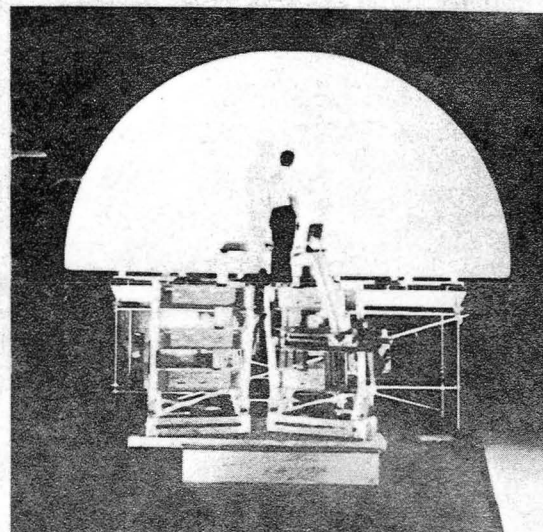
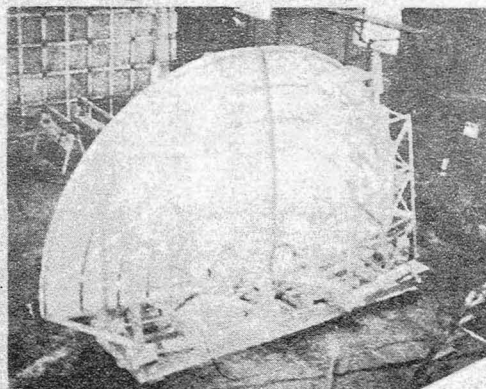


# FABRICATION OF PRECISION RF VERIFICATION MODEL

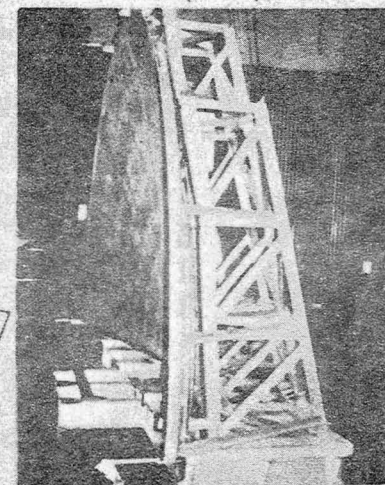


A MOLD WITH 0.05 mm  
(0.002 IN.) RMS ACCURACY  
IS USED TO BUILD  
FIBERGLASS  
FACE SKINS

FACE SKINS ARE  
ASSEMBLED TO  
RIGID BACKUP  
STRUCTURE



ASSEMBLED  
ANTENNA TEST  
MODEL



ADJUSTMENT SCREWS  
BETWEEN FACE SKINS AND  
BACKUP STRUCTURE PROVIDE  
A REFLECTOR ACCURACY OF  
0.05 mm (0.008 IN.) RMS

Figure 5. PHOTOGRAPH OF THE REFLECTOR AND BACKUP STRUCTURE AND ASSEMBLY DURING FABRICATION



Figure 6. PHOTOGRAPH OF THE REFLECTOR STRUCTURE  
BEING LIFTED ON THE ANTENNA RANGE

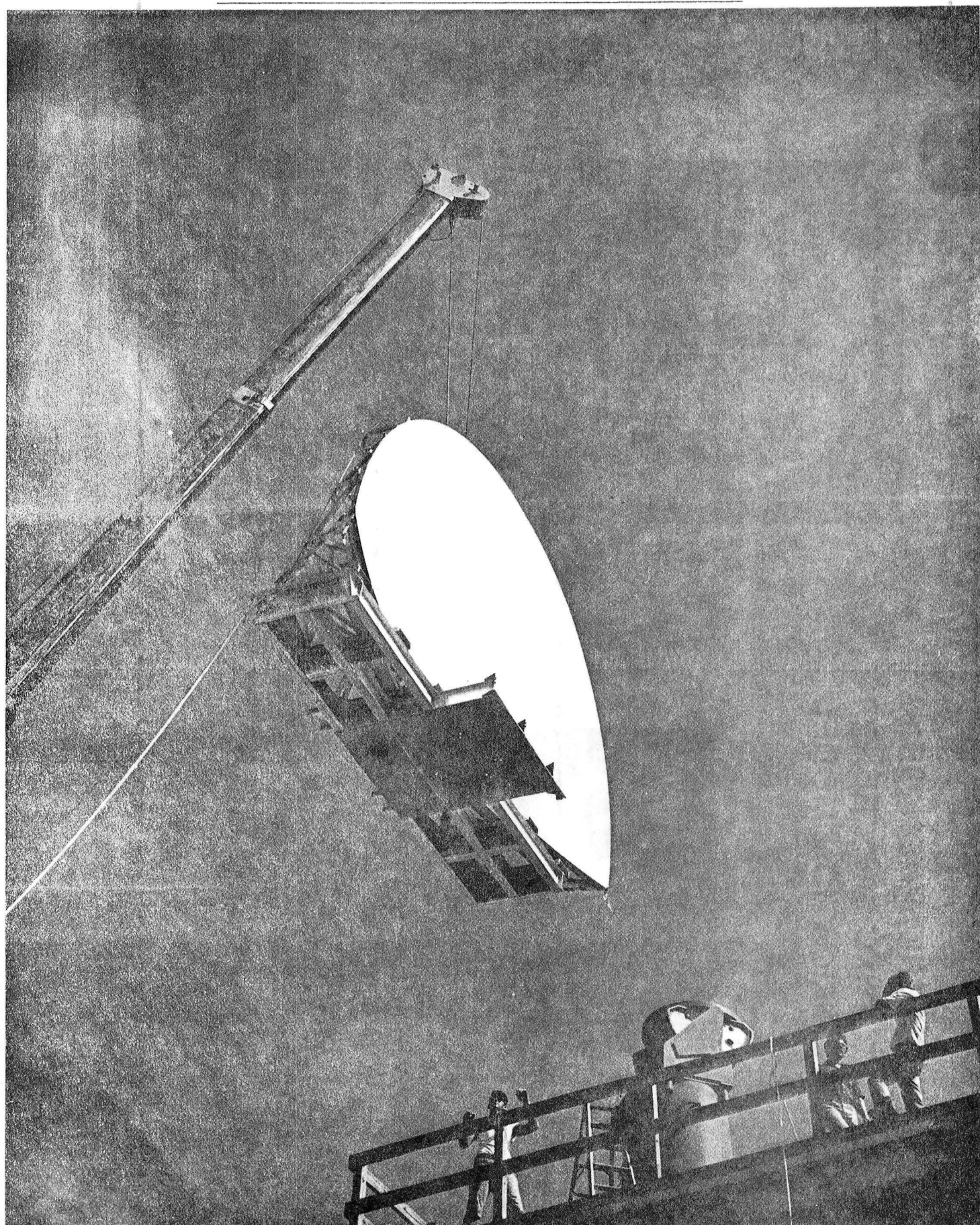


Figure 7. PHOTOGRAPH OF FEED ALIGNMENT STRUCTURE  
BEING USED ON ANTENNA RANGE

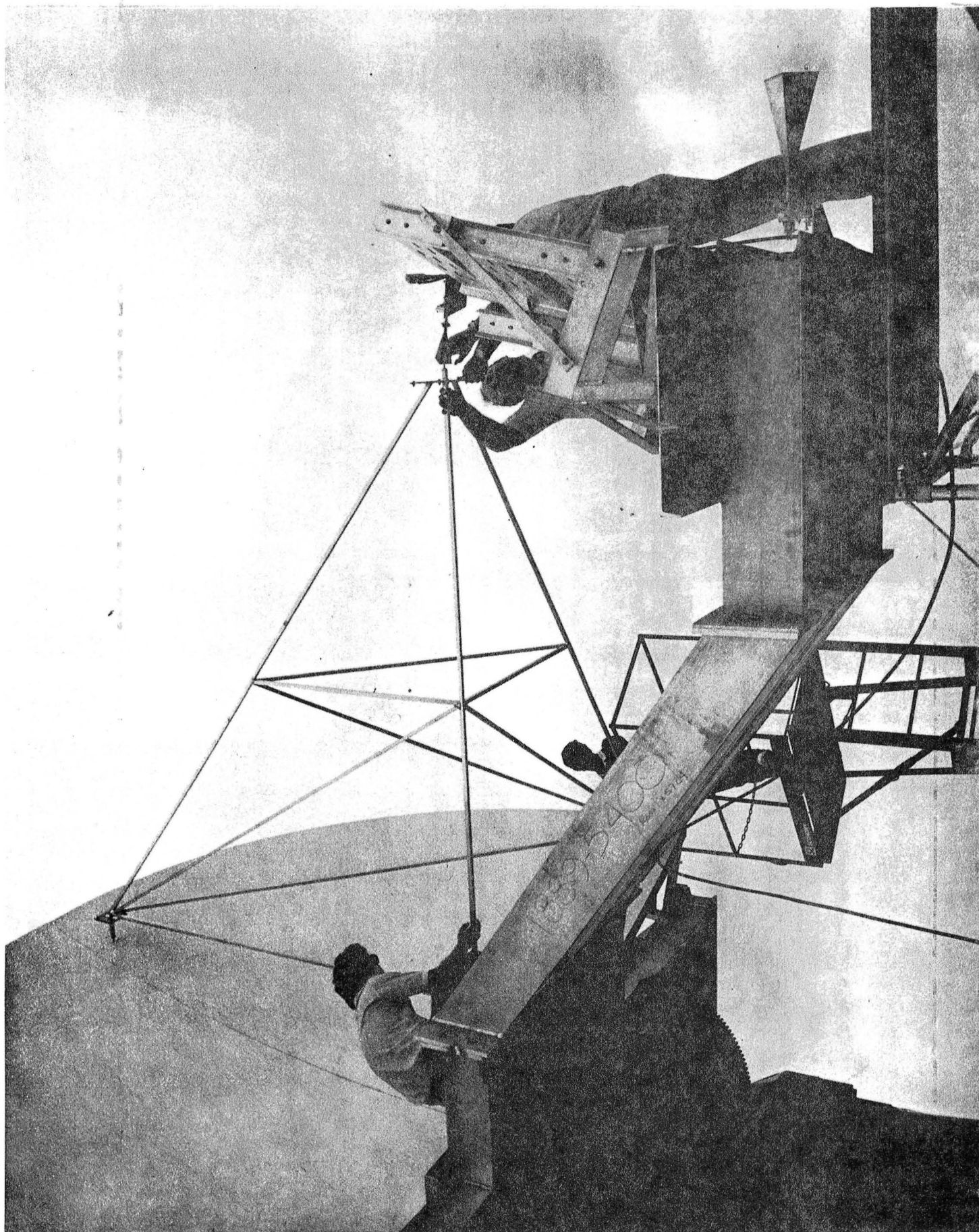




Figure 8. PHOTOGRAPH OF RF VERIFICATION MODEL LOCATED ON ANTENNA RANGE SHOWING THE ALIGNMENT SCOPE AND TRANSMITTING ANTENNA AND TOWER

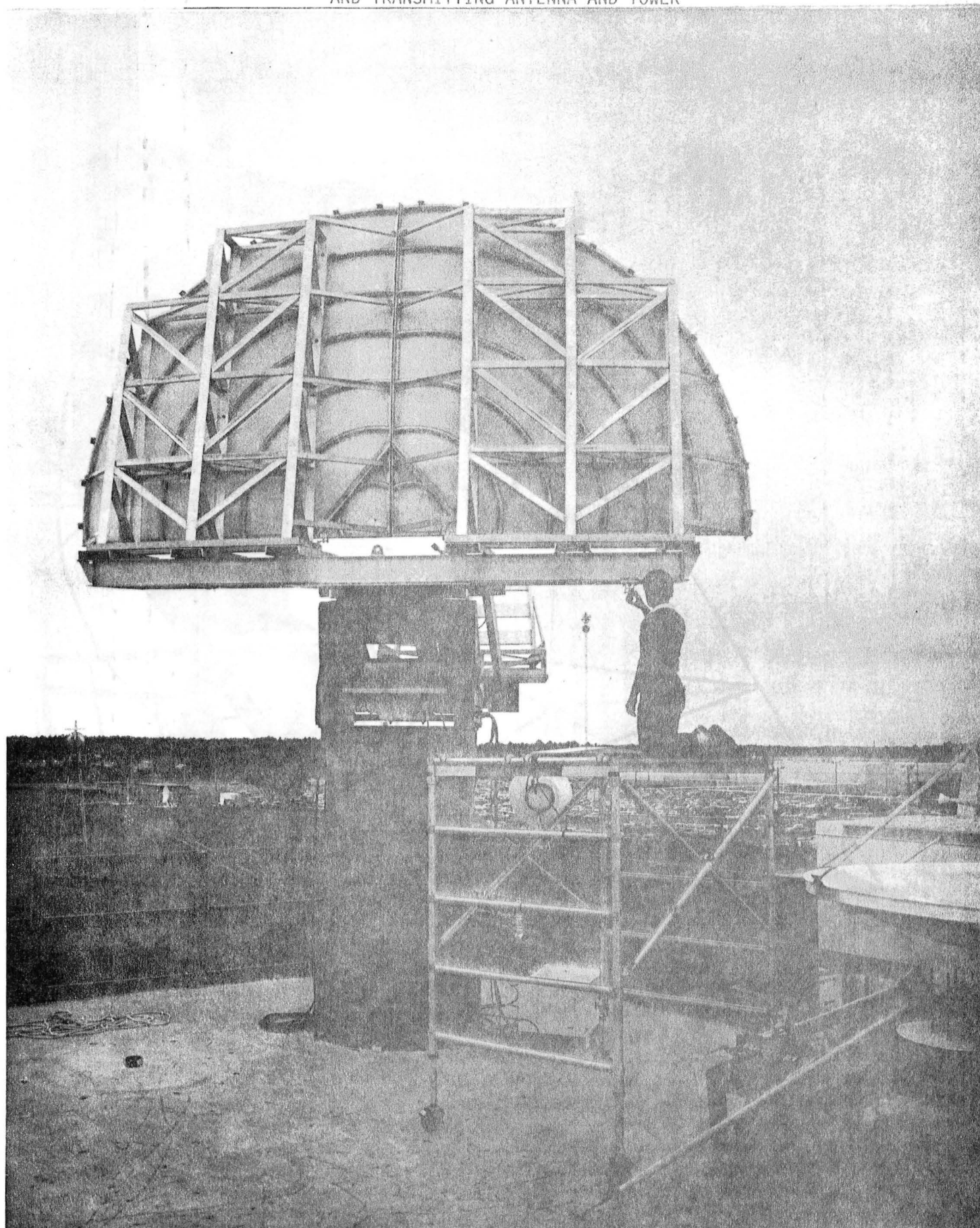


Figure 9. RF VERIFICATION MODEL SHOWING  
QUARTZ CORDS, FRONT VIEW

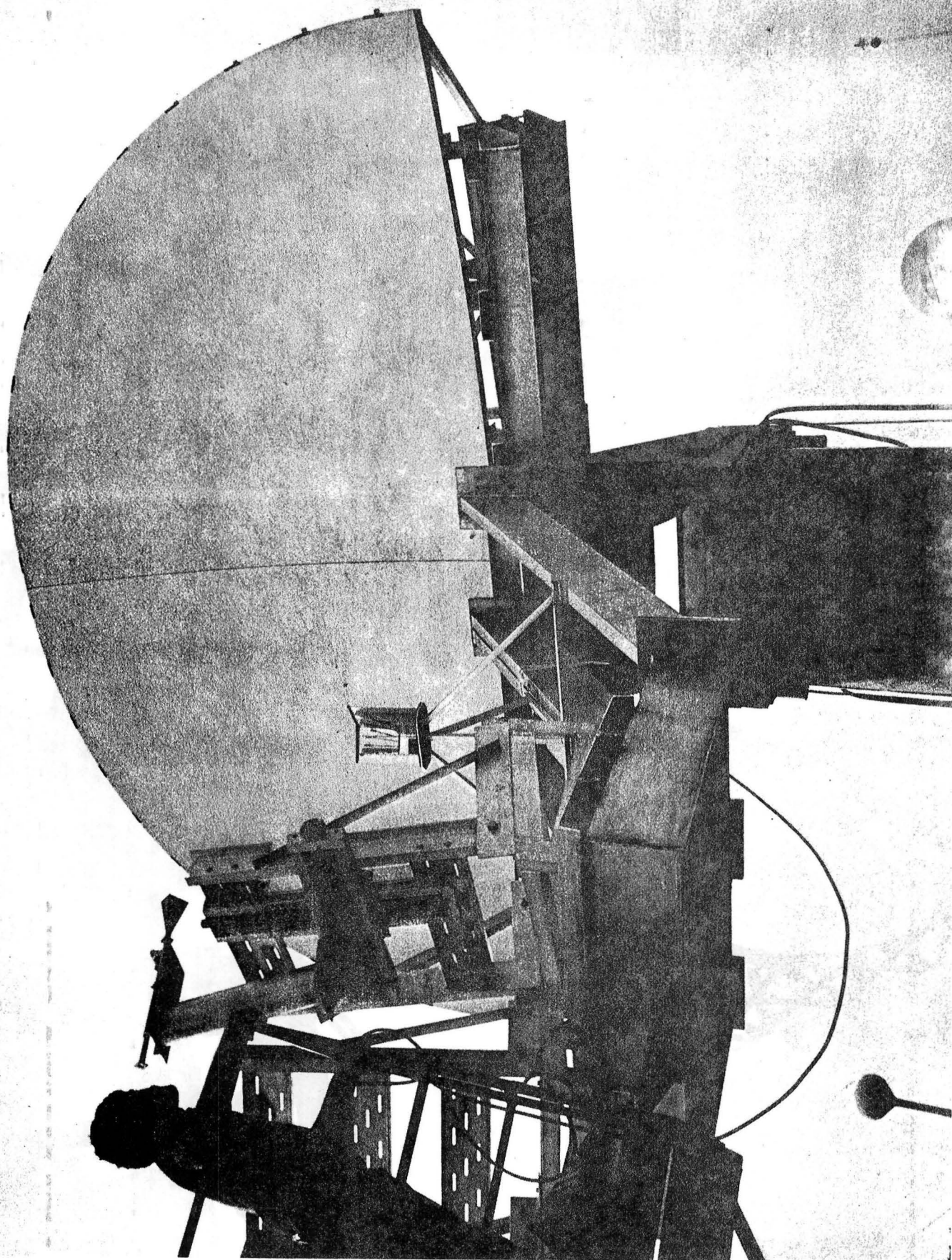
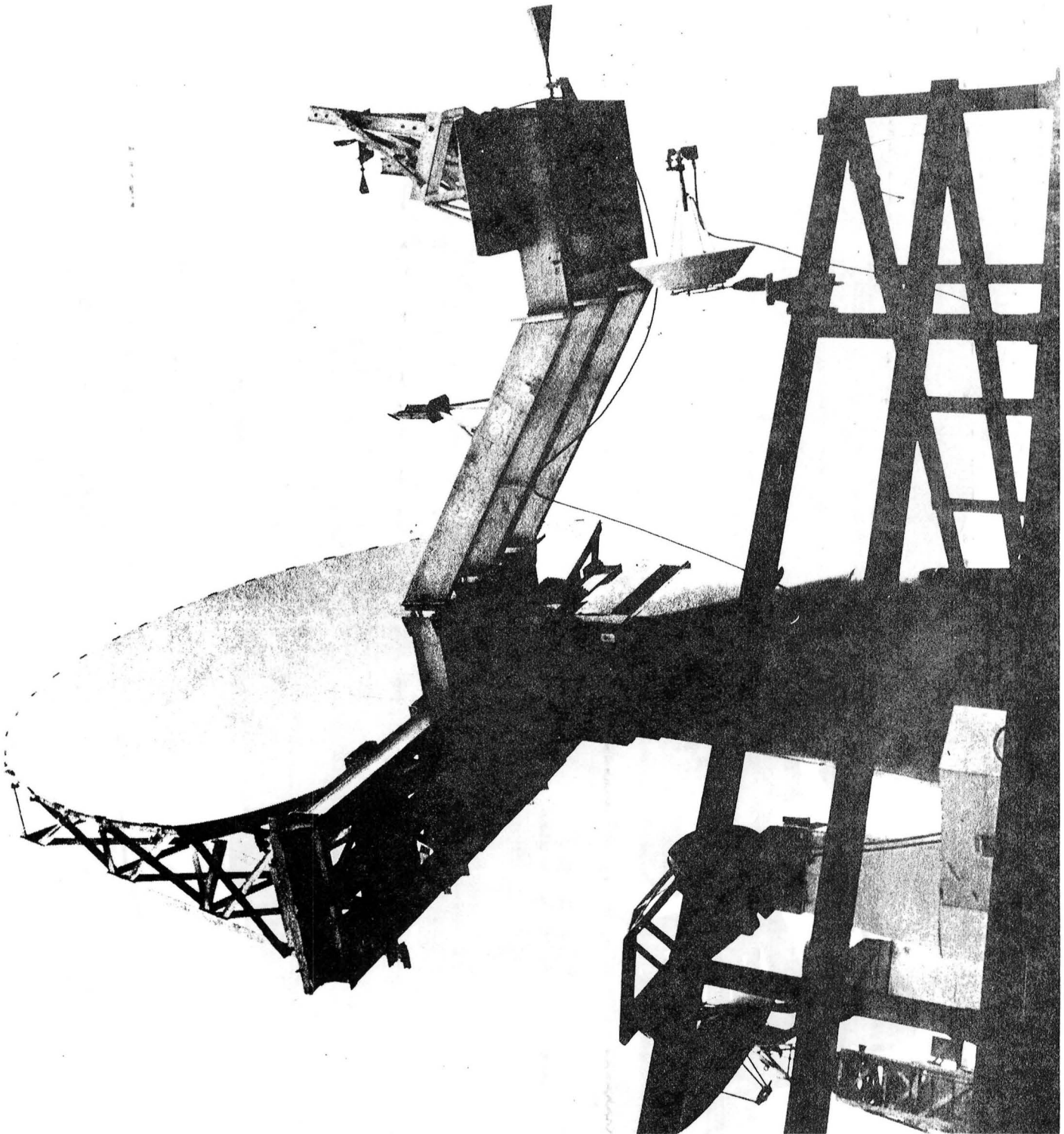


Figure 10. RF VERIFICATION MODEL SHOWING  
QUARTZ CORDS, SIDE VIEW

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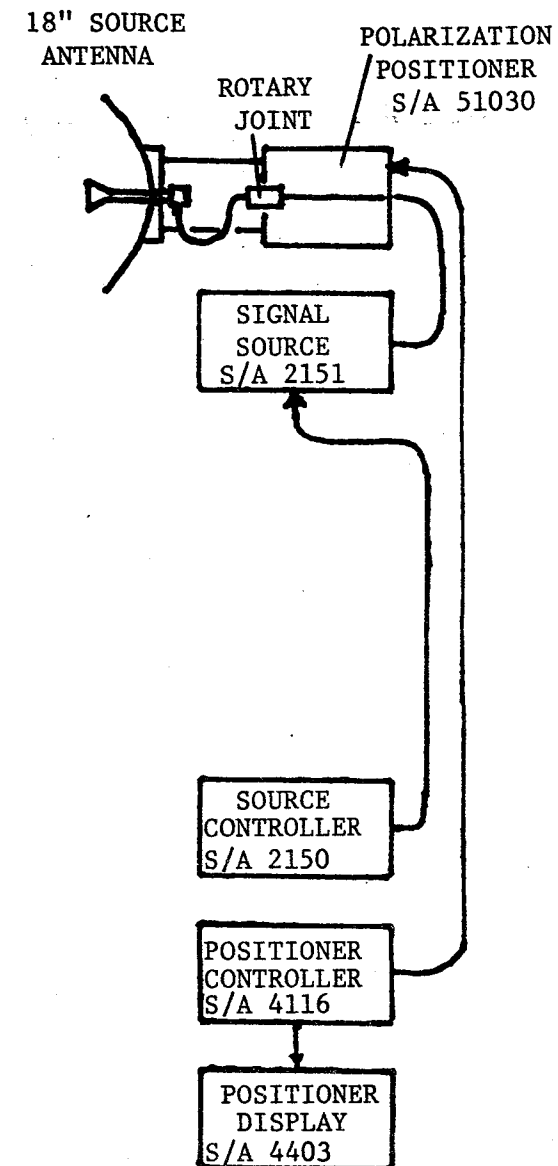
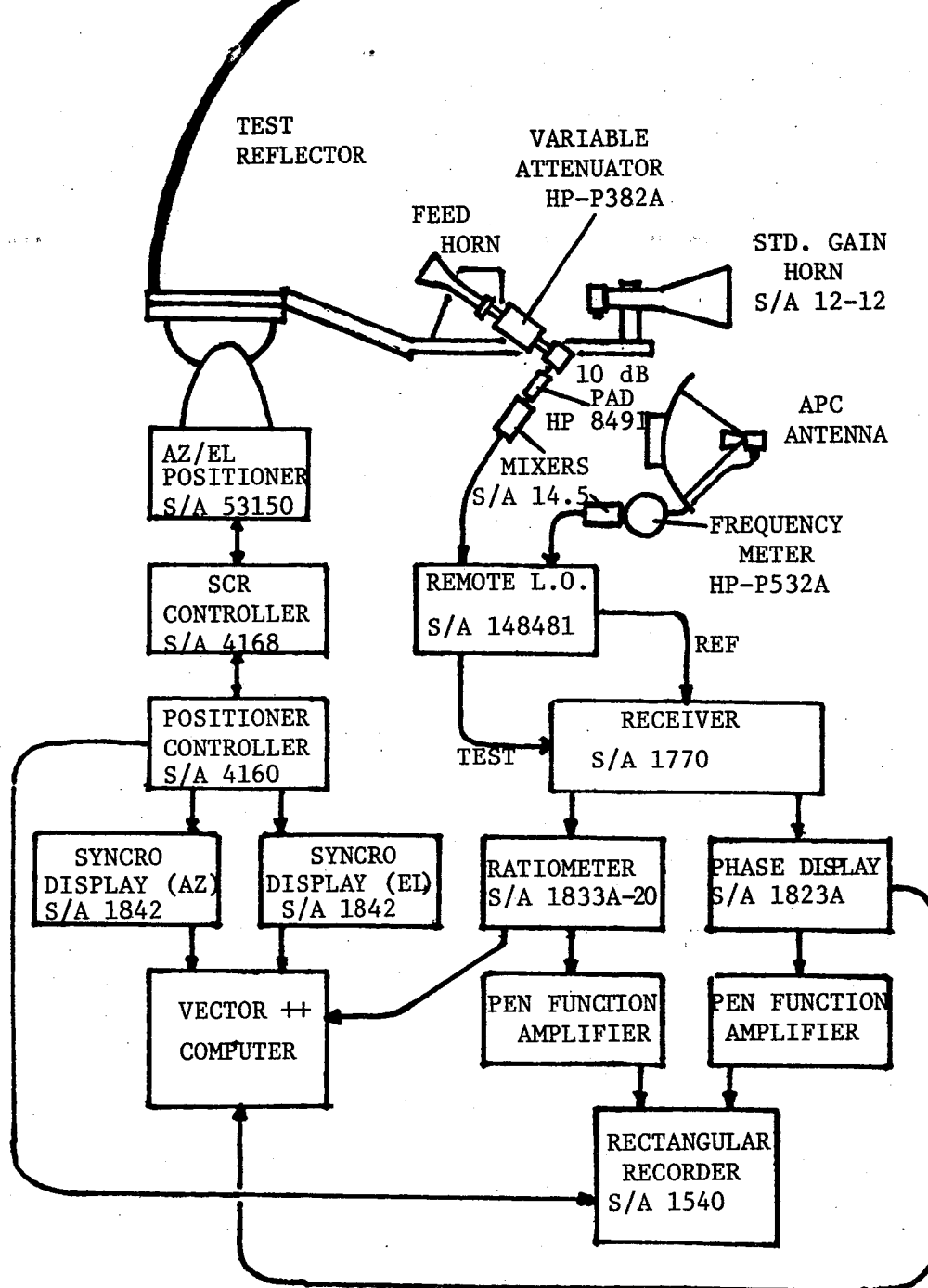
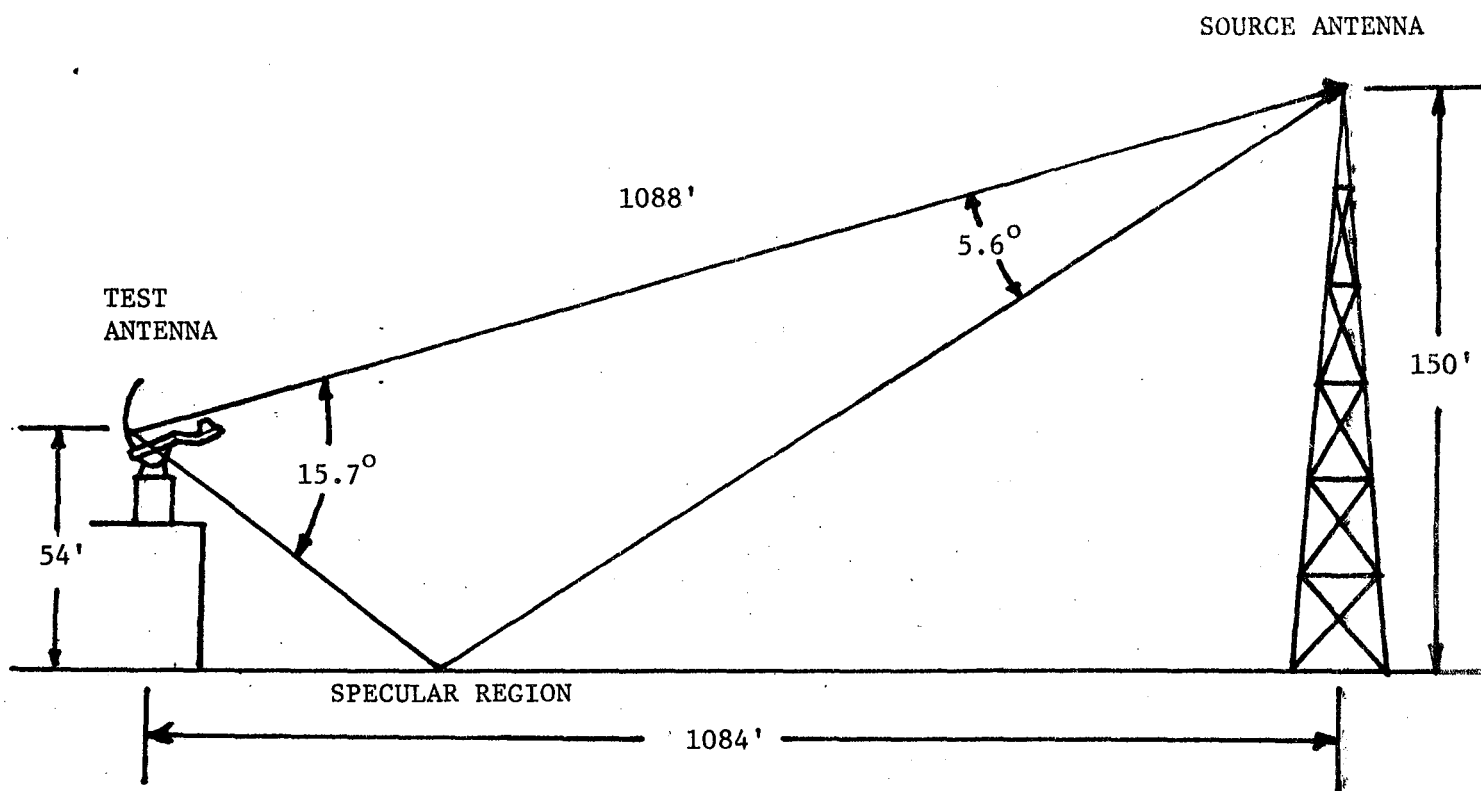


FIGURE 11. ANTENNA RANGE EQUIPMENT DIAGRAM



RANGE LINK BUDGET

	SIGNAL SOURCE	+	8.0 dBm.
	.141 COAX CABLE	-	5.0 dB.
	SOURCE ANTENNA	+	31.0 dB.
	RANGE LOSS	-	106.0 dB.
	APC ANTENNA	+	33.0 dB.
REFERENCE CHANNEL	RECEIVED POWER	-	39.0 dBm.
	RECEIVER SENSITIVITY	-	50.0 dBm.
	MARGIN	+	11.0 dB.
TEST CHANNEL	RECEIVED POWER	-	22.0 dBm.
	RECEIVER SENSITIVITY	-	90.0 dBm.
	DYNAMIC RANGE		68.0 dB.

FIGURE 12. RANGE GEOMETRY and LINK CALCULATIONS

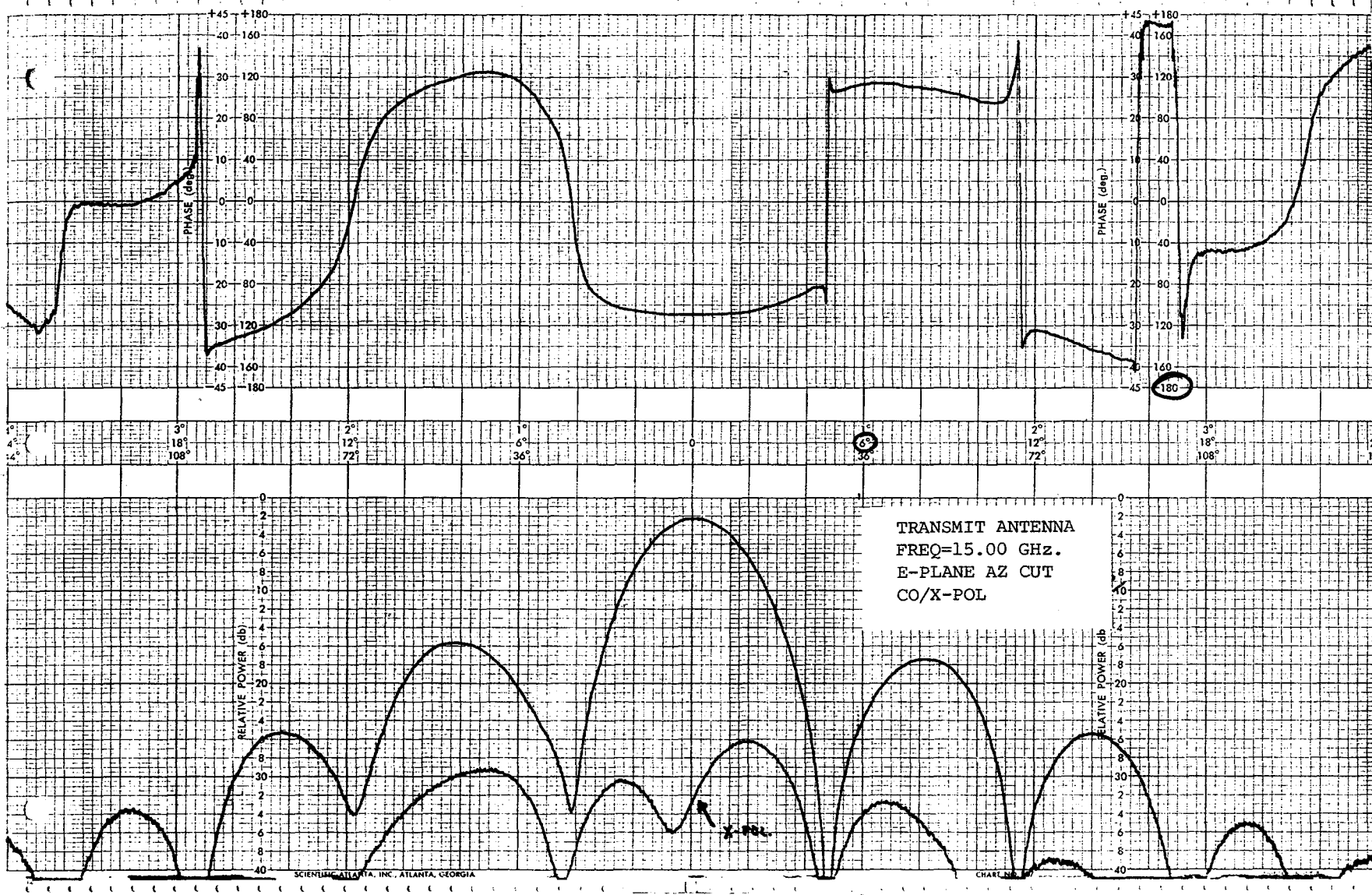


Figure 13. TRANSMIT ANTENNA PATTERNS, E PLANE-AZIMUTH CUT.

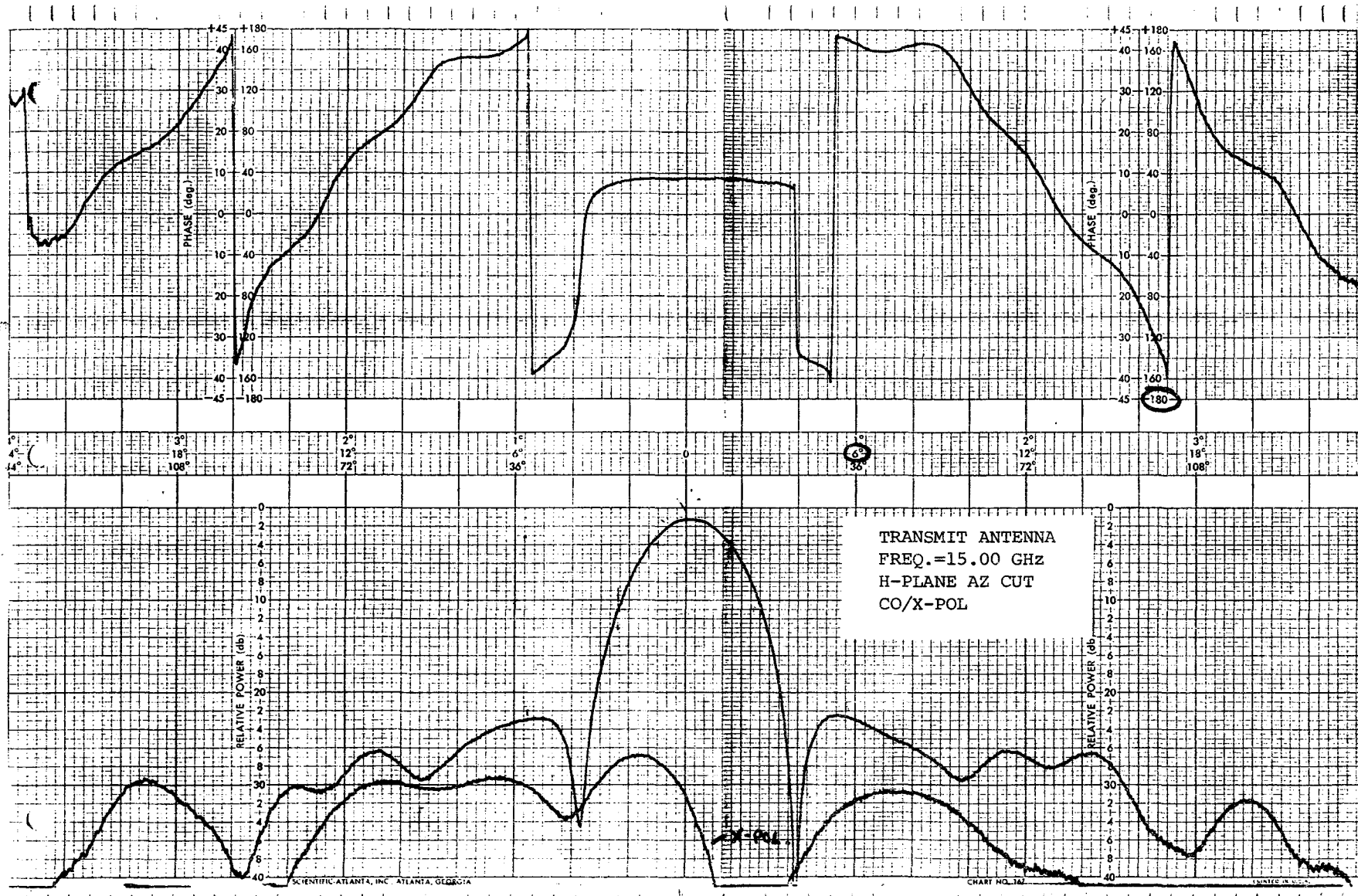
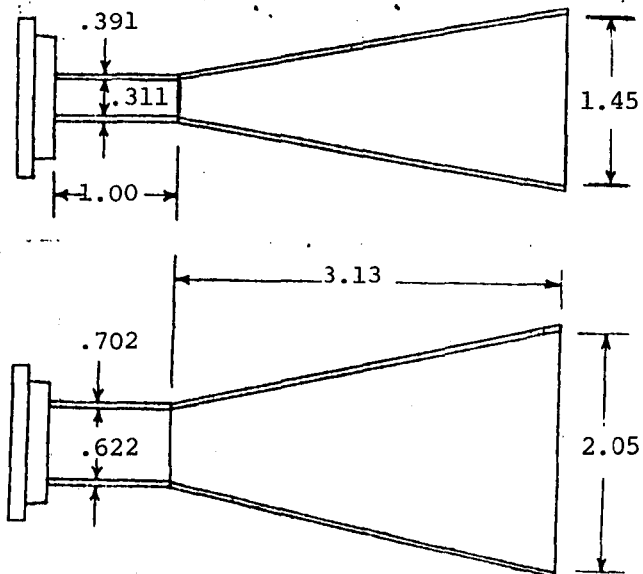
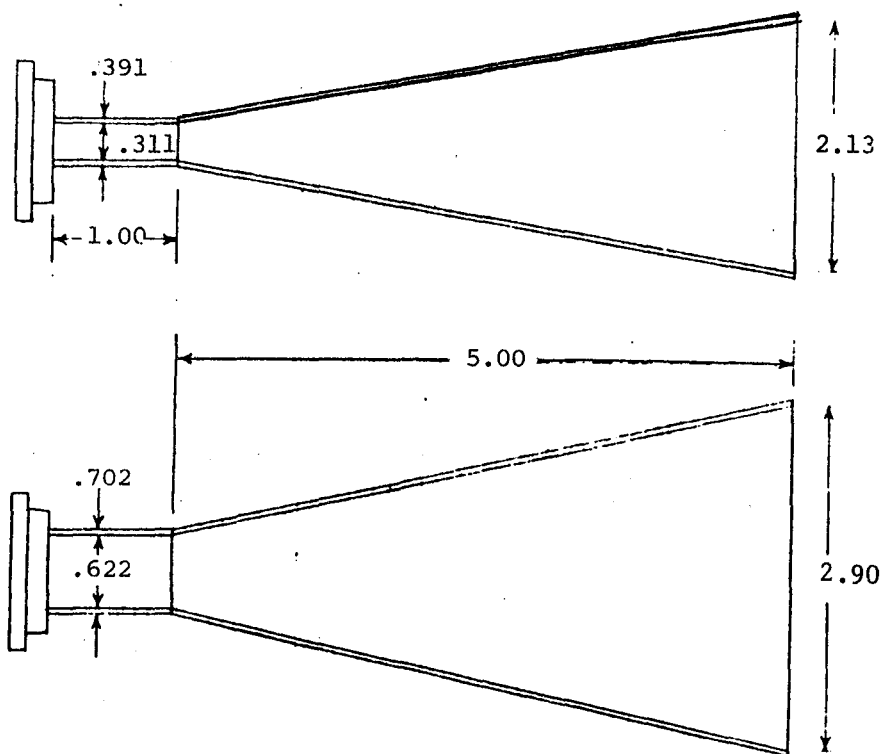


Figure 14. TRANSMIT ANTENNA PATTERNS, H PLANE AZIMUTH CUT.

A) LARGE HORN  
14dB TAPER



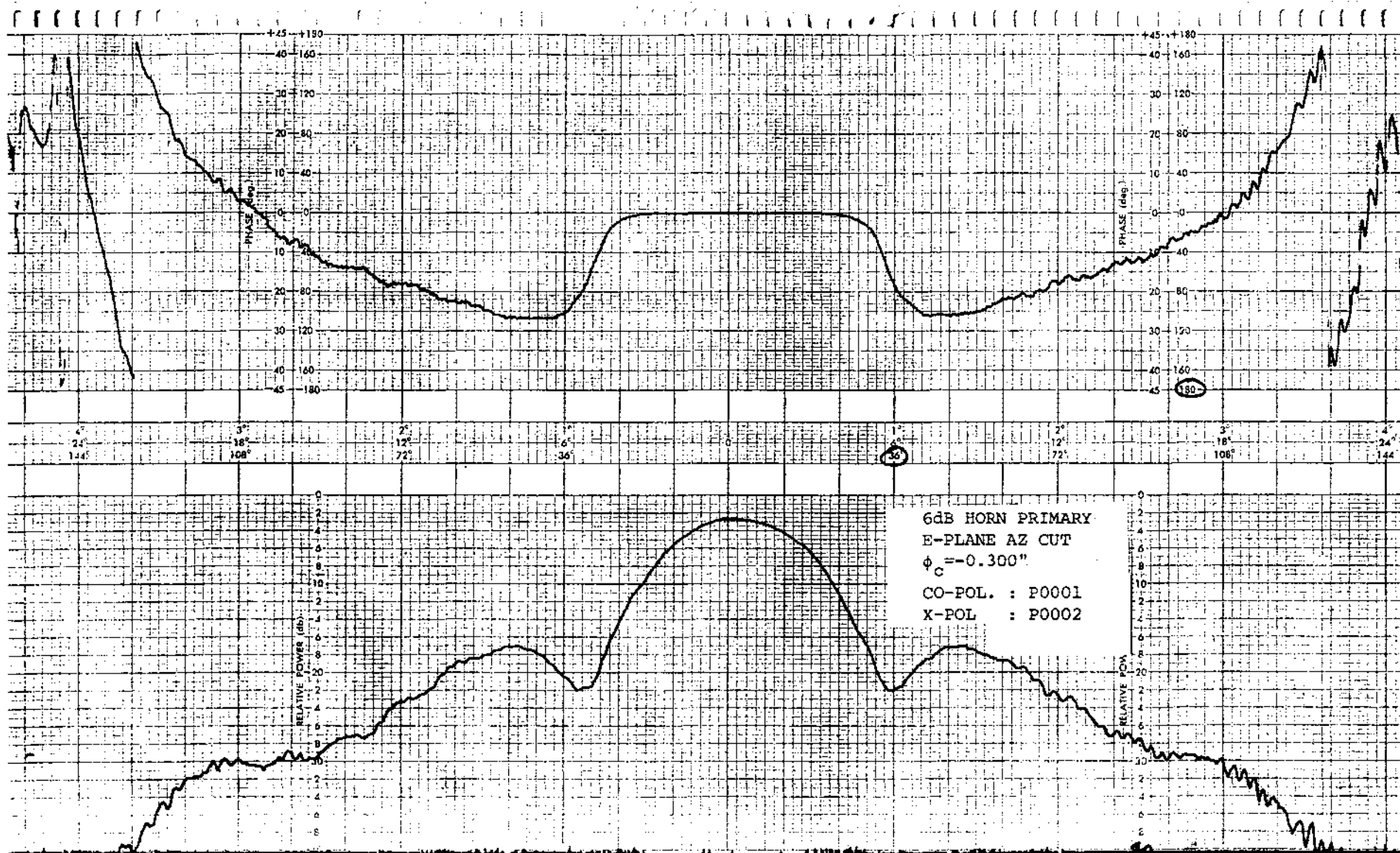
B) SMALL HORN  
6dB TAPER

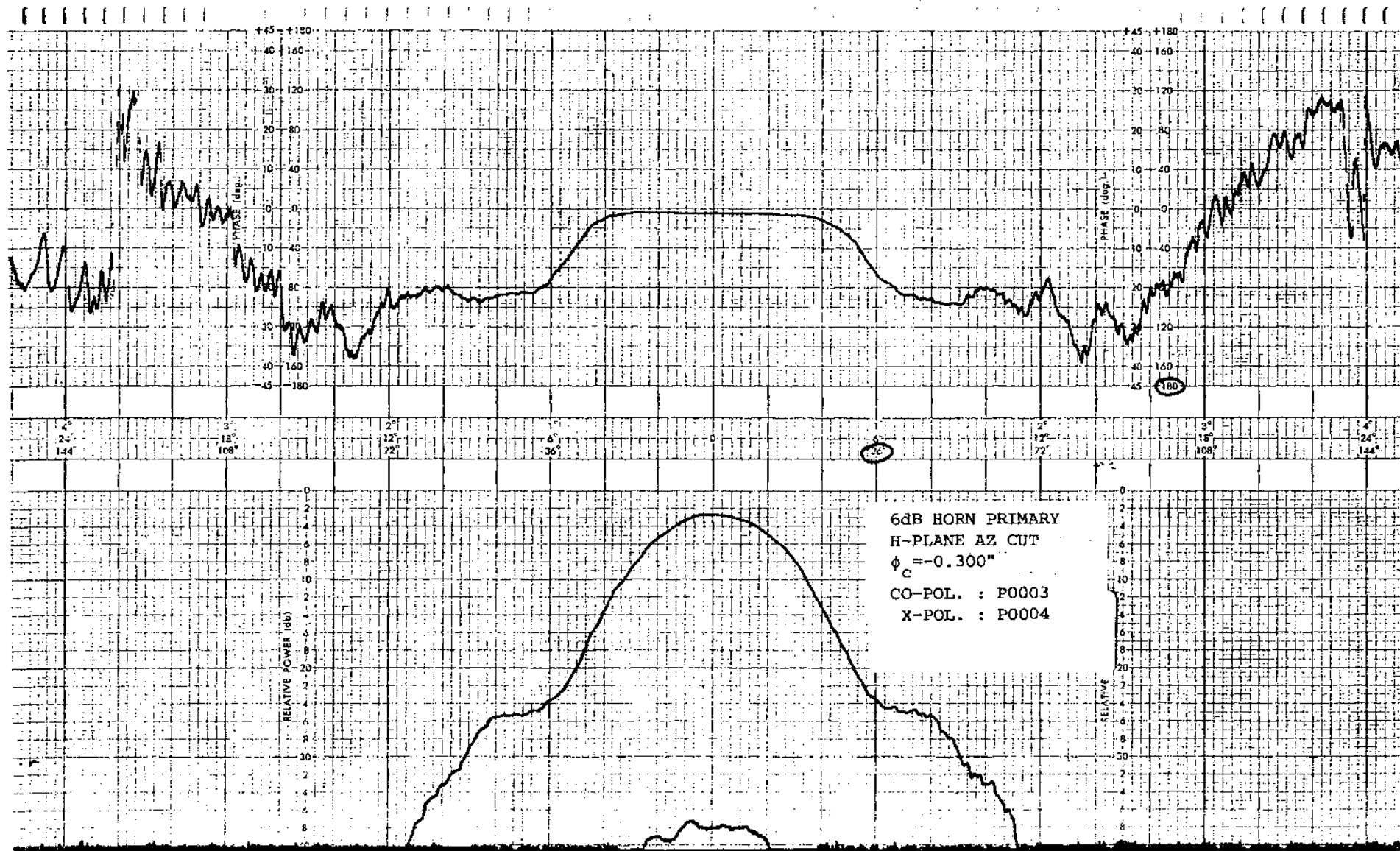
FIGURE 15. FEED HORNS

LSST - I

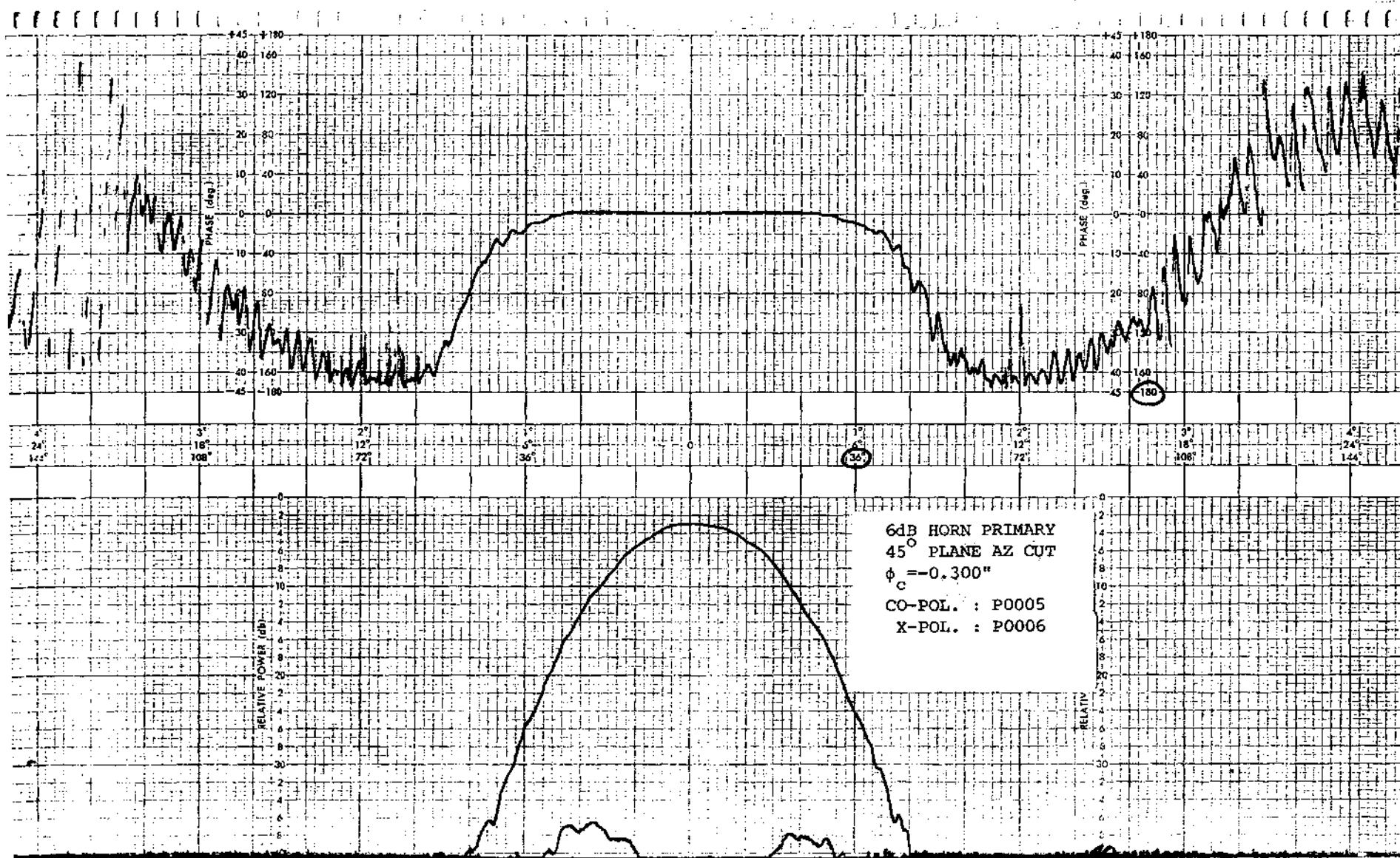
PRIMARY PATTERN LOG

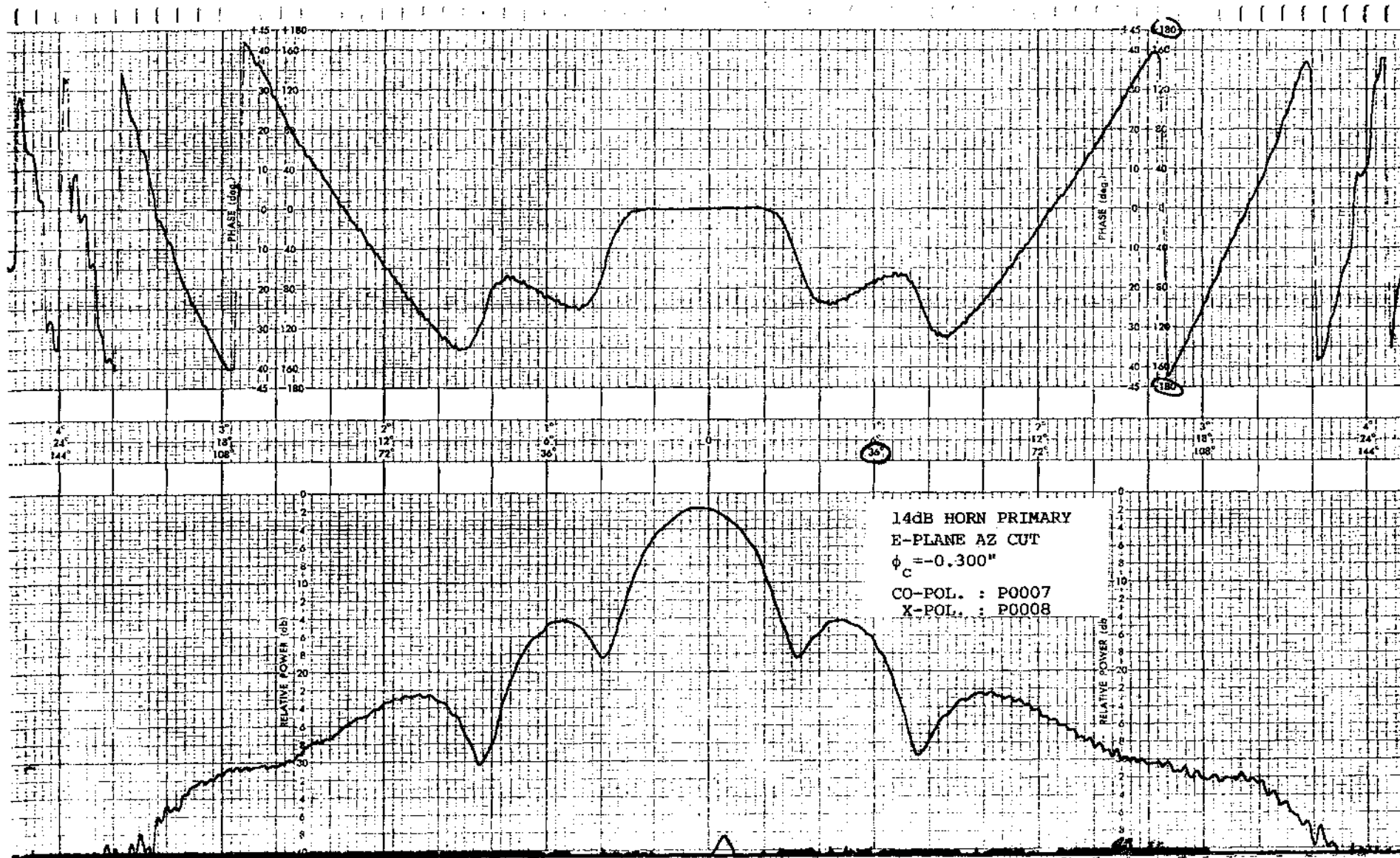
<u>HORN</u>	<u>PLANE</u>	<u>POLARIZATION</u>	<u>FILE NAME</u>	<u>PAGE NUMBER</u>
6 dB	E	CO	P0001	25
6 dB	E	X	P0002	25
6 dB	H	CO	P0003	26
6 dB	H	X	P0004	26
6 dB	45°	CO	P0005	27
6 dB	45°	X	P0006	27
14 dB	E	CO	P0007	28
14 dB	E	X	P0008	28
14 dB	H	CO	P0009	29
14 dB	H	X	P0010	29
14 dB	45°	CO	P0011	30
14 dB	45°	X	P0012	30

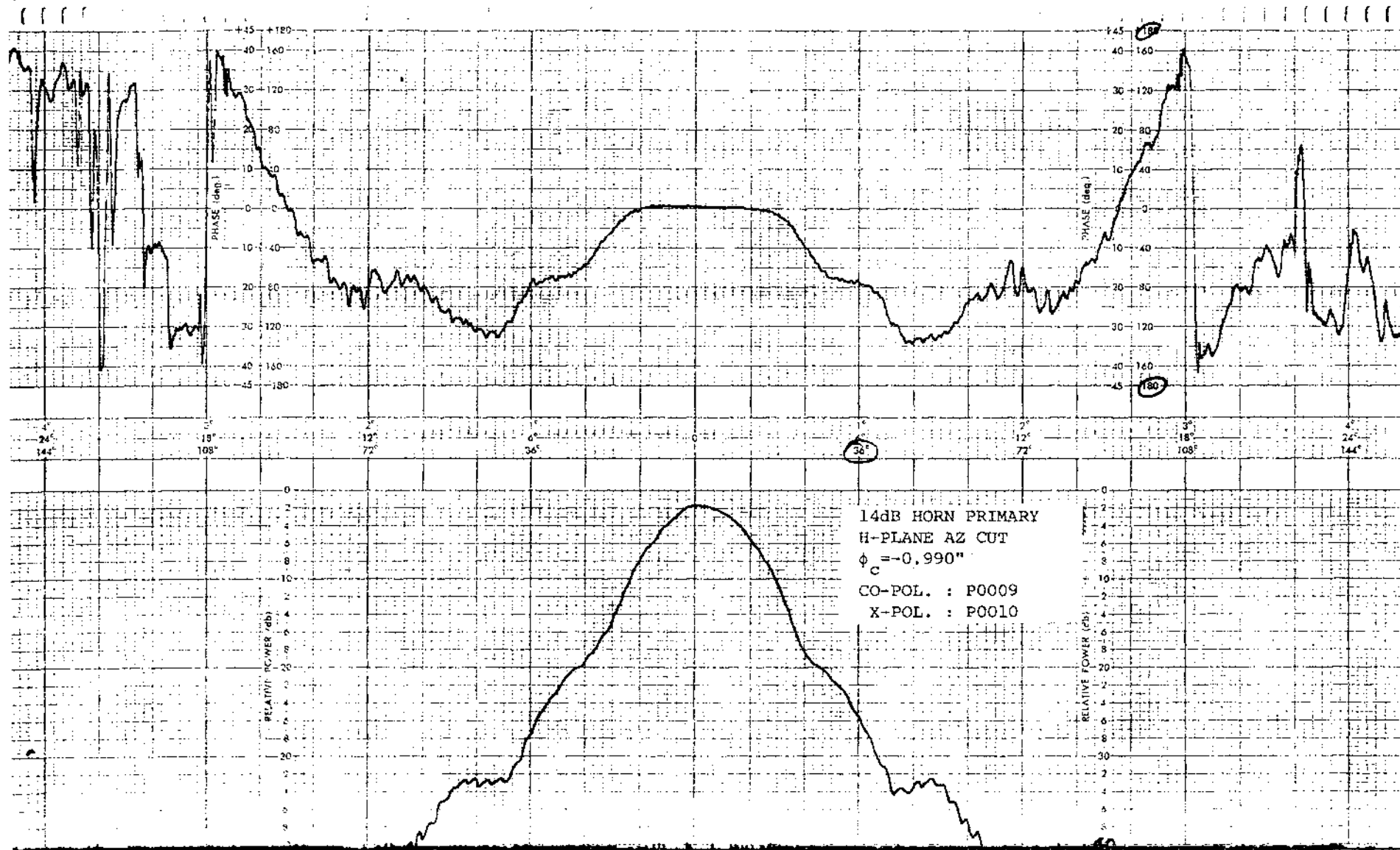


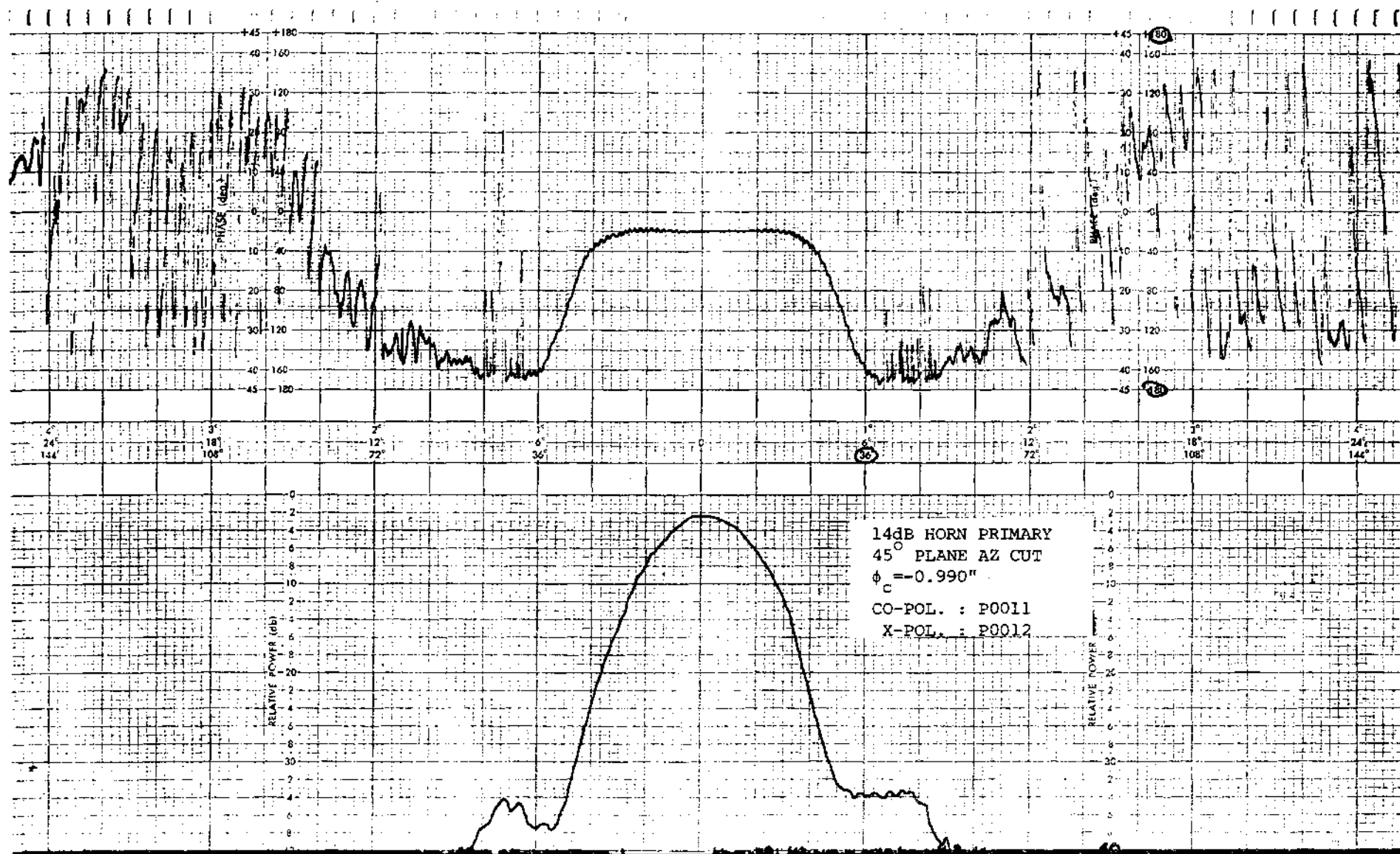













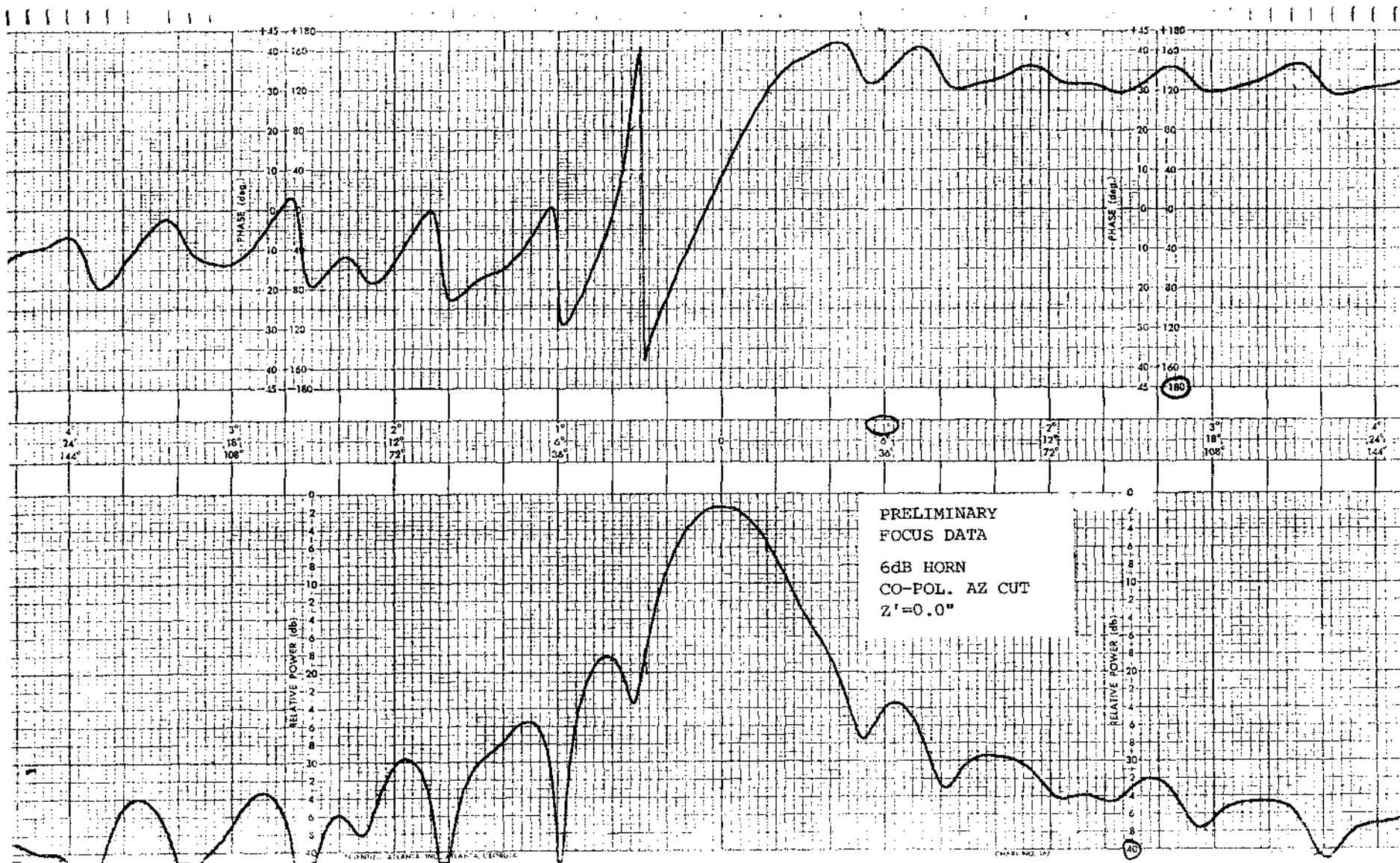
LSST - II  
PRELIMINARY FOCUS DATA  
SECONDARY PATTERN LOG

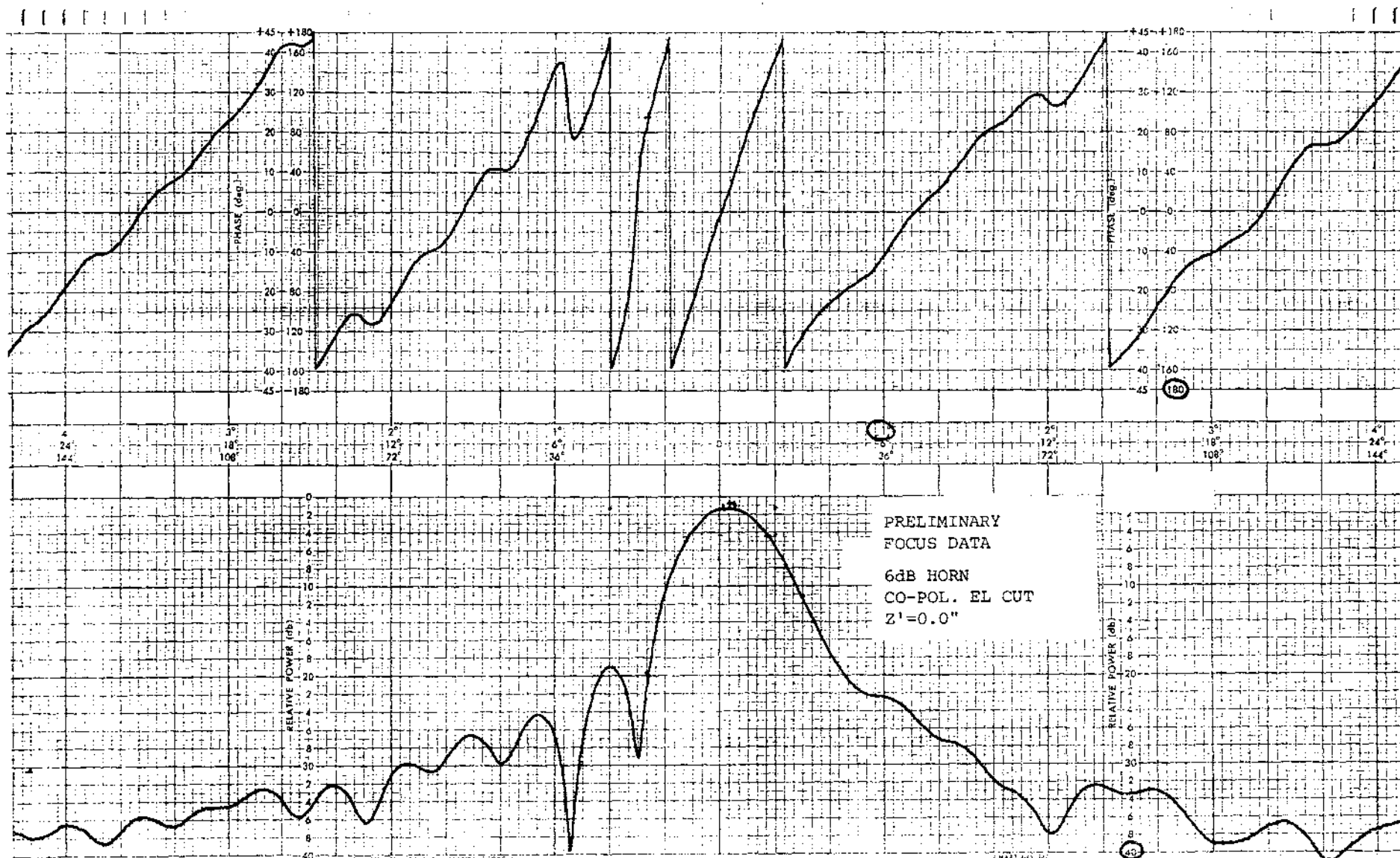
-31-

<u>CONFIGURATION</u>	<u>HORN</u>	<u>FEED AXIAL POSITION</u>	<u>POL.</u>	<u>PEAK GAIN (dB1)</u>	<u>PATTERN</u>	<u>PAGE NUMBER</u>
	6 dB	0.0"*	CO	50.36	+ 5° AZ	32
	6 dB	0.0"	CO	"	+ 5° EL	33
	6 dB	+0.4"	CO	50.70	+ 5° AZ	34
	6 dB	+0.4"	CO	"	+ 5° EL	35
	6 dB	+0.8"	CO	50.83	+ 5° AZ	36
	6 dB	+0.8"	CO	"	+ 5° EL	37
	6 dB	+1.2"#	CO	50.85	+ 5° AZ	38
	6 dB	+1.2"	CO	"	+ 5° EL	39
	6 dB	+1.6"	CO	50.77	+ 5° AZ	40
	6 dB	+1.6"	CO	"	+ 5° EL	41
	6 dB	+1.8"	CO	50.66	+ 5° AZ	42
	6 dB	+1.8"	CO	"	+ 5° EL	43
	6 dB	+2.0"	CO	50.50	+ 5° AZ	44
	6 dB	+2.0"	CO	"	+ 5° EL	45
	14 dB	0.0"*	CO	50.00	+ 5° AZ	46
	14 dB	0.0"	CO	"	+ 5° EL	47
	14 dB	+0.8"	CO	50.48	+ 5° AZ	48
	14 dB	+0.8"	CO	"	+ 5° EL	49
	14 dB	+1.2"#	CO	50.52	+ 5° AZ	50
	14 dB	+1.2"	CO	"	+ 5° EL	51
	14 dB	+1.6"	CO	50.37	+ 5° AZ	52
	14 dB	+1.6"	CO	"	+ 5° EL	53
	14 dB	+1.8"	CO	50.35	+ 5° AZ	54
	14 dB	+1.8"	CO	"	+ 5° EL	55
	14 dB	+2.0"	CO	50.36	+ 5° AZ	56
	14 dB	+2.0"	CO	"	+ 5° EL	57

\* Z' = 0.0" is the mechanical focus position as determined with alignment tool.

# Z' = +1.2" is the range corrected focus position used for all secondary measurements.

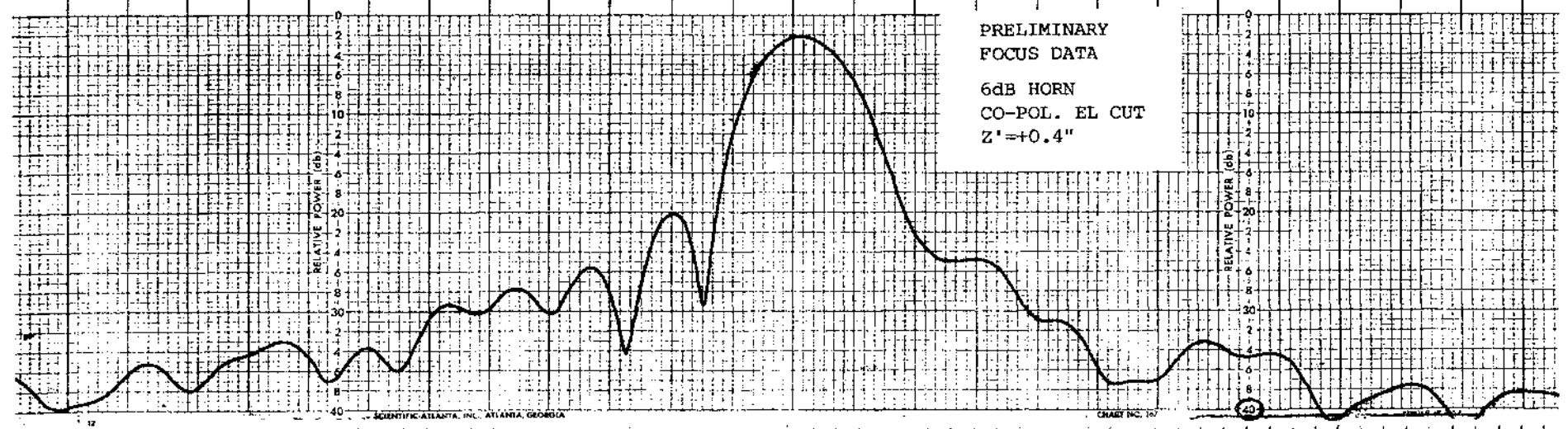
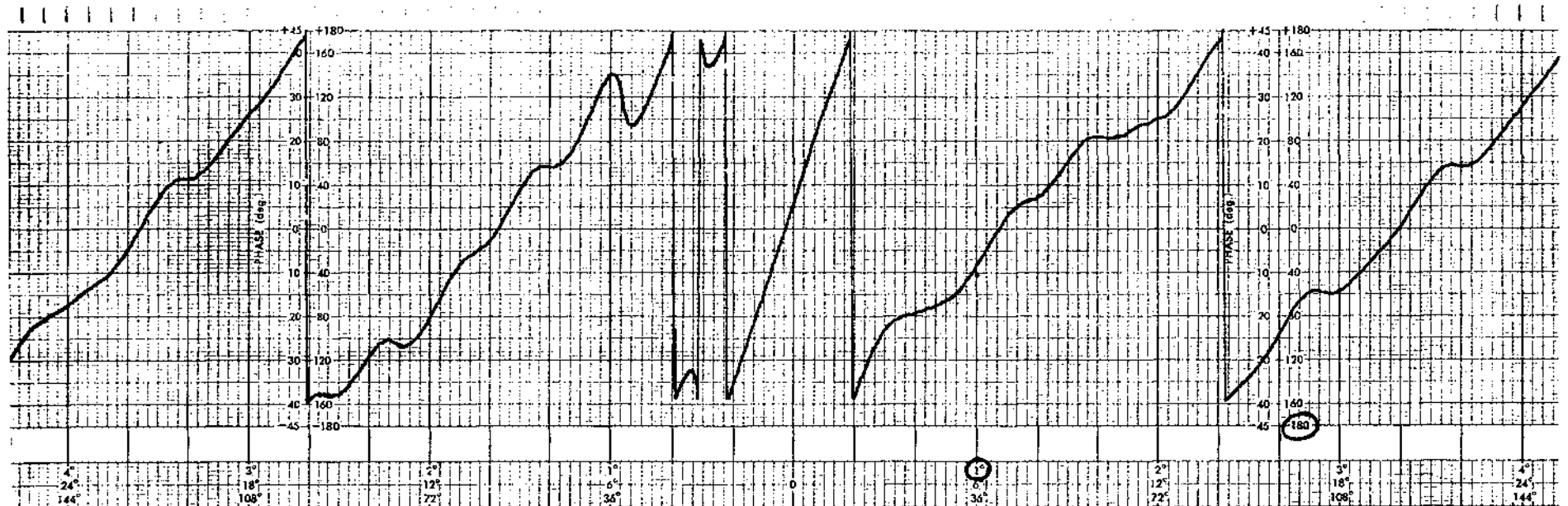


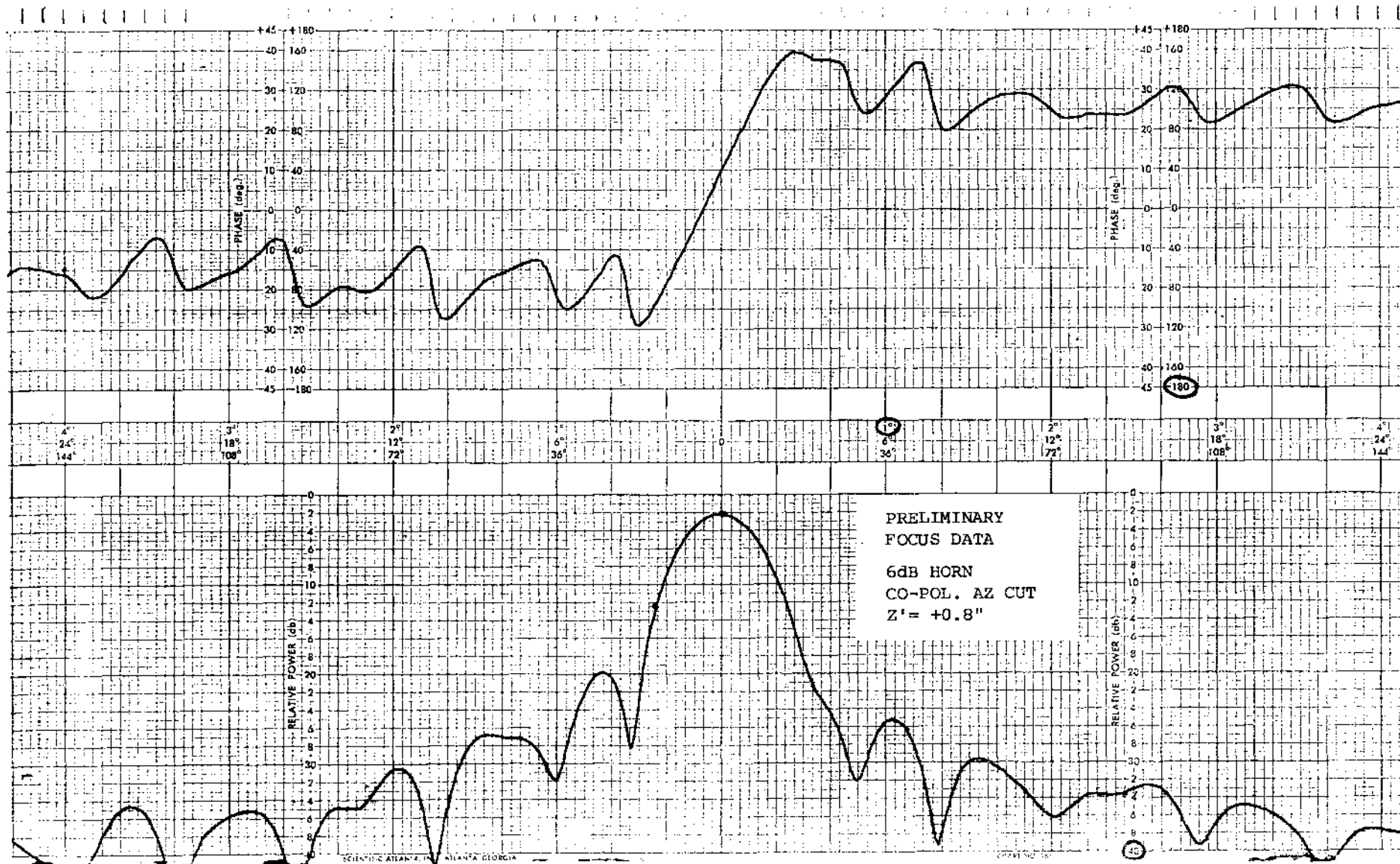




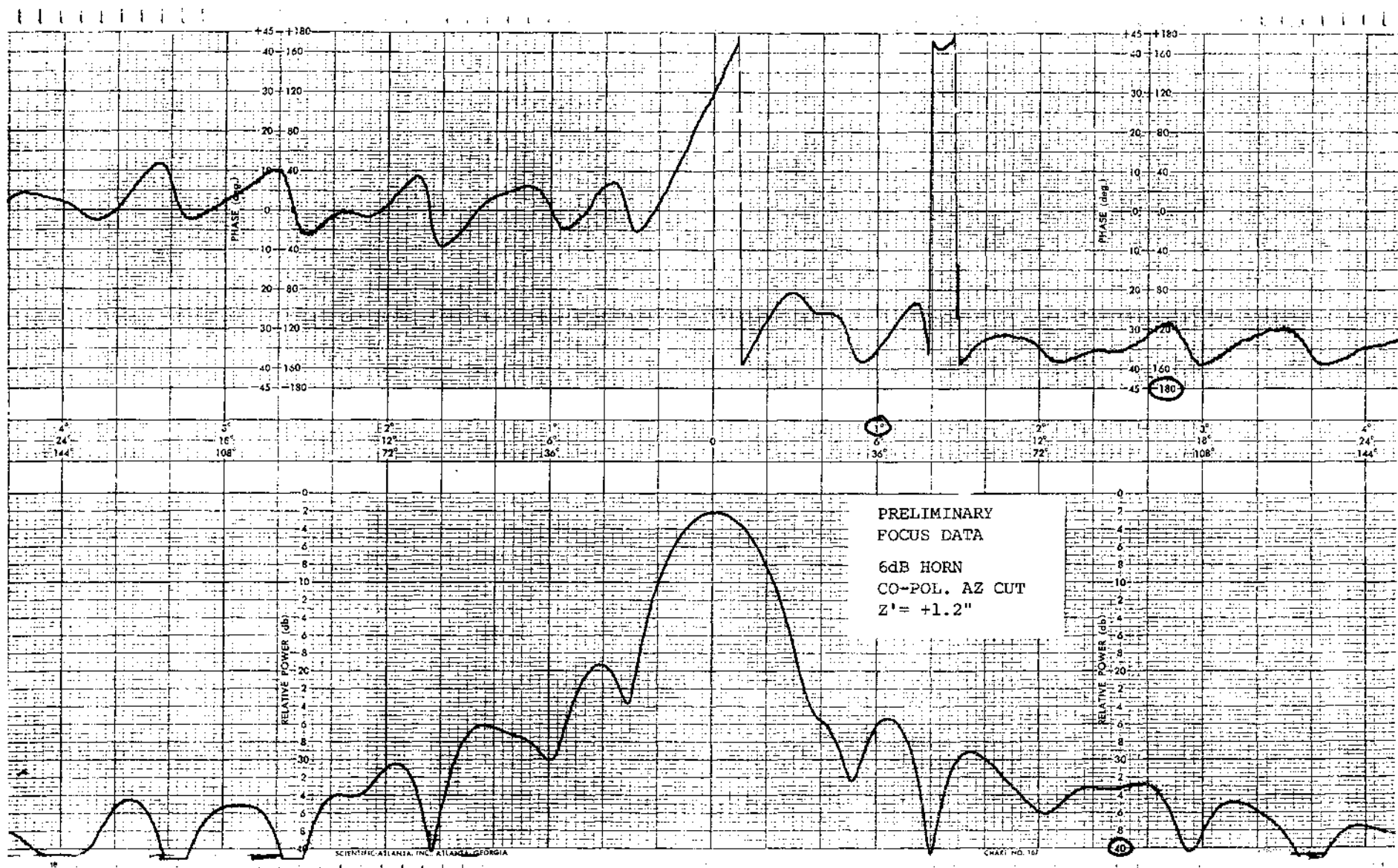




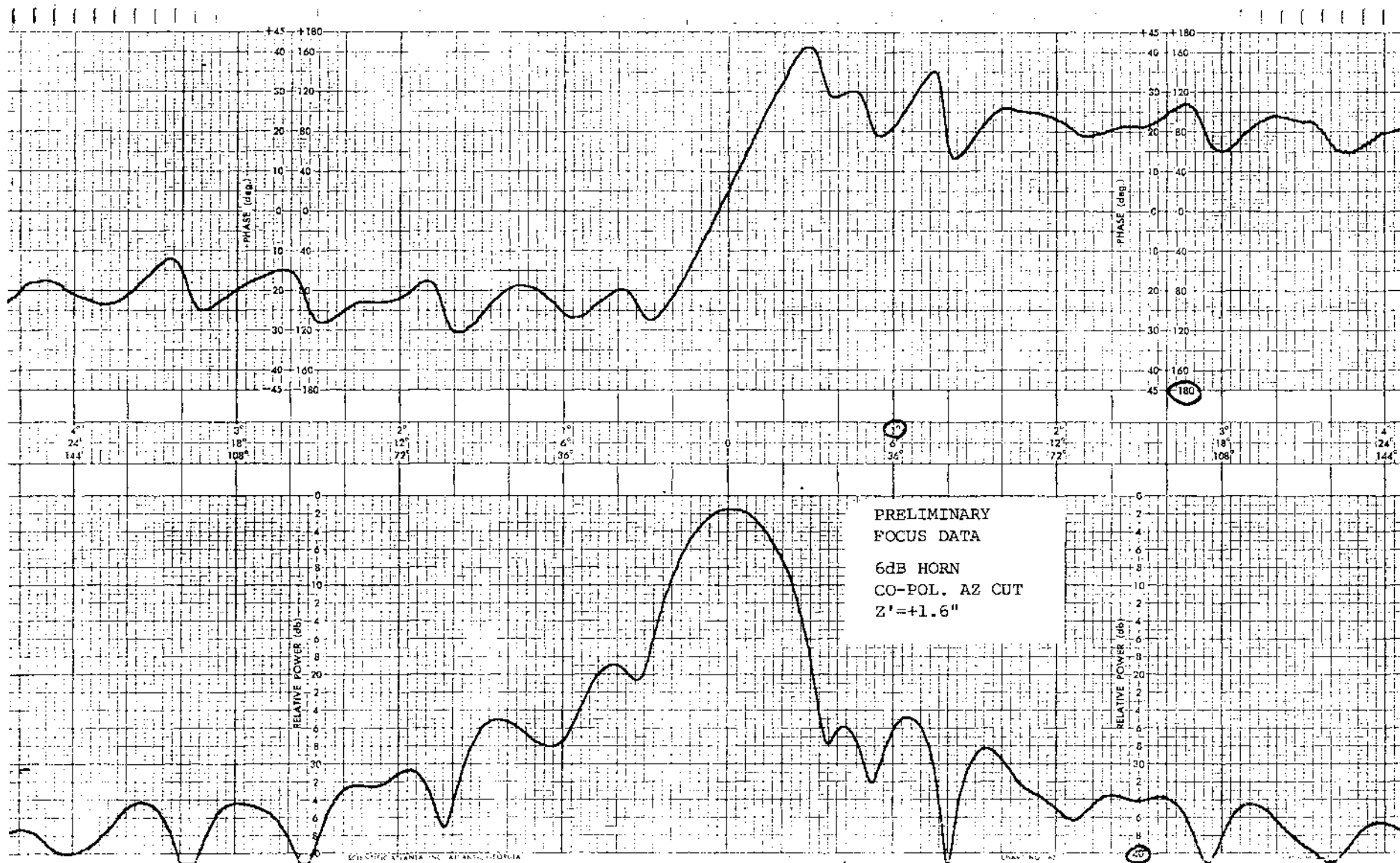




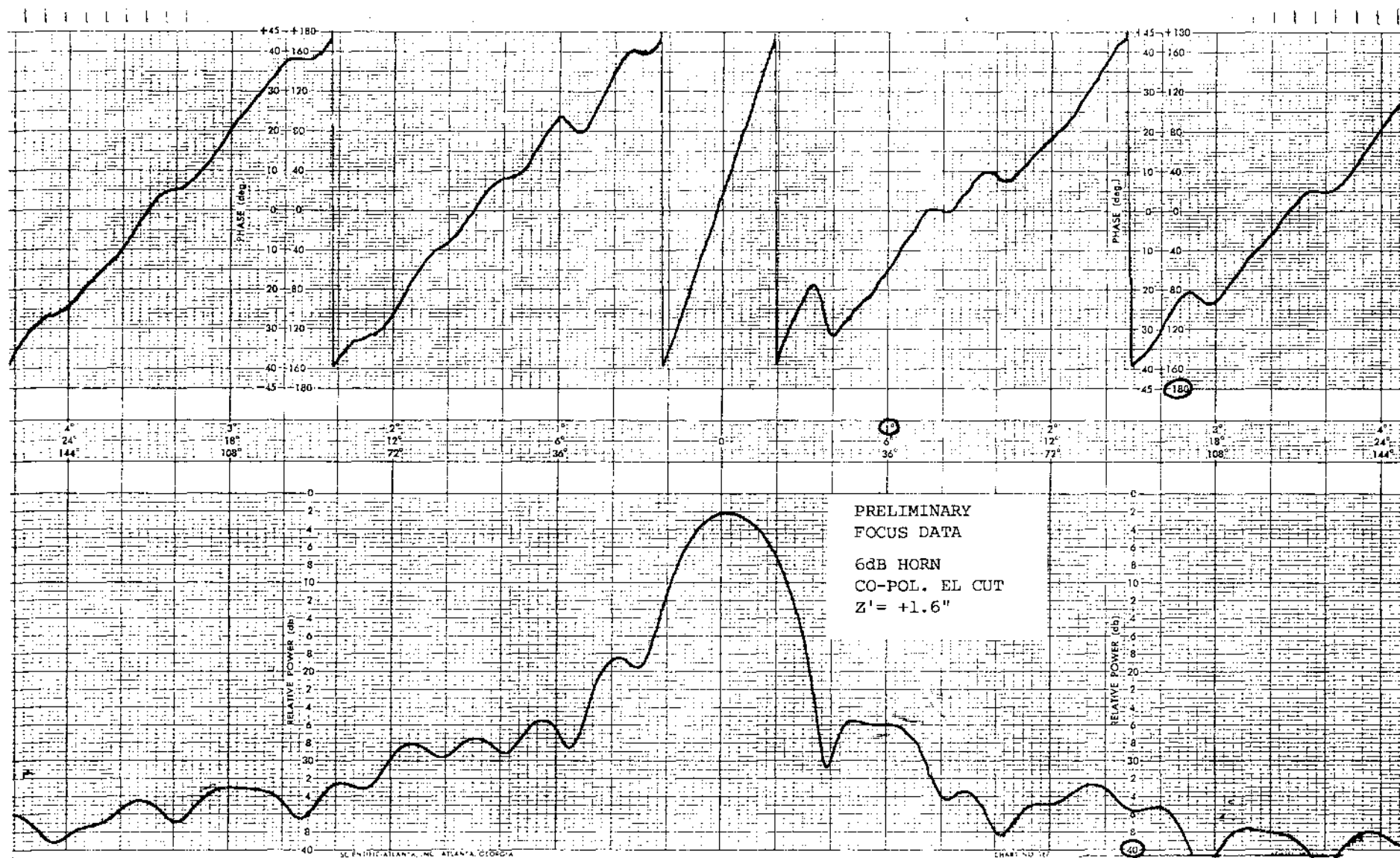


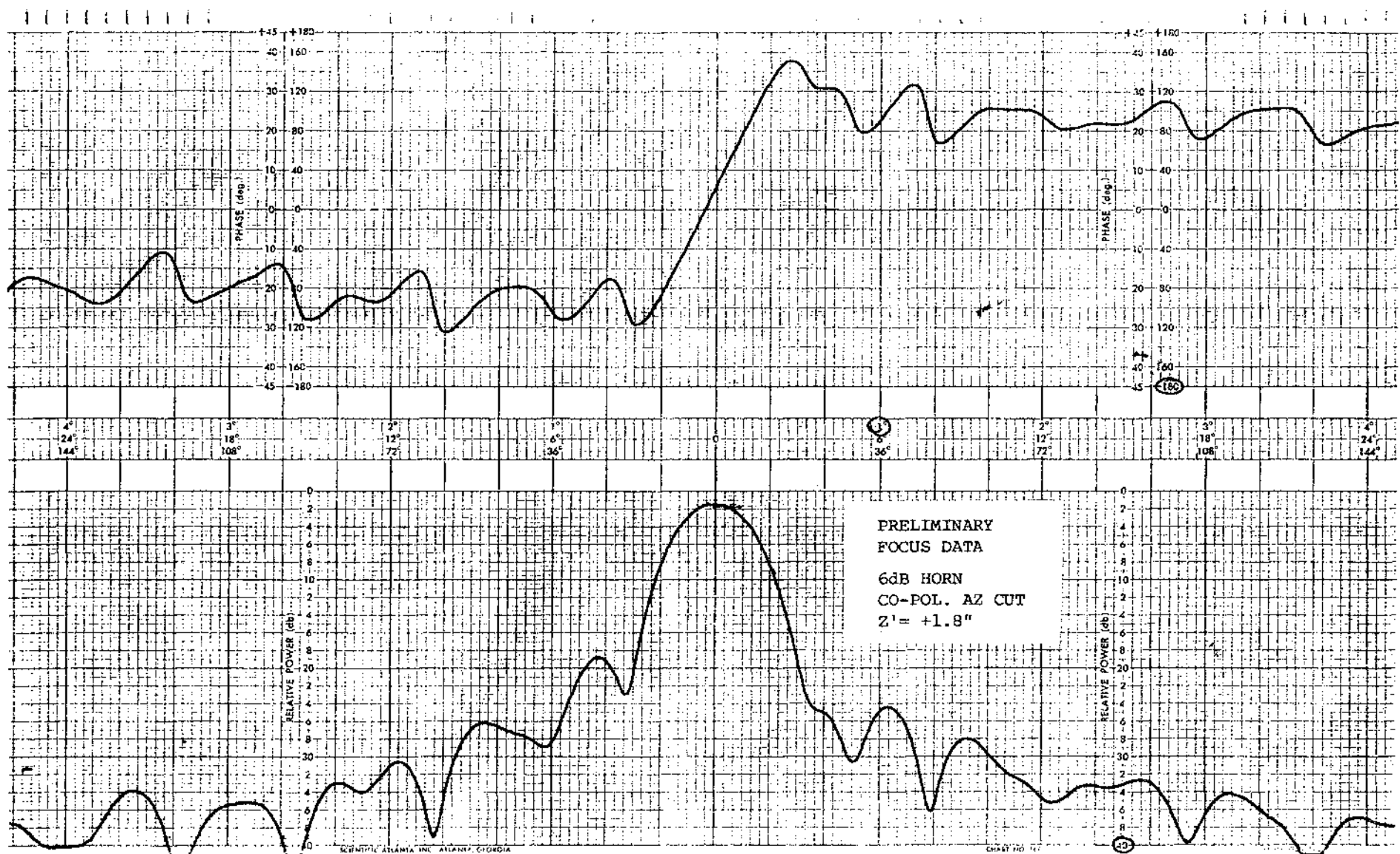




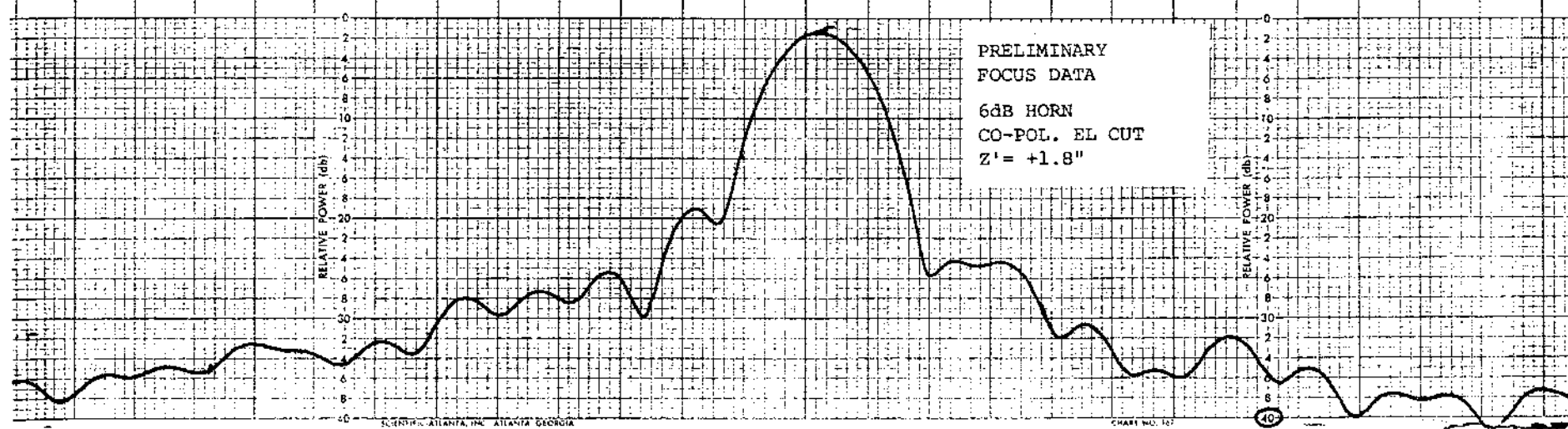
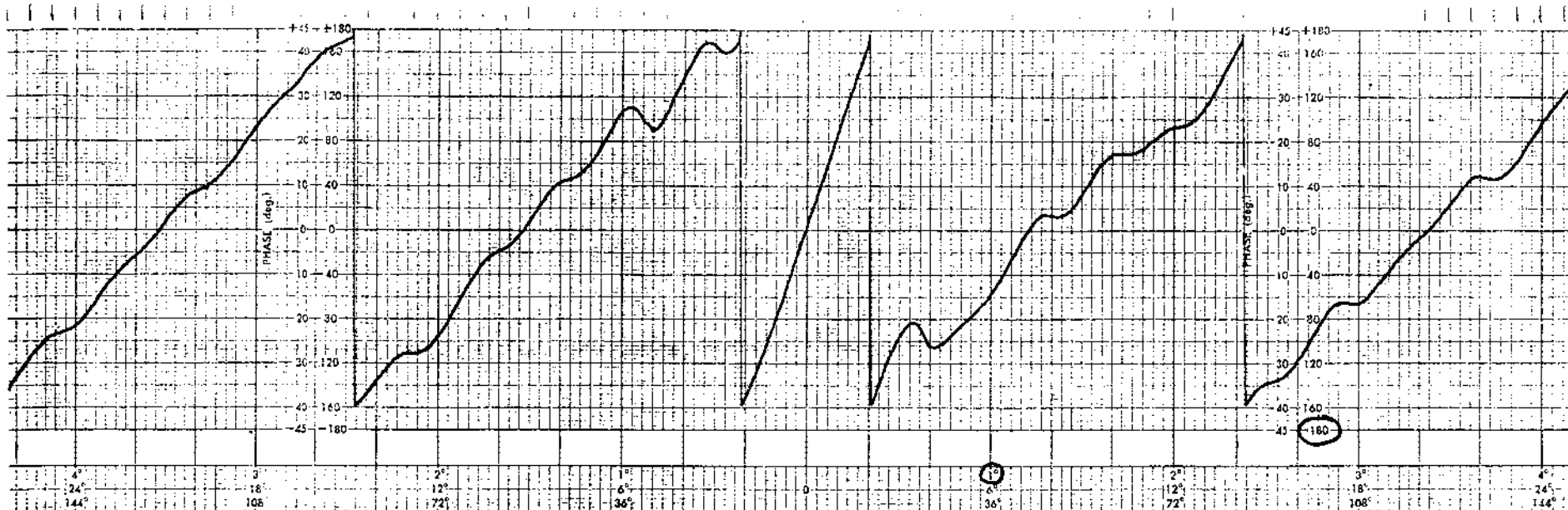


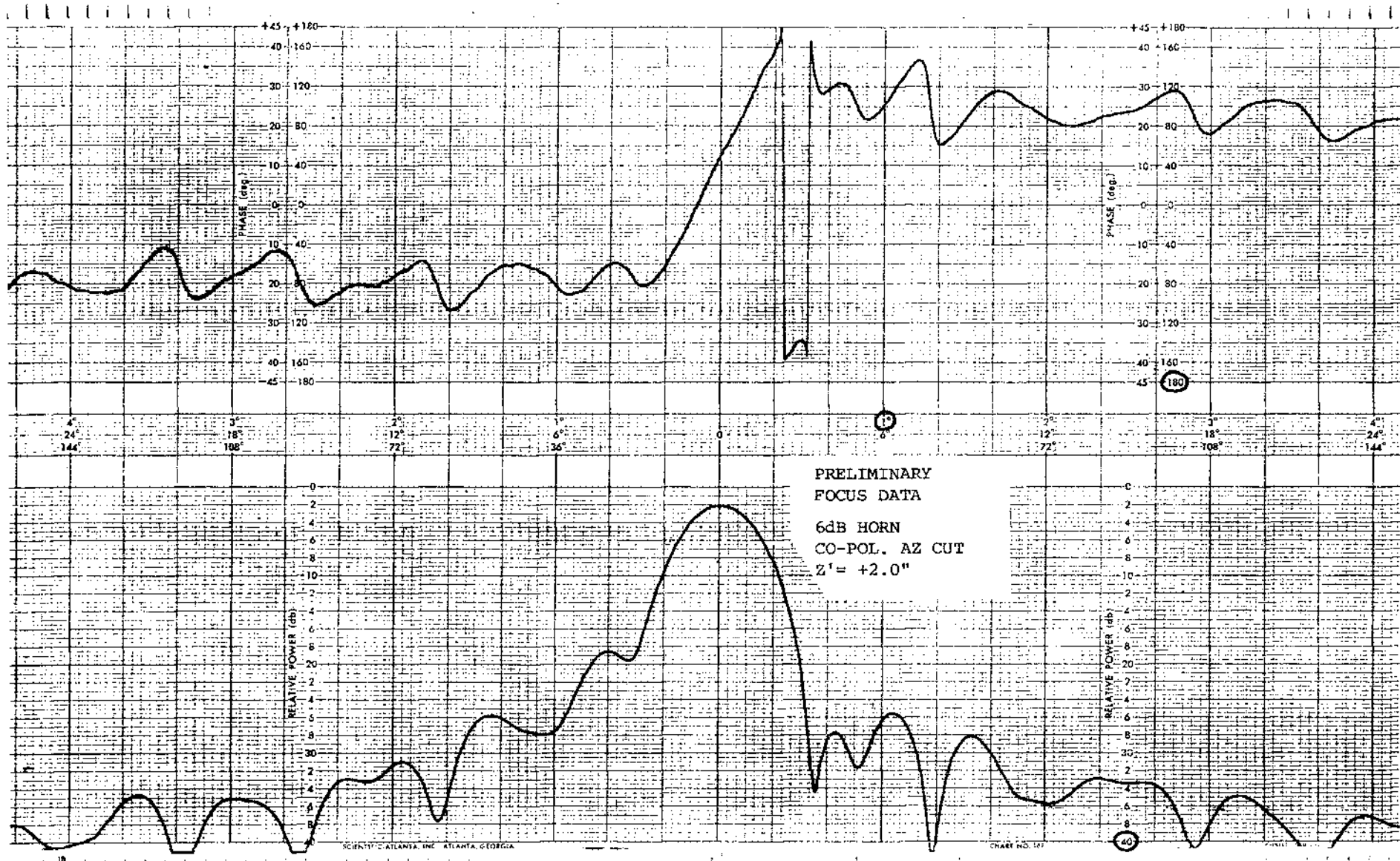


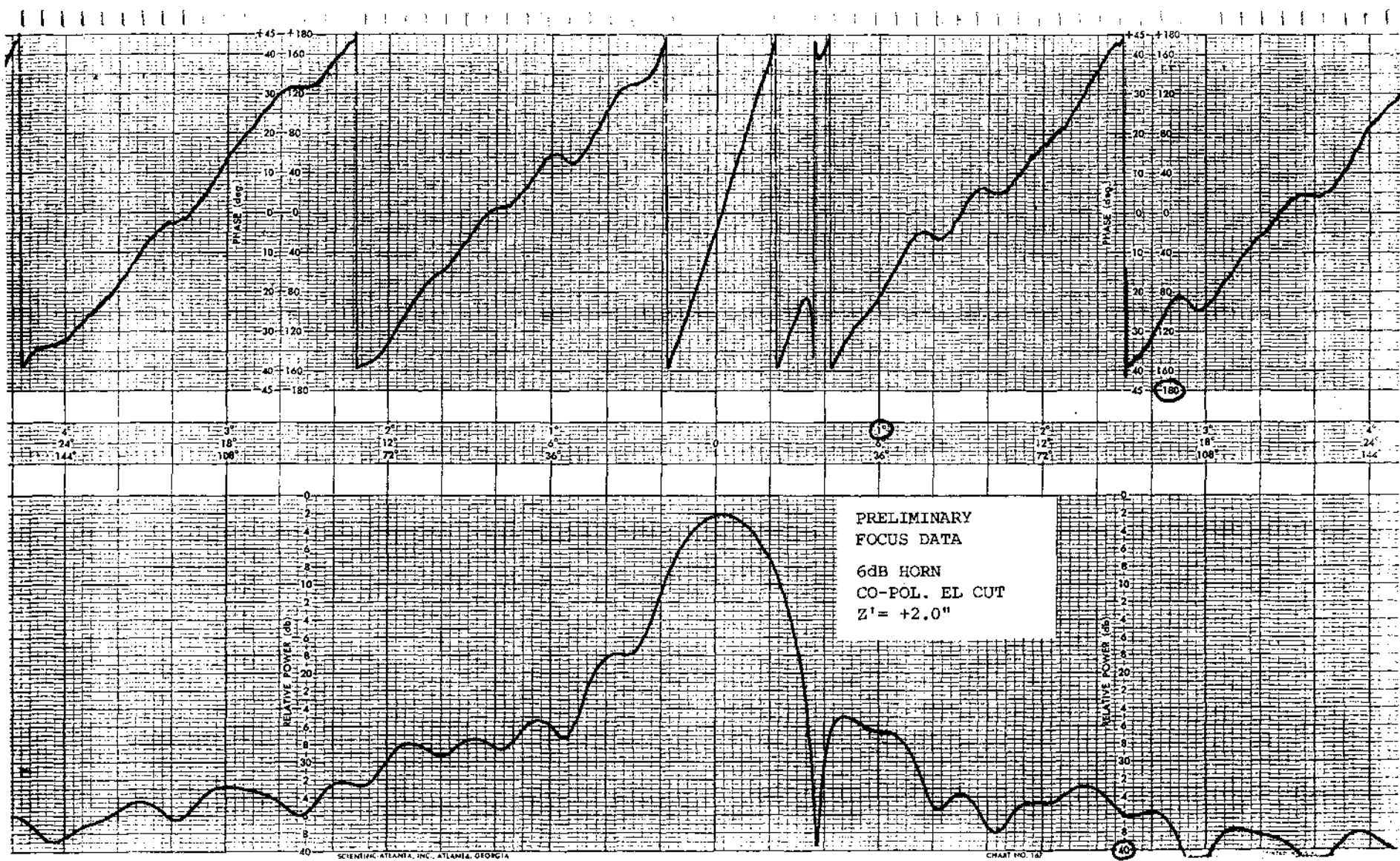


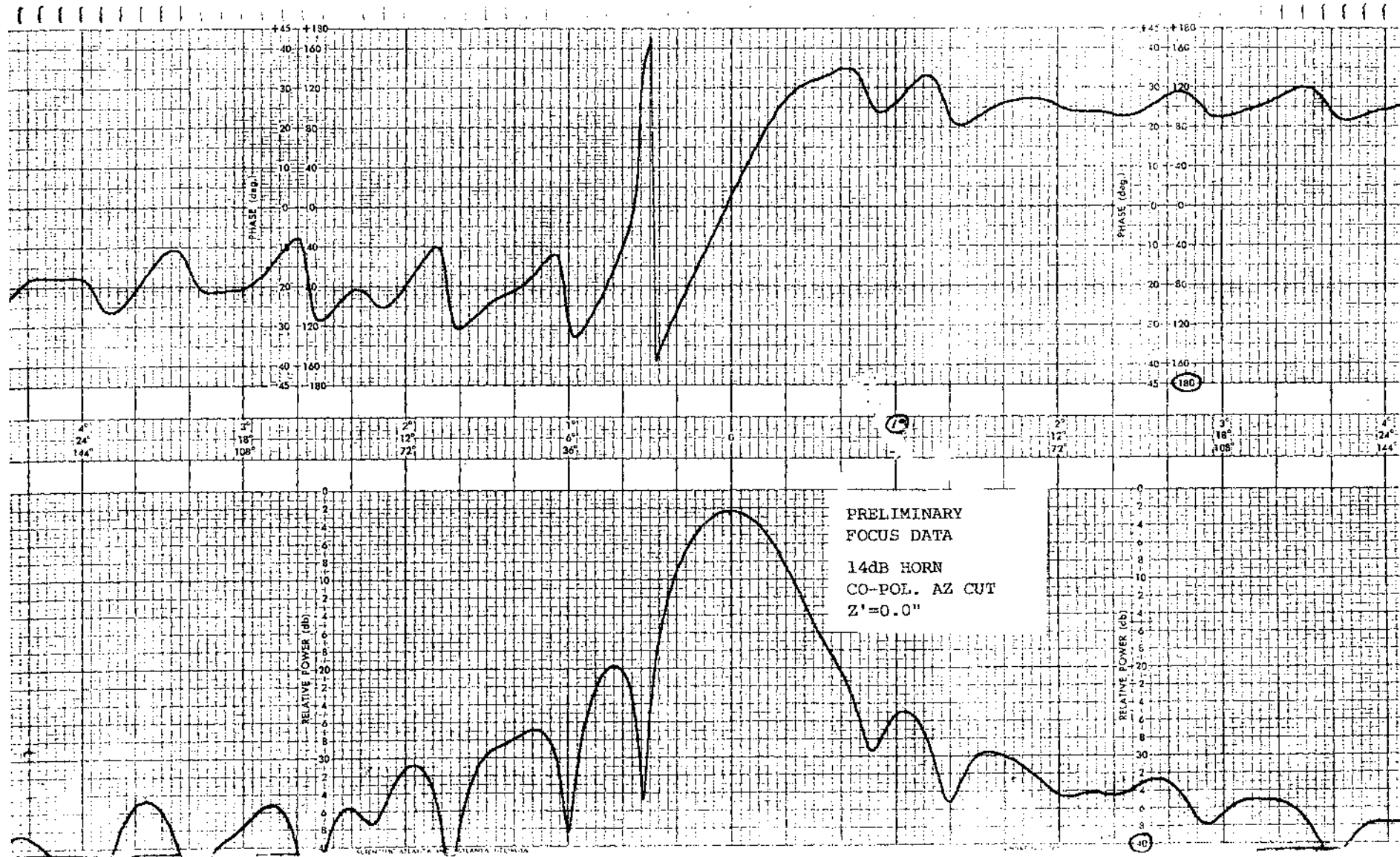


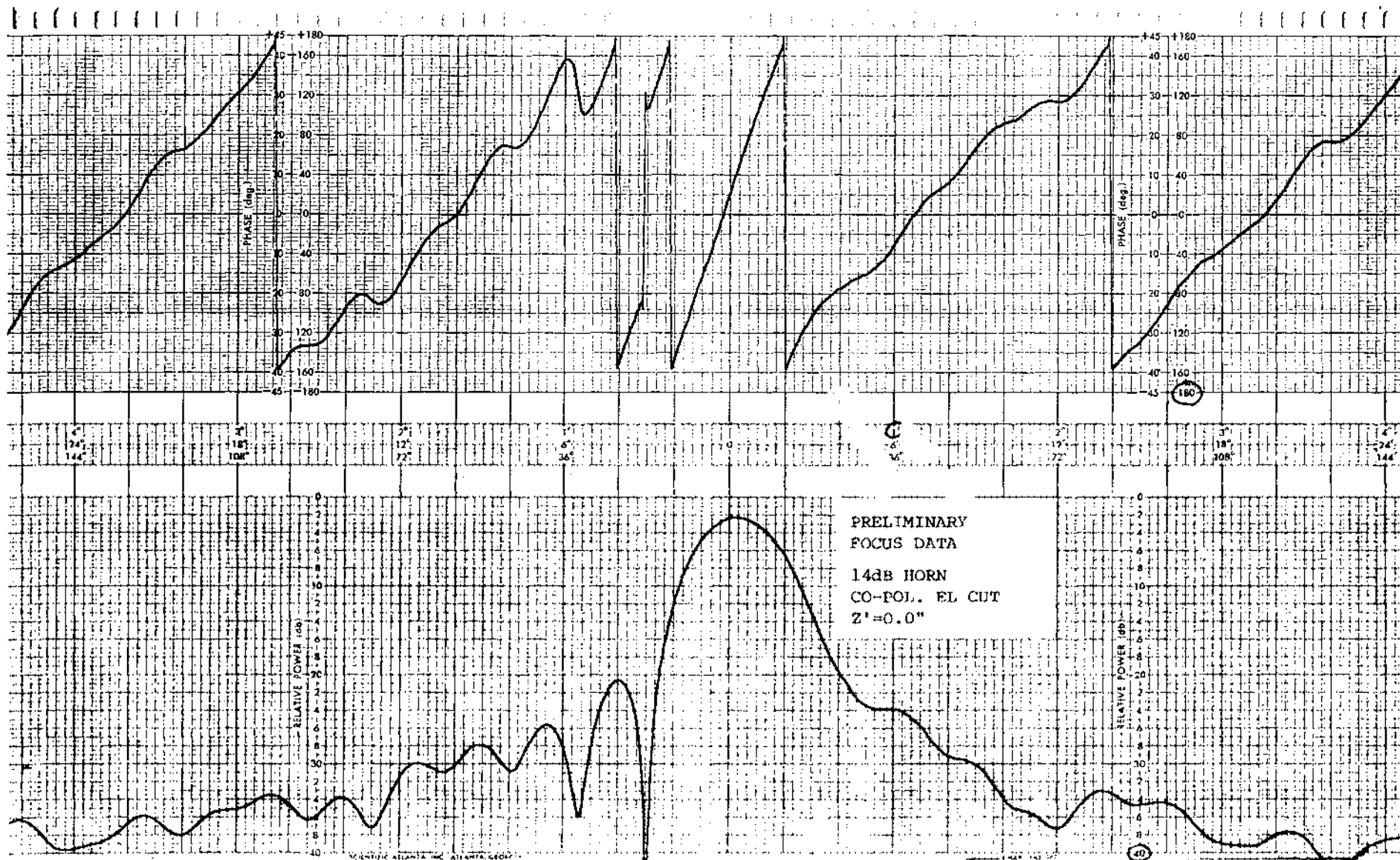






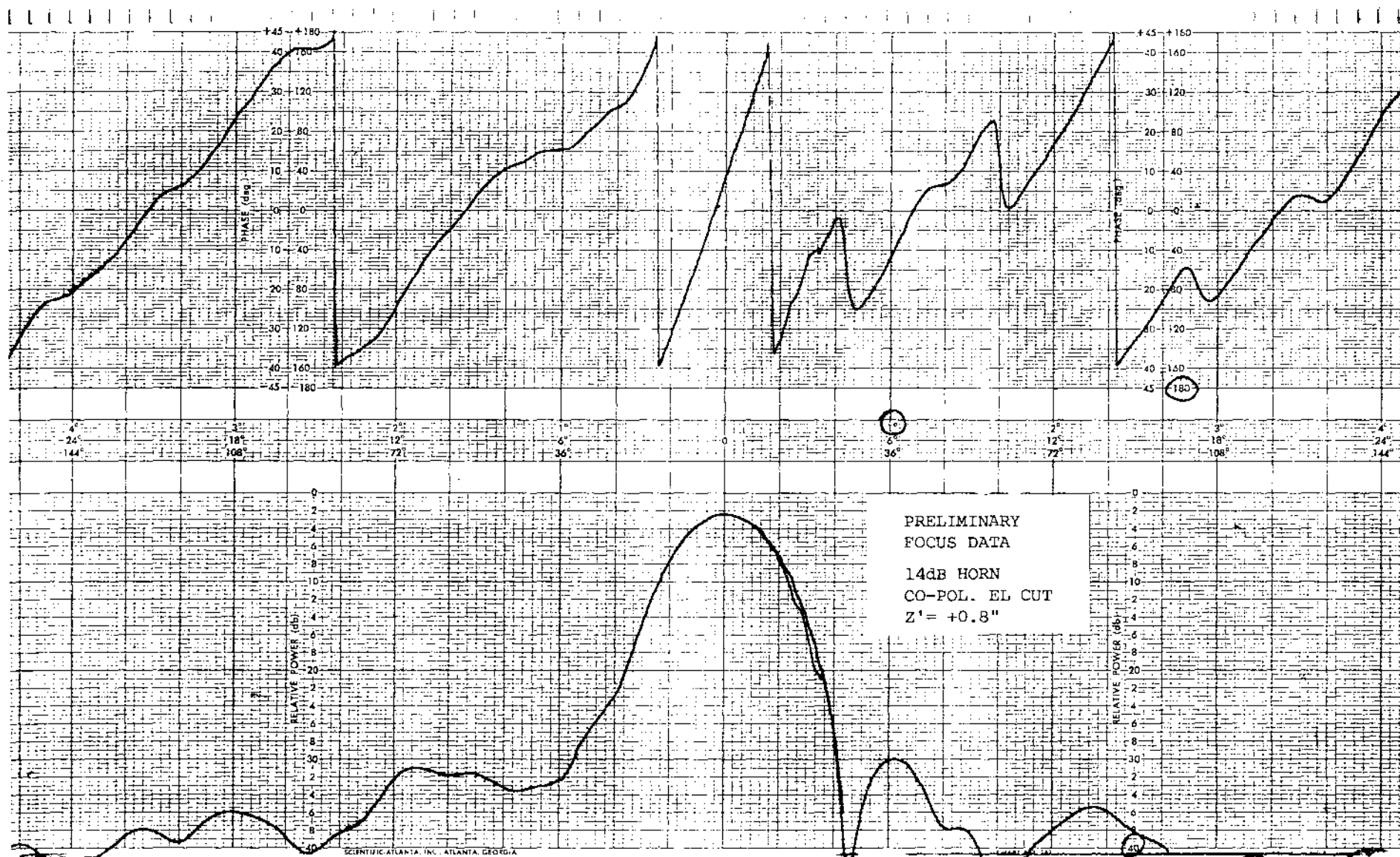


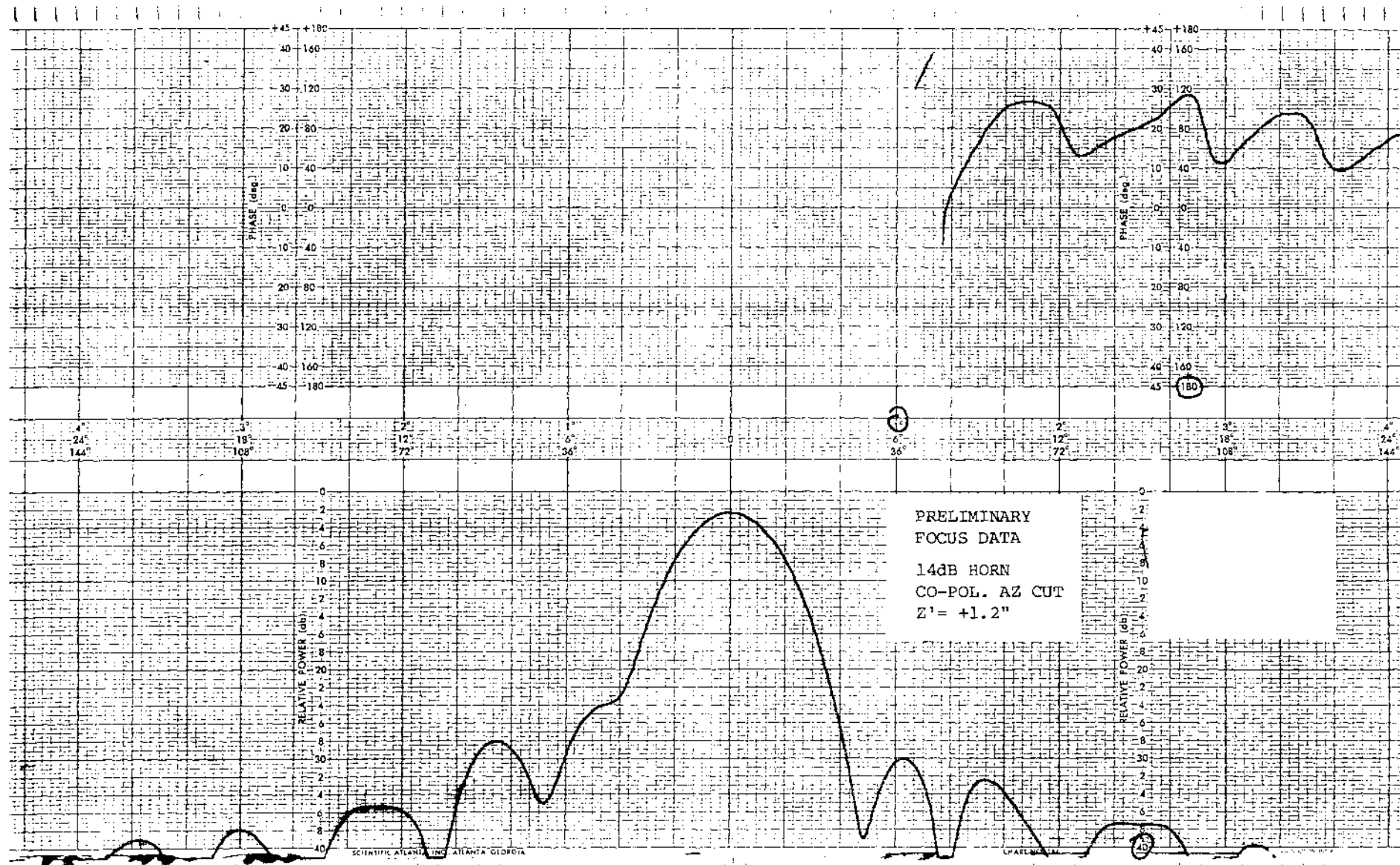




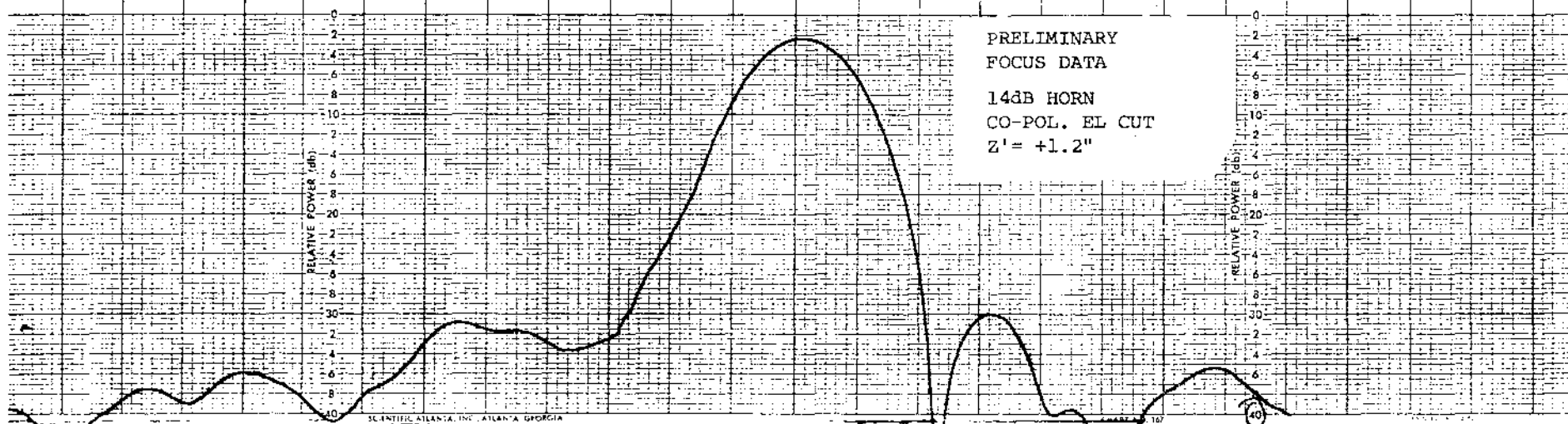
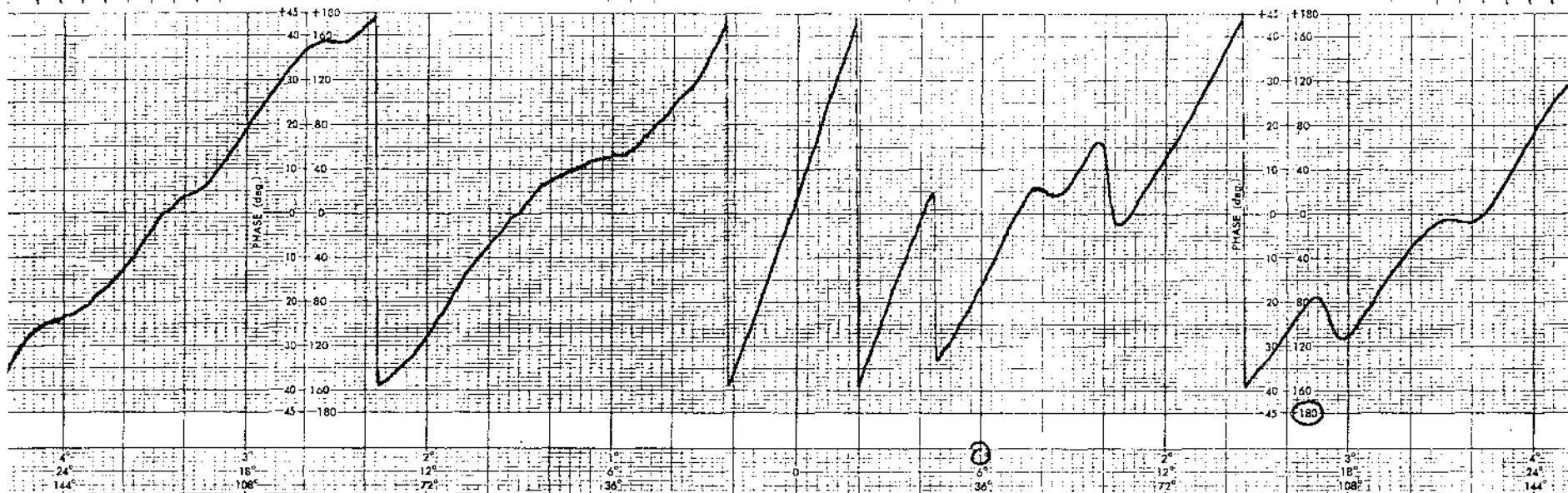


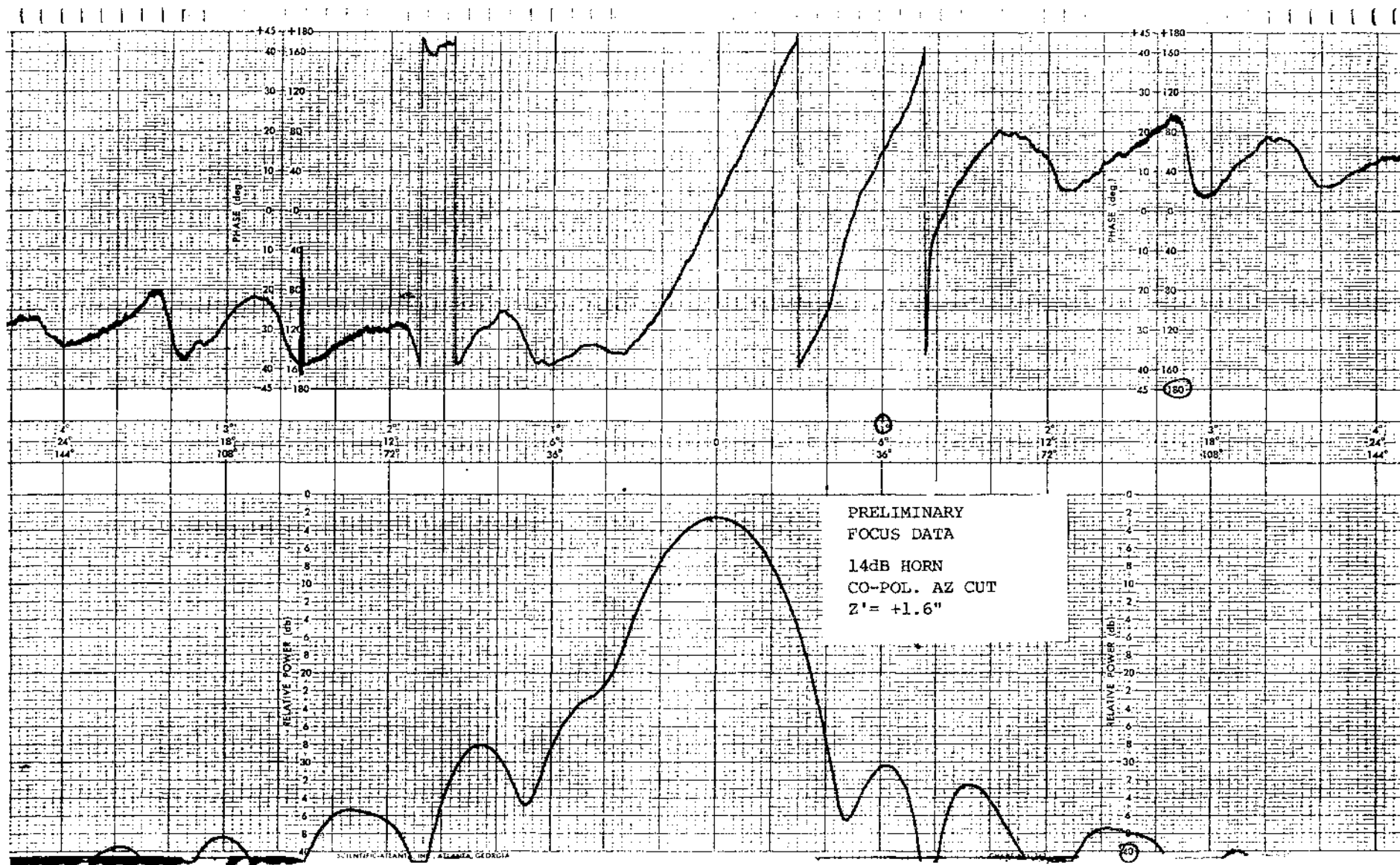


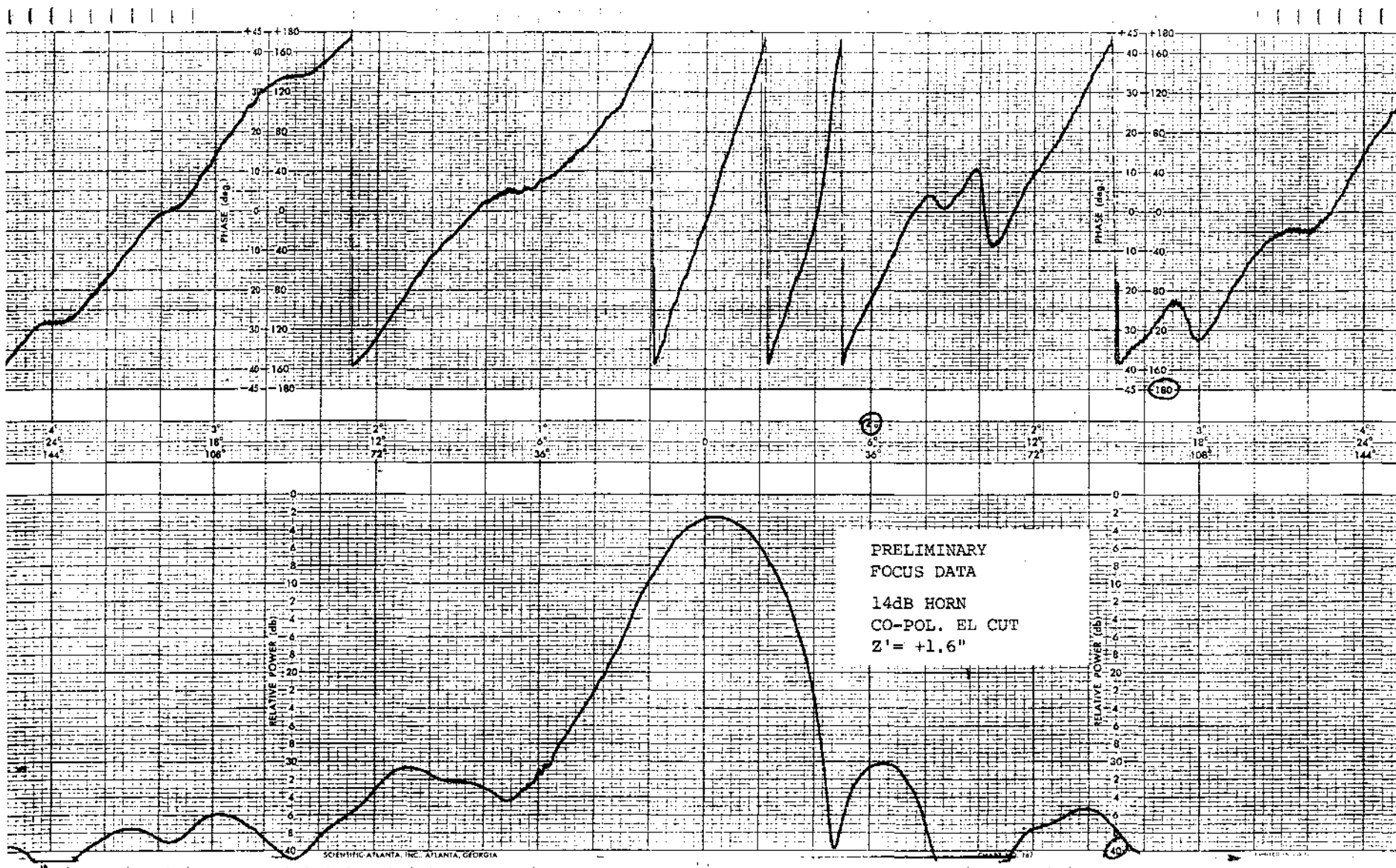


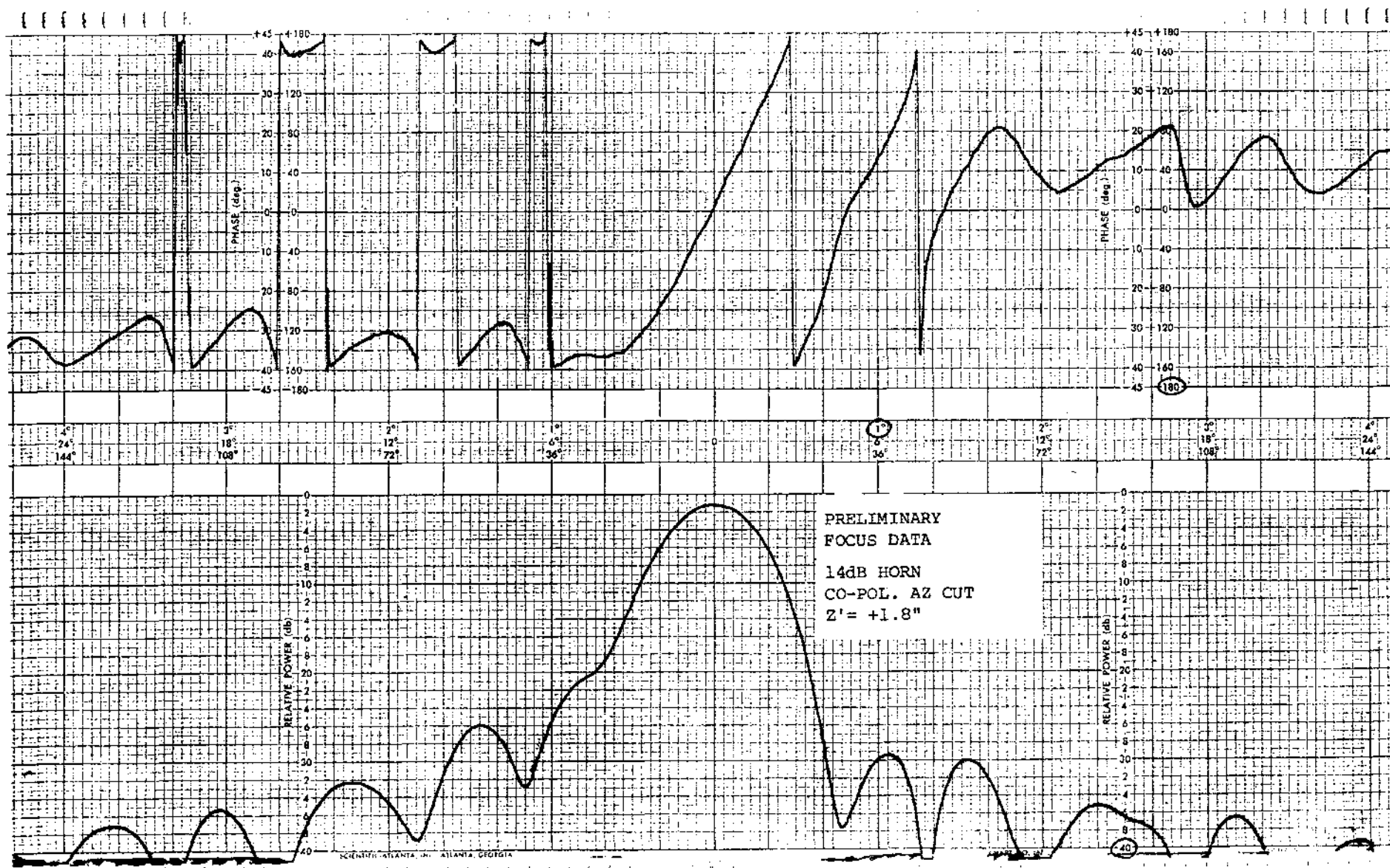


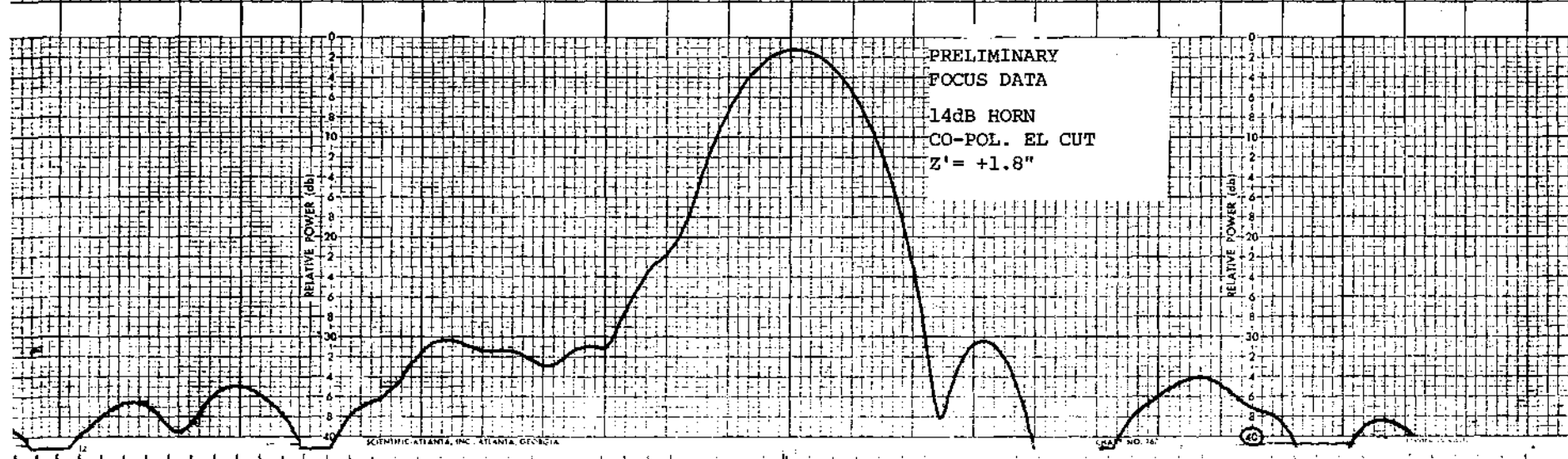


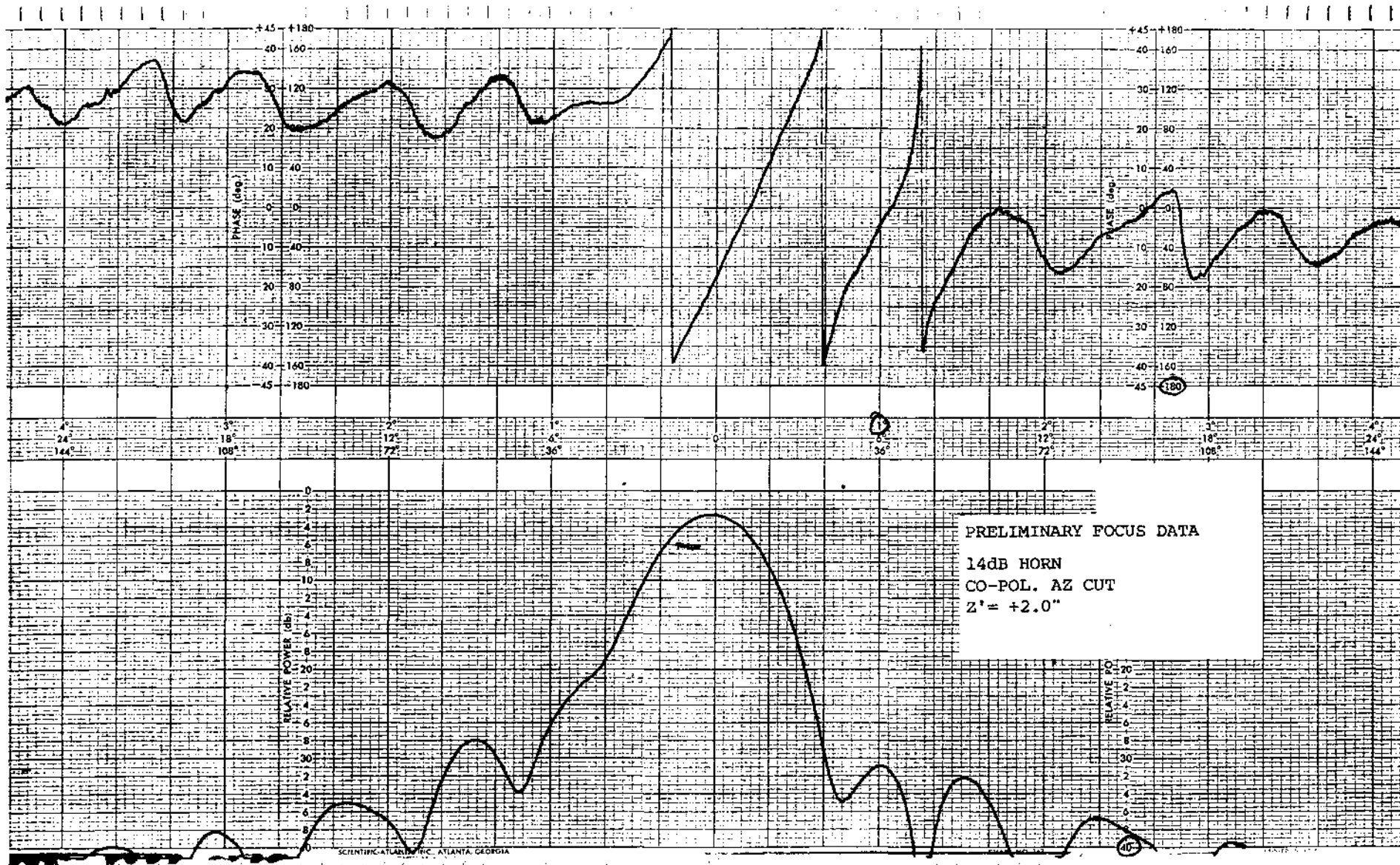




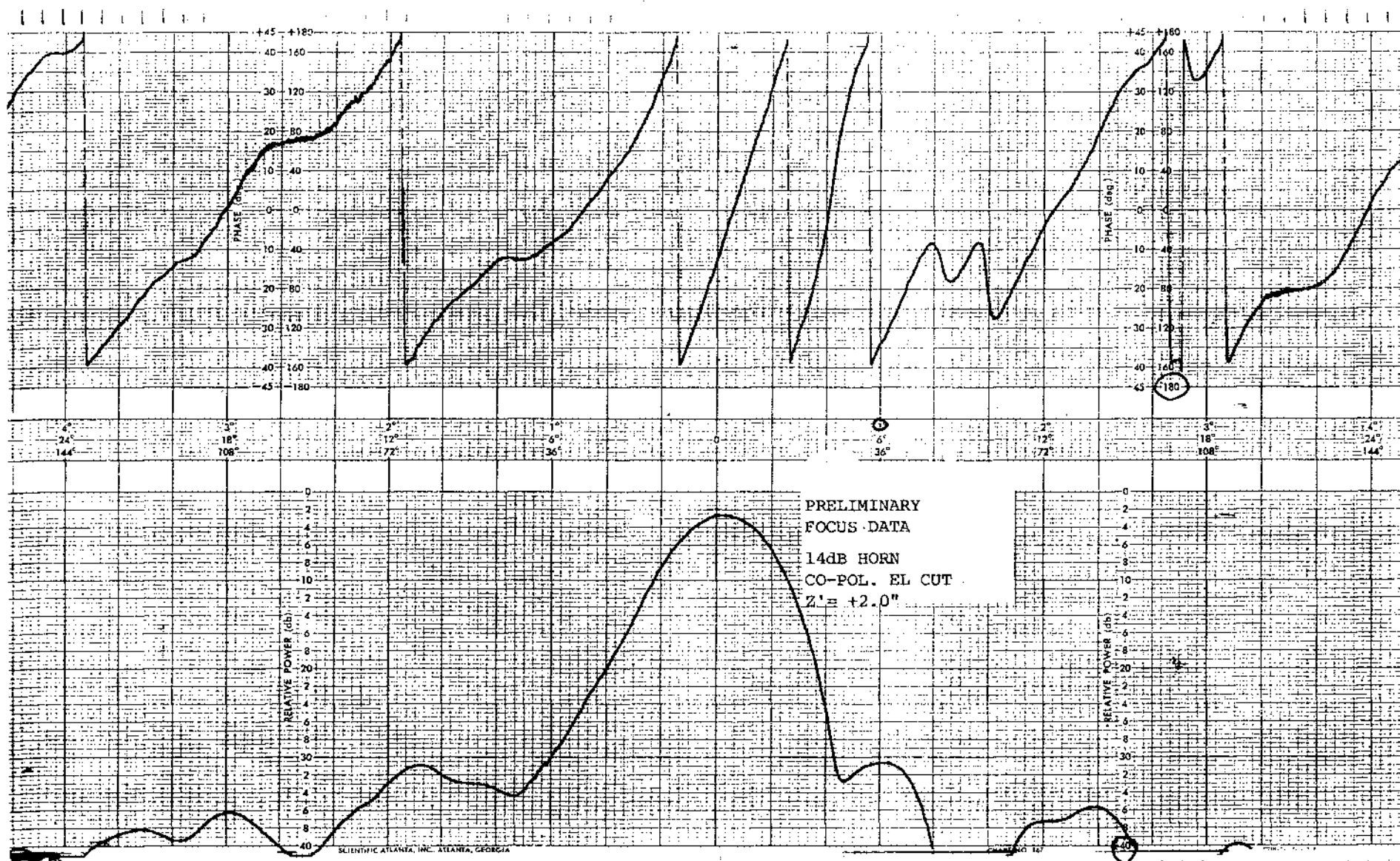








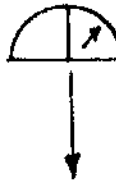









LSST - IIIRASTER SCAN LOG

<u>CONFIG.</u>	<u>HORN</u>	<u>SCAN</u>	<u>POL.</u>	<u>PK. GAIN</u>	<u>AZIMUTH</u>	<u>ELEVATION</u>	<u>FILE NAME</u>	<u>PAGE NO.</u>
	6 dB	0.0"	CO	50.75	$\pm 2^0$	$\pm 2^0$	RAST 07	59 - 61
	6 dB	0.0"	X	-	$\pm 2^0$	$\pm 2^0$	RAST 08	62 - 64
	6 dB	4.5"	CO	50.55	$\pm 2^0$	$\pm 2^0$	RAST 09	65 - 67
	6 dB	4.5"	X	-	$\pm 2^0$	$\pm 2^0$	RAST 10	68 - 70
	6 dB	0.0"	CO	50.75	$-6^0$ to $+2^0$	$\pm 2^0$	RAST 17	71 - 73
	6 dB	0.0"	X	-	$-6^0$ to $+2^0$	$\pm 2^0$	RAST 18	74 - 76
	6 dB	4.5"	CO	50.45	$-6^0$ to $+2^0$	$\pm 2^0$	RAST 15	77 - 79
	6 dB	4.5"	X	-	$-6^0$ to $+2^0$	$\pm 2^0$	RAST 16	80 - 82
	6 dB	0.0"	CO		$-6^0$ to $+2^0$	$\pm 2^0$	RAST 35	83 - 85
	14 dB	0.0"	CO	50.52	$\pm 2^0$	$\pm 2^0$	RAST 01	86 - 88
	14 dB	0.0"	X	-	$\pm 2^0$	$\pm 2^0$	RAST 02	89 - 91
	14 dB	4.5"	CO	50.35	$\pm 2^0$	$\pm 2^0$	RAST 05	92 - 94
	14 dB	4.5"	X	-	$\pm 2^0$	$\pm 2^0$	RAST 06	95 - 97
	14 dB	6.5"	CO	50.05	$\pm 2^0$	$\pm 2^0$	RAST 03	98 - 100
	14 dB	6.5"	X	-	$\pm 2^0$	$\pm 2^0$	RAST 04	101 - 103
	14 dB	0.0"	CO	50.39	$-6^0$ to $+2^0$	$\pm 2^0$	RAST 11	104 - 106
	14 dB	0.0"	X	-	$-6^0$ to $+2^0$	$\pm 2^0$	RAST 12	107 - 109
	14 dB	4.5"	CO	50.00	$-6^0$ to $+2^0$	$\pm 2^0$	RAST 13	110 - 112
	14 dB	4.5"	X	-	$-6^0$ to $+2^0$	$\pm 2^0$	RAST 14	113 - 115
	14 dB	0.0"	CO	50.55	$-6^0$ to $+2^0$	$\pm 2^0$	RAST 36	116 - 118



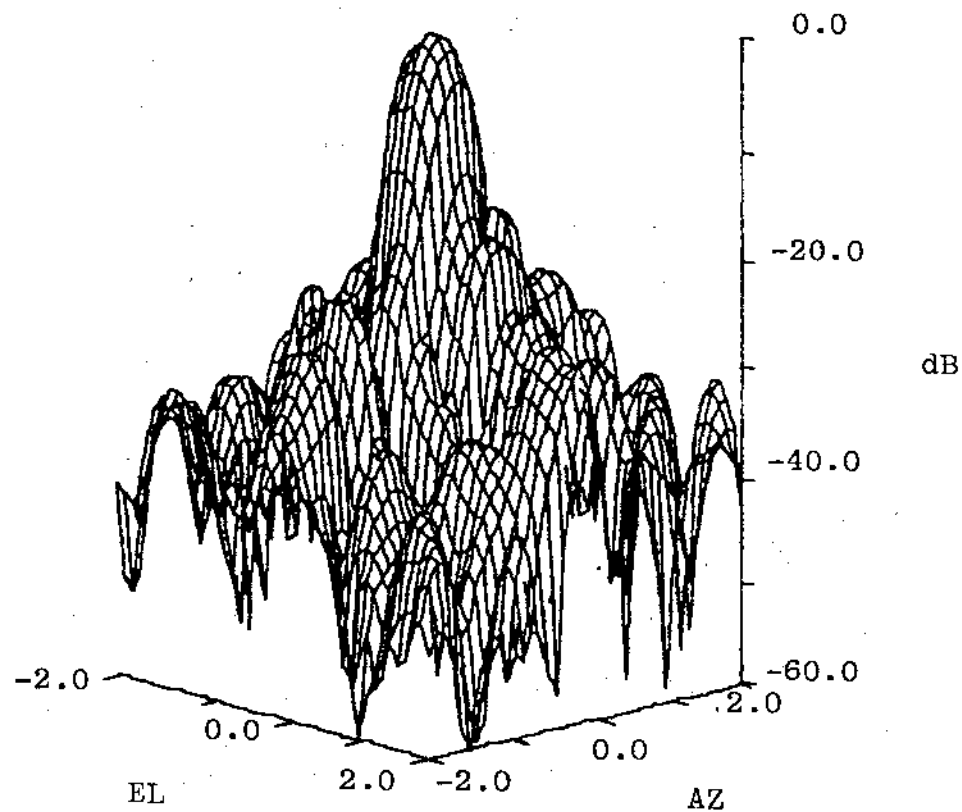
YHIGH\* -1.9000  
YLOW\* -71.3000  
CEILING\* 0.0000  
FLOOR\* -60.0000



6 dB HORN

Scan: 0.0"

Co-Pol RASTER 07



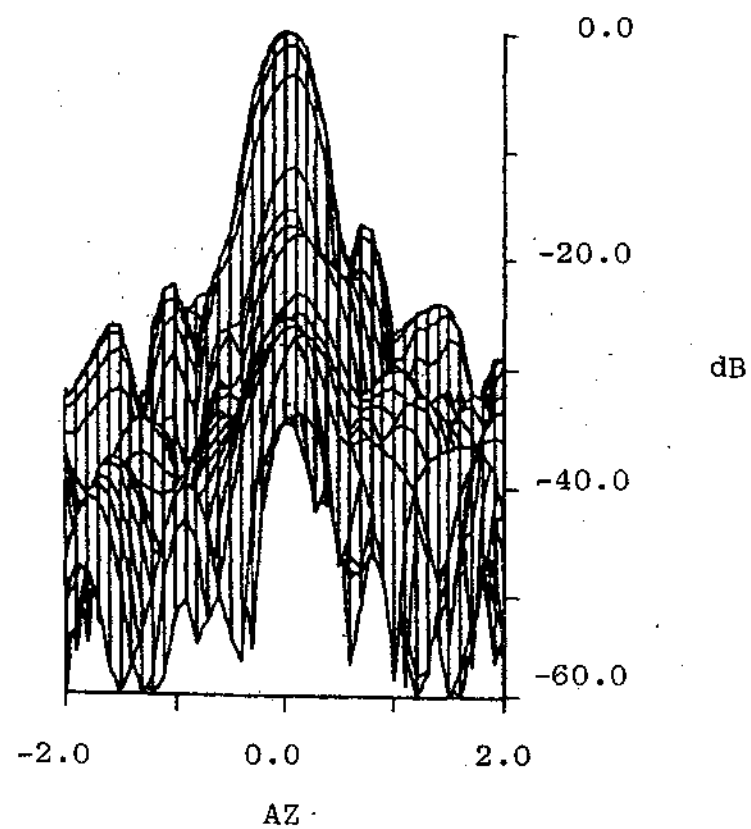
VHIGH= -1.9000  
VLOW= -71.3000  
CEILING= 0.0000  
FLOOR= -60.0000



6 dB HORN

Scan: 0.0"

Co-Pol RASTER 07

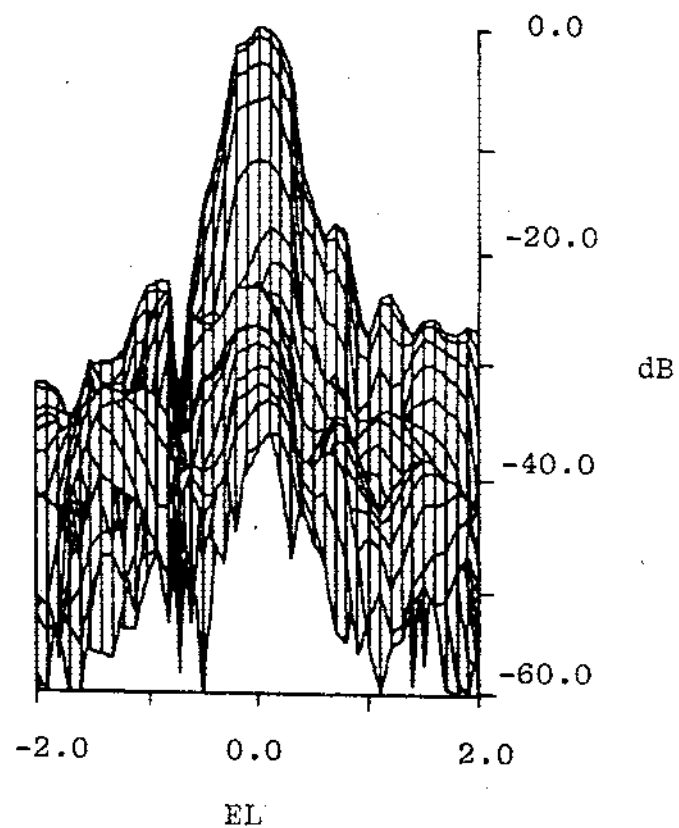


YHIGH= -1.9000  
YLOW= -71.3000  
CEILING= 8.0000  
FLOOR= -60.0000



6 dB HORN  
Scan: 0.0"

Co-Pol RASTER 07



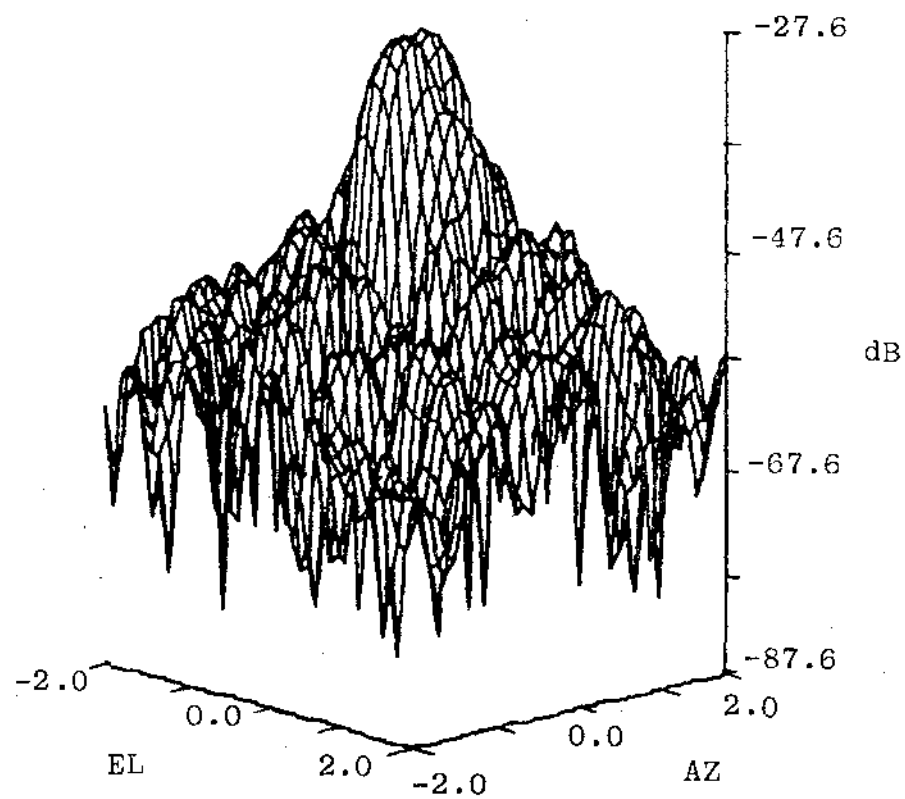
VHIGH--29.5000  
YLOW--82.9000  
CEILING--20.0000  
FLOOR--30.0000



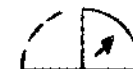
6 dB · HORN

Scan: 0.0°

X-Pol RASTER 08



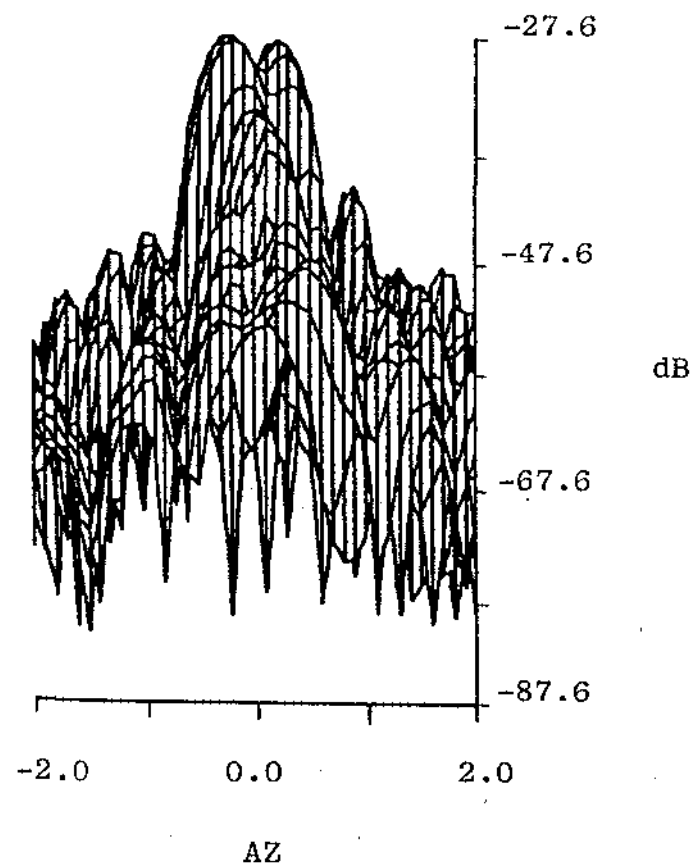
YHIGH--29.5000  
YLOW--52.9000  
CEILING--20.0000  
FLOOR--80.0000



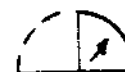
6 dB HORN

Scan: 0.0"

X-Pol RASTER 08



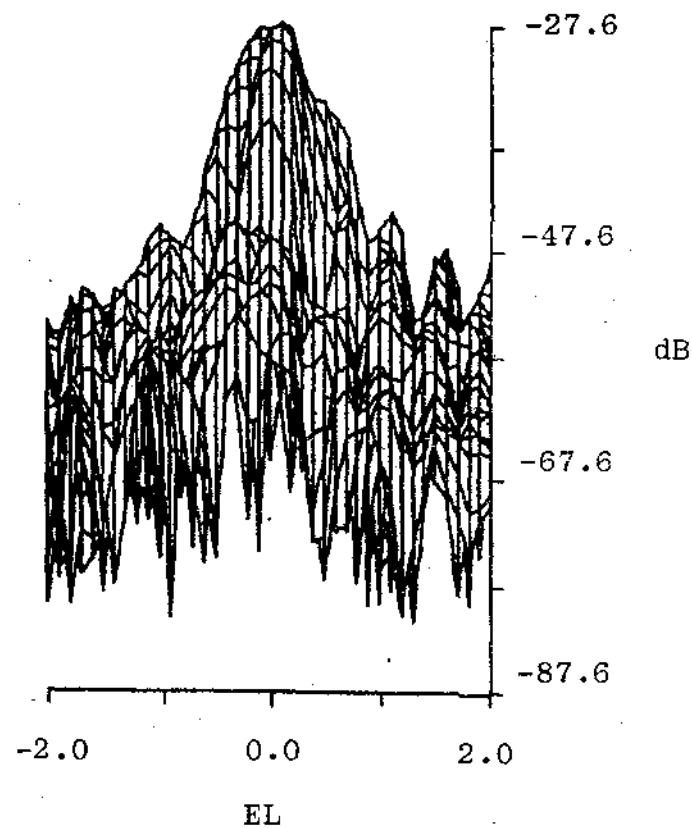
YHIGH--29.5000  
YLOW--82.9000  
CEILING--20.0000  
FLOOR--80.0000



6 dB HORN

Scan: 0.0"

X-Pol RASTER 08



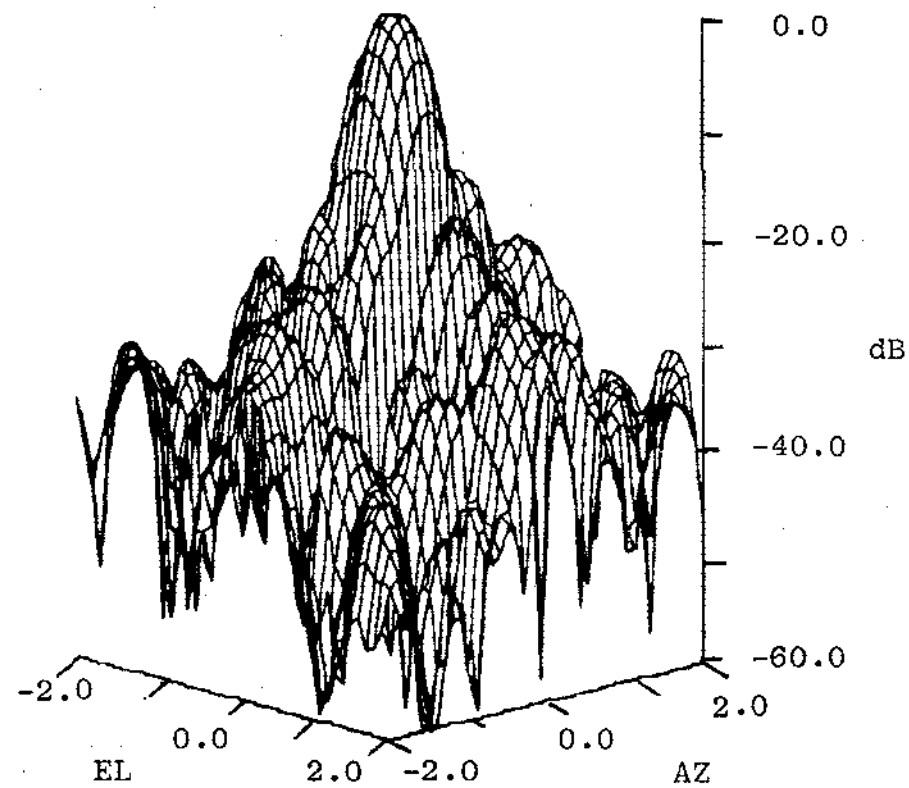
YHIGH= -3.4000  
YLOW= -78.3000  
CEILING= 0.0000  
FLOOR= -60.0000



6 dB HORN

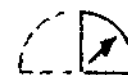
SCAN: 4.5"

Co-Pol. RASTER 00





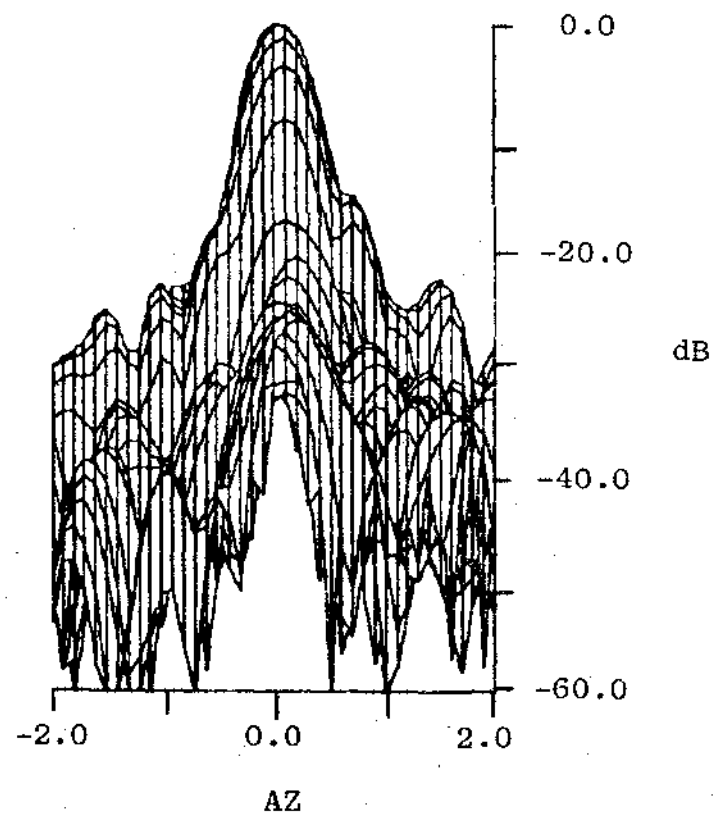
YNIGH\* -3.4000  
YLOW\* -78.3000  
CEILING\* 0.0000  
FLOOR\* -60.0000



6 dB HORN

SCAN: 4.5"

Co-Pol. RASTER 09



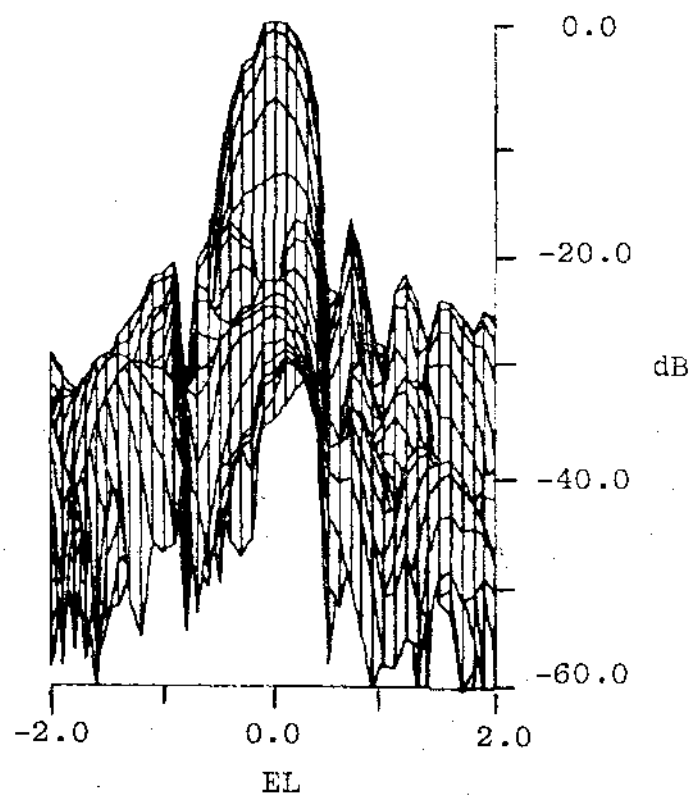
WITCH\* -7.4000  
WLOW\* -75.3000  
CEILING\* 0.0000  
FLOOR\* -60.0000



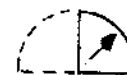
6 dB HORN

SCAN: 4.5"

Co-Pol. RASTER 09



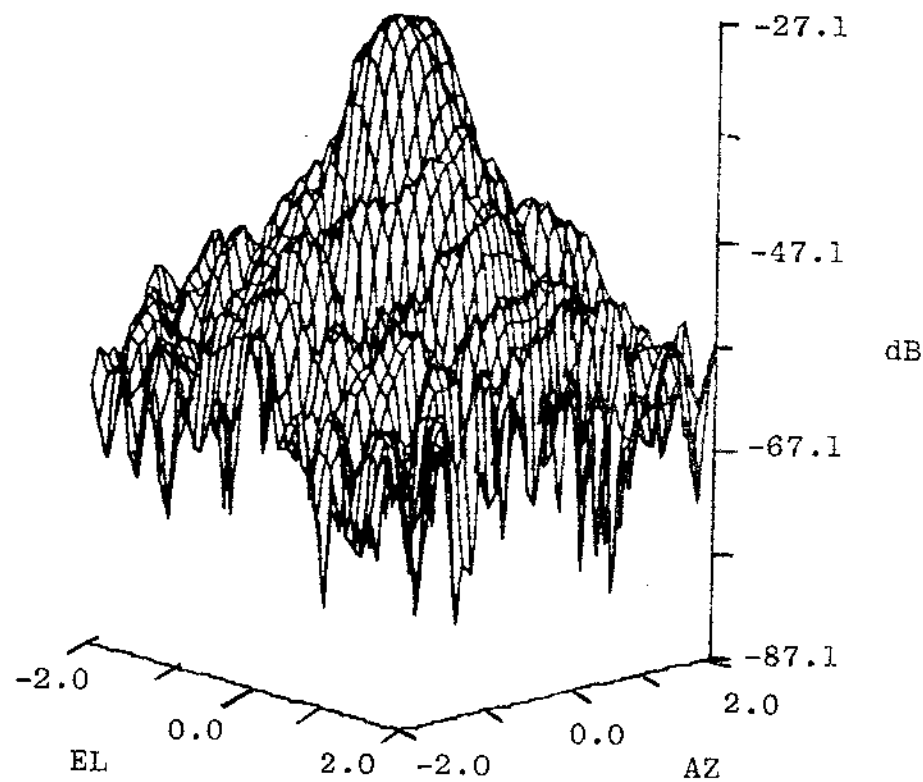
VHIGH=-30.5000  
VLOW=-84.5000  
CEILING=-20.0000  
FLOOR=-80.0000



6 dB HORN

SCAN: 4.5"

X-Pol. RASTER 10



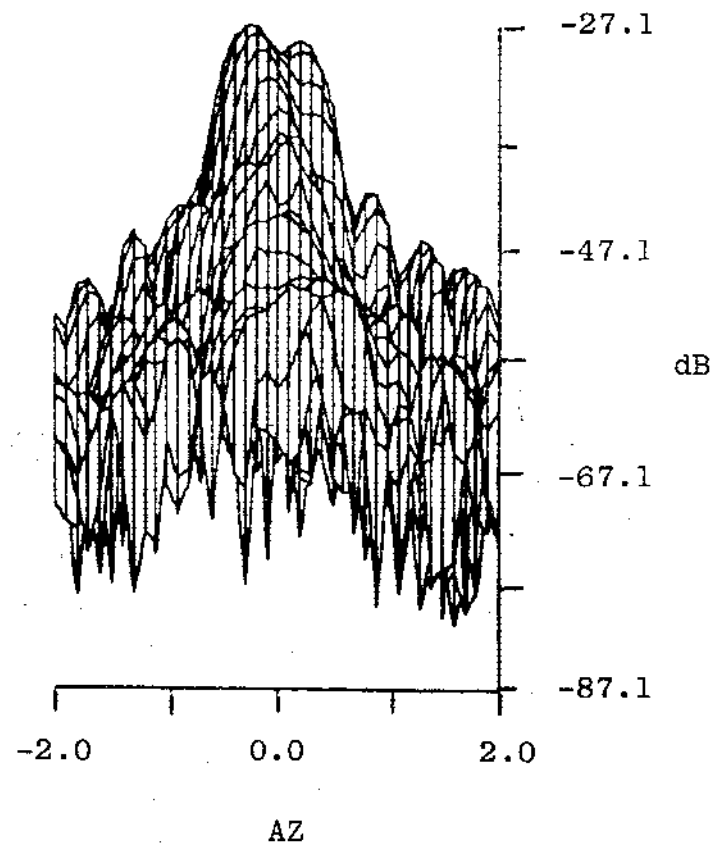
YHIGH=-30.5000  
YLOW=-84.5000  
CEILING=-20.0000  
FLOOR=-80.0000



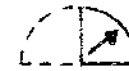
6 dB HORN

SCAN: 4.5"

X-Pol. RASTER 10



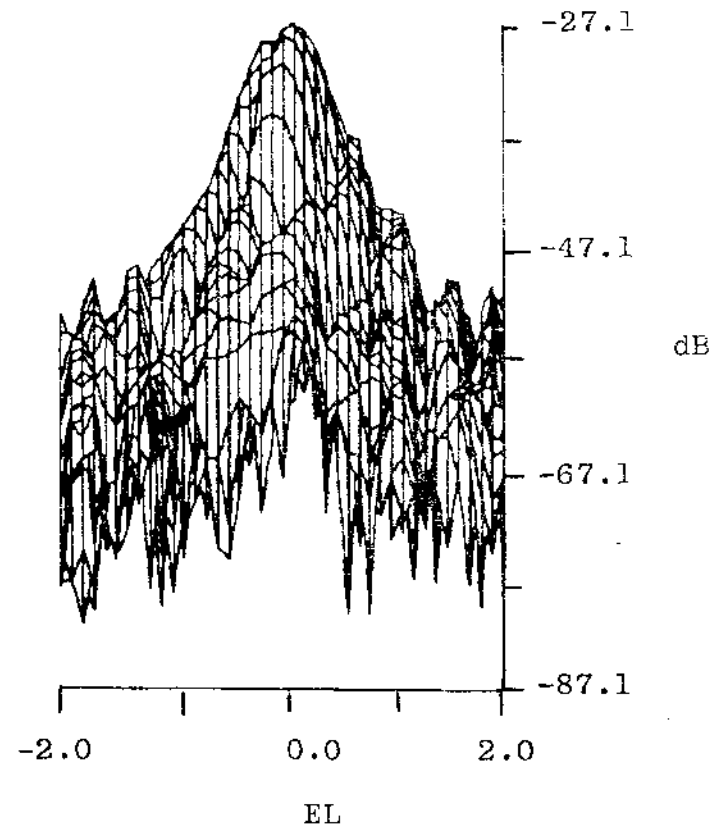
YHIGH=-38.5000  
YLOW=-84.5000  
CEILING=-20.0000  
FLOOR=-80.0000



6 dB HORN

SCAN: 4.5"

X-Pol. RASTER 10



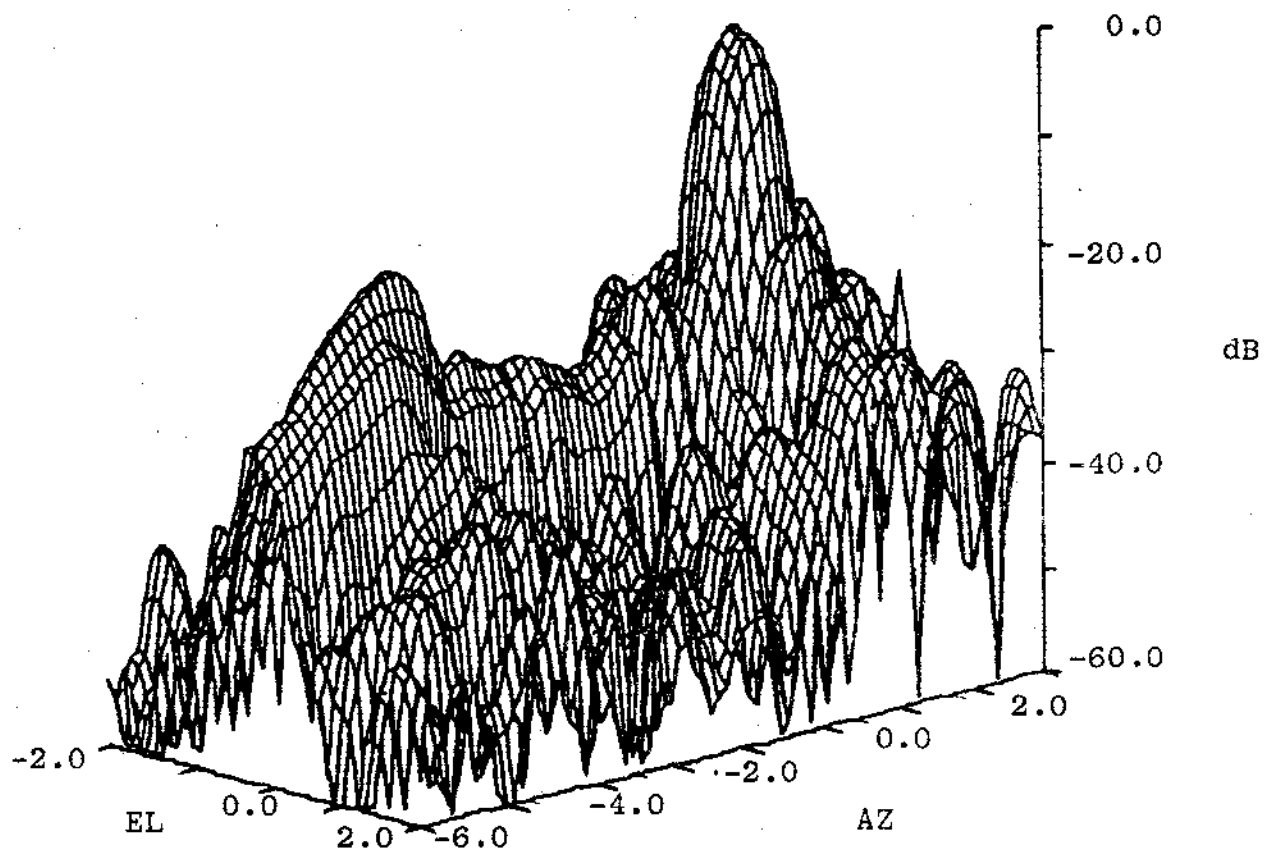
YHIGH- -3.1000  
YLOW- -53.3000  
CEILING- 0.0000  
FLOOR- -60.0000



6 dB HORN

Scan: 0.0"

Co-Pol RASTER 17

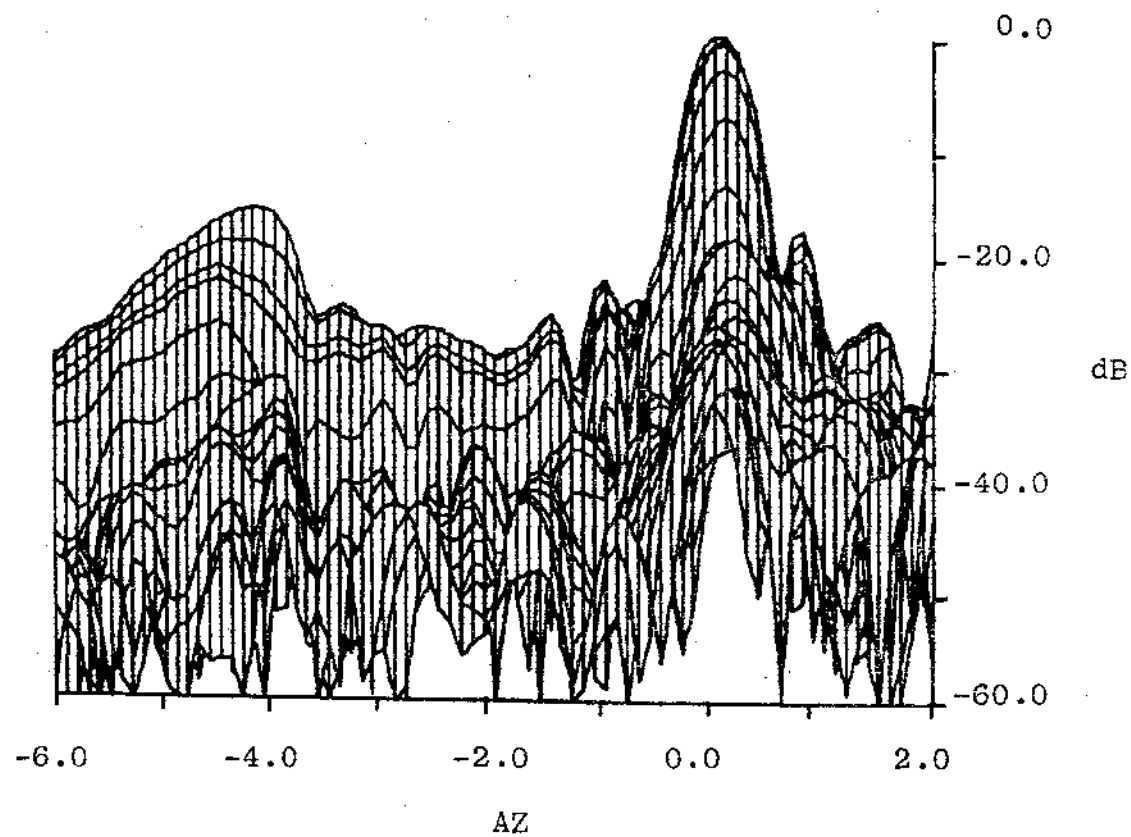


WHICH\* -3.1000  
YLOW\* -83.3000  
CEILING\* 0.0000  
FLOOR\* -60.0000



6 dB HORN  
Scan: 0.0"

Co-Pol RASTER 17





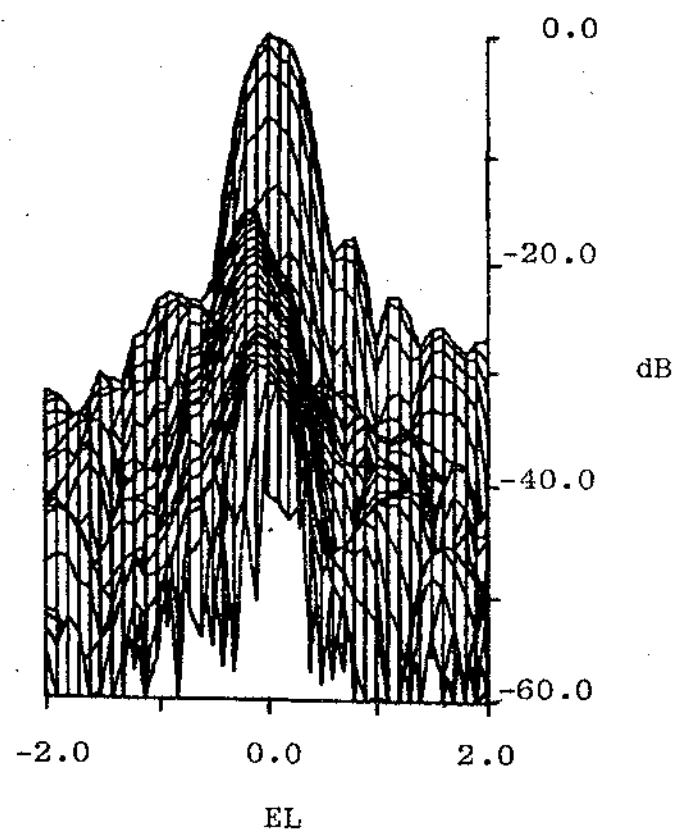
YHIGH\* -3.1000  
YLOW\* -83.3000  
CEILING\* 0.0000  
FLOOR\* -60.0000



6 dB HORN

Scan: 0.0"

Co-Pol RASTER 17



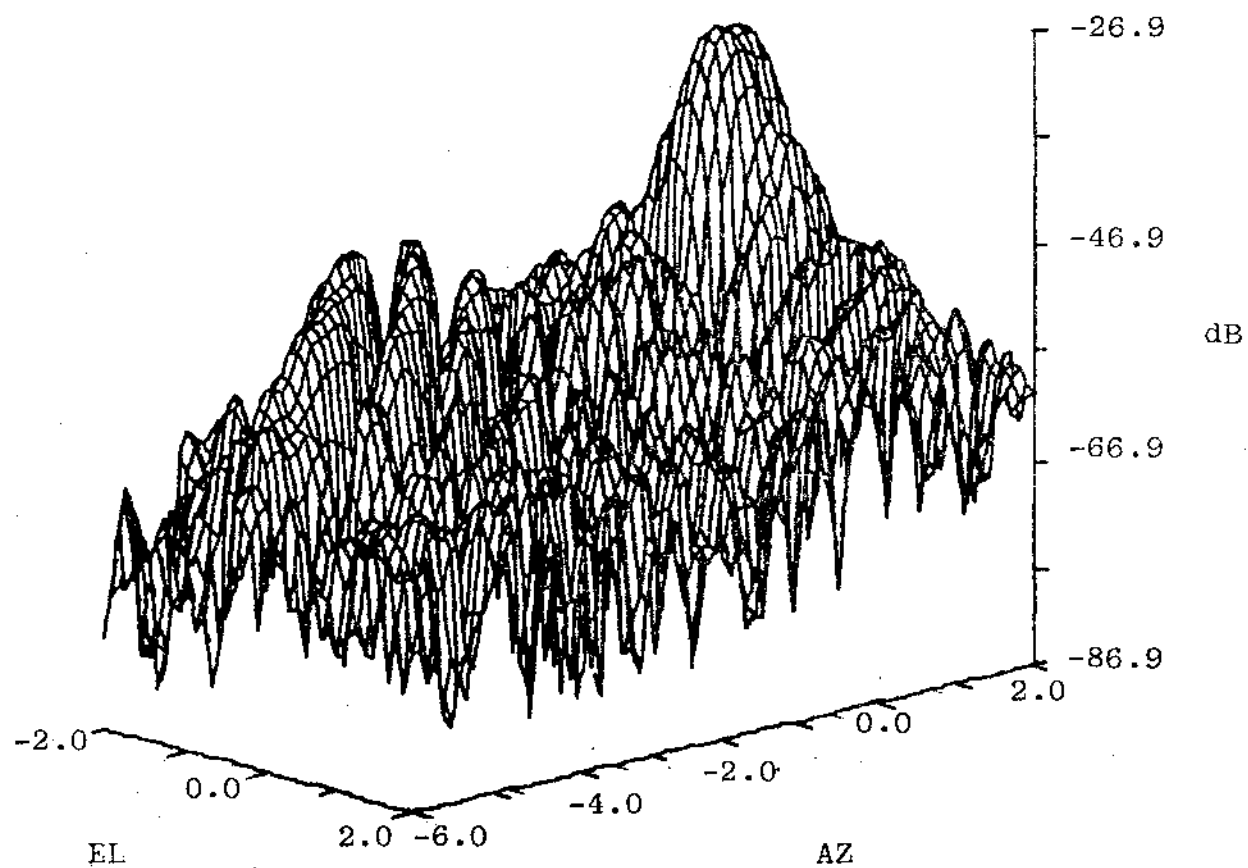
VHIGH--38.0000  
YLOW--86.2000  
CEILING--20.0000  
FLOOR--80.0000



6 dB HORN

Scan: 0.0"

X-Pol RASTER 18



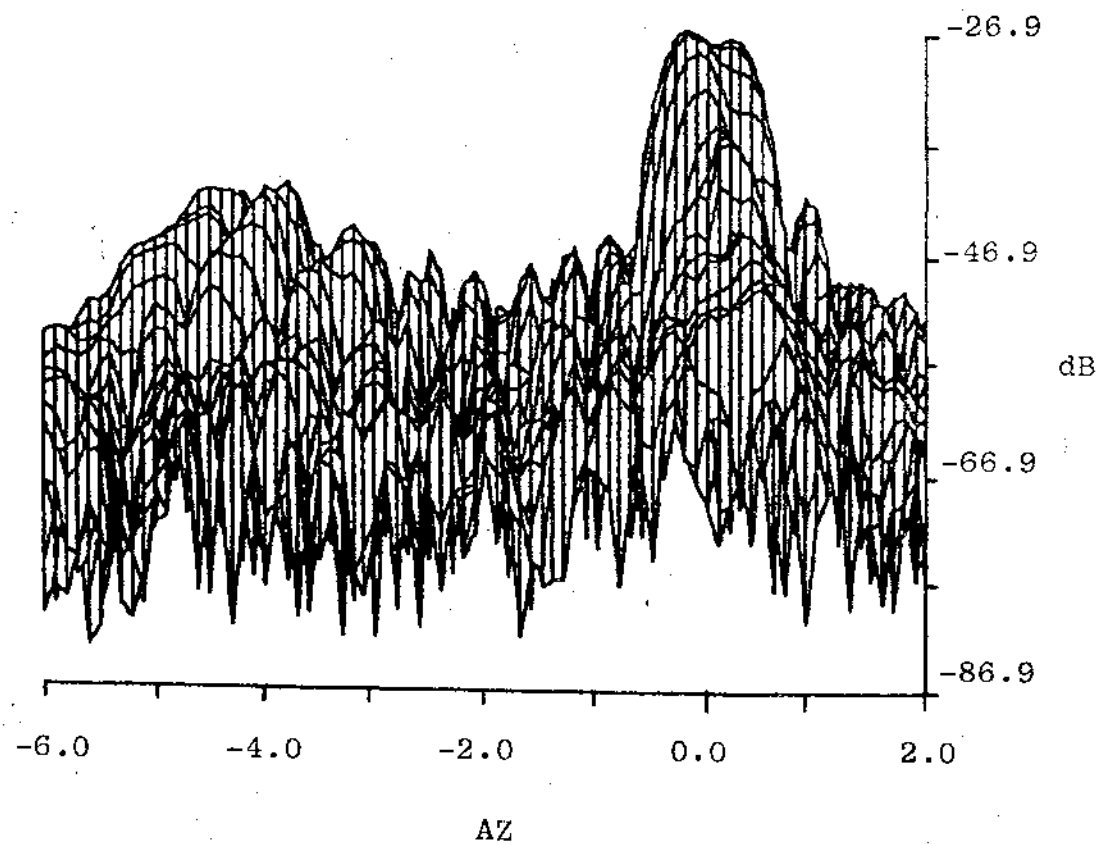
YHIGH--30.0000  
YLOW--86.2000  
CEILING--20.0000  
FLOOR--90.0000



6 dB HORN

Scan: 0.0"

X-Pol RASTER 18



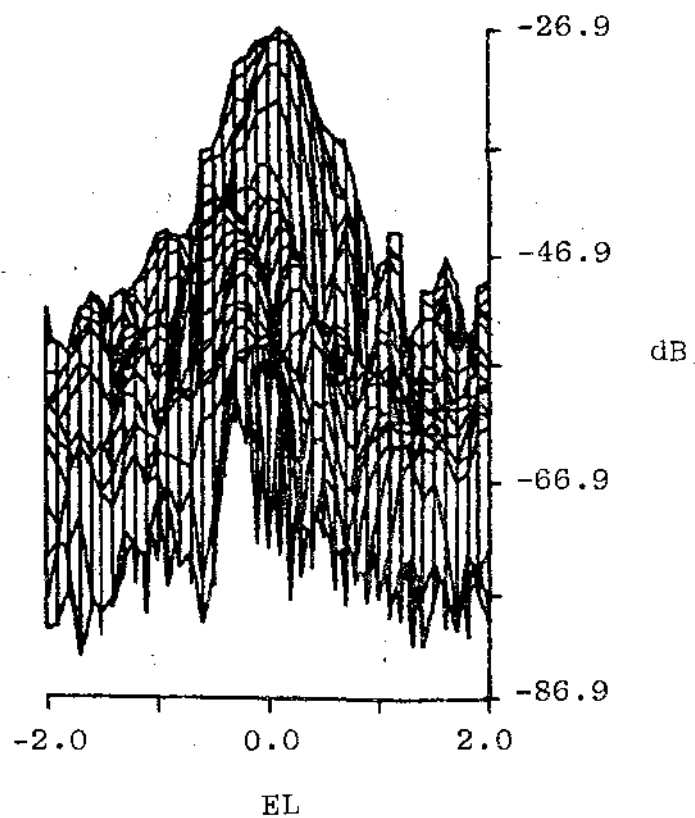
YHIGH--30.0000  
YLOW--86.2000  
CEILING--20.0000  
FLOOR--80.0000



6 dB HORN

Scan: 0.0"

X-Pol RASTER 18



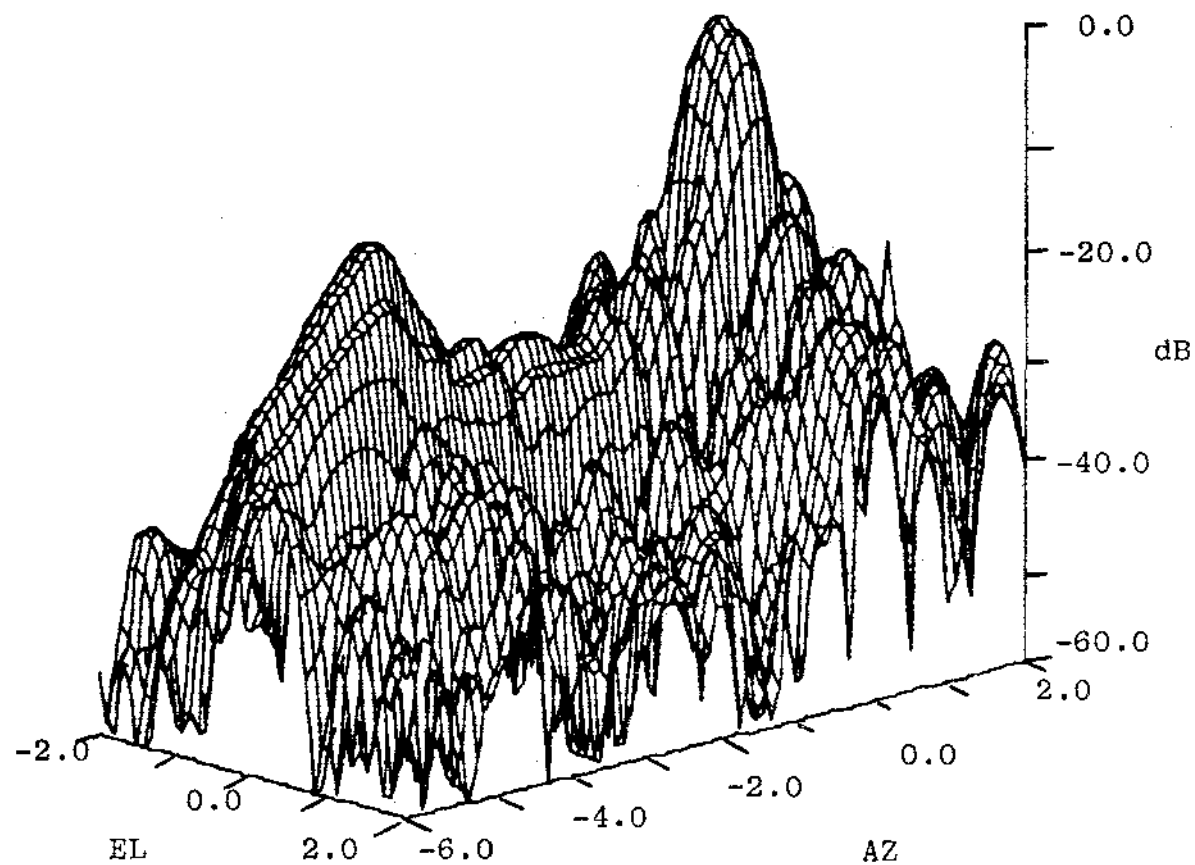
VHIGH- -3.5000  
VLOW- -79.4000  
CEILING- 2.0000  
FLOOR- -50.0000



6 dB HORN

SCAN: 4.5"

Co-Pol. RASTER 15



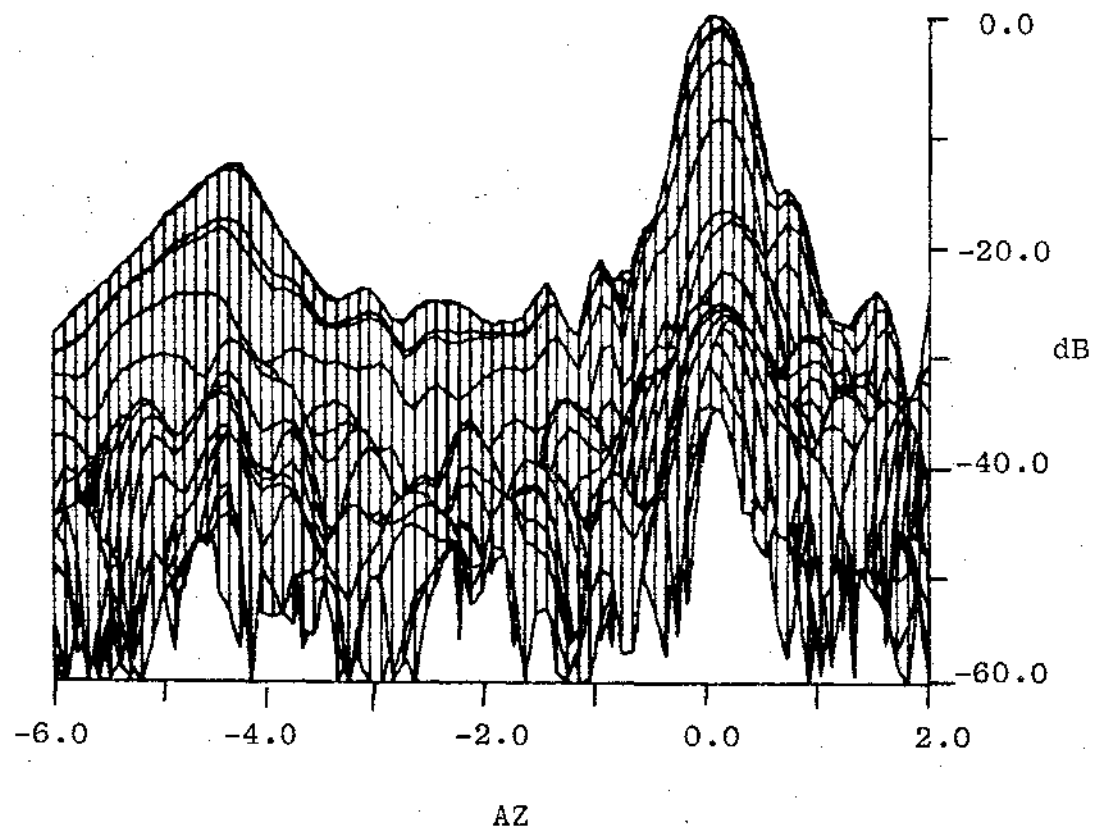
YHIGH= -3.5000  
YLOW= -79.4000  
CEILING= 0.0000  
FLOOR= -60.0000



6 dB HORN

SCAN: 4.5"

Co-Pol. RASTER 15



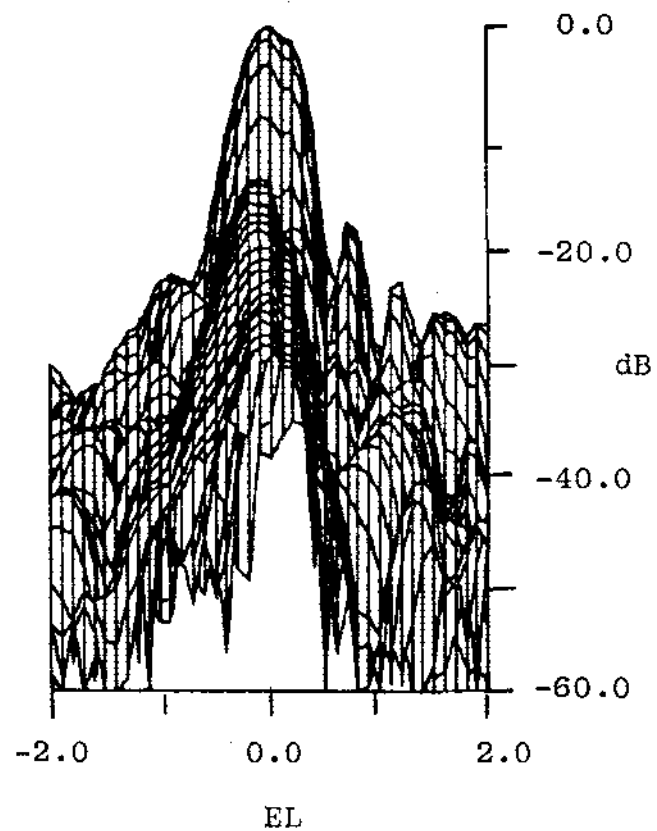
VHIGH= -3.5000  
VLOW= -79.4000  
CEILING= 0.0000  
FLOOR= -60.0000



6 dB HORN

SCAN: 4.5"

Co-Pol. RASTER 15





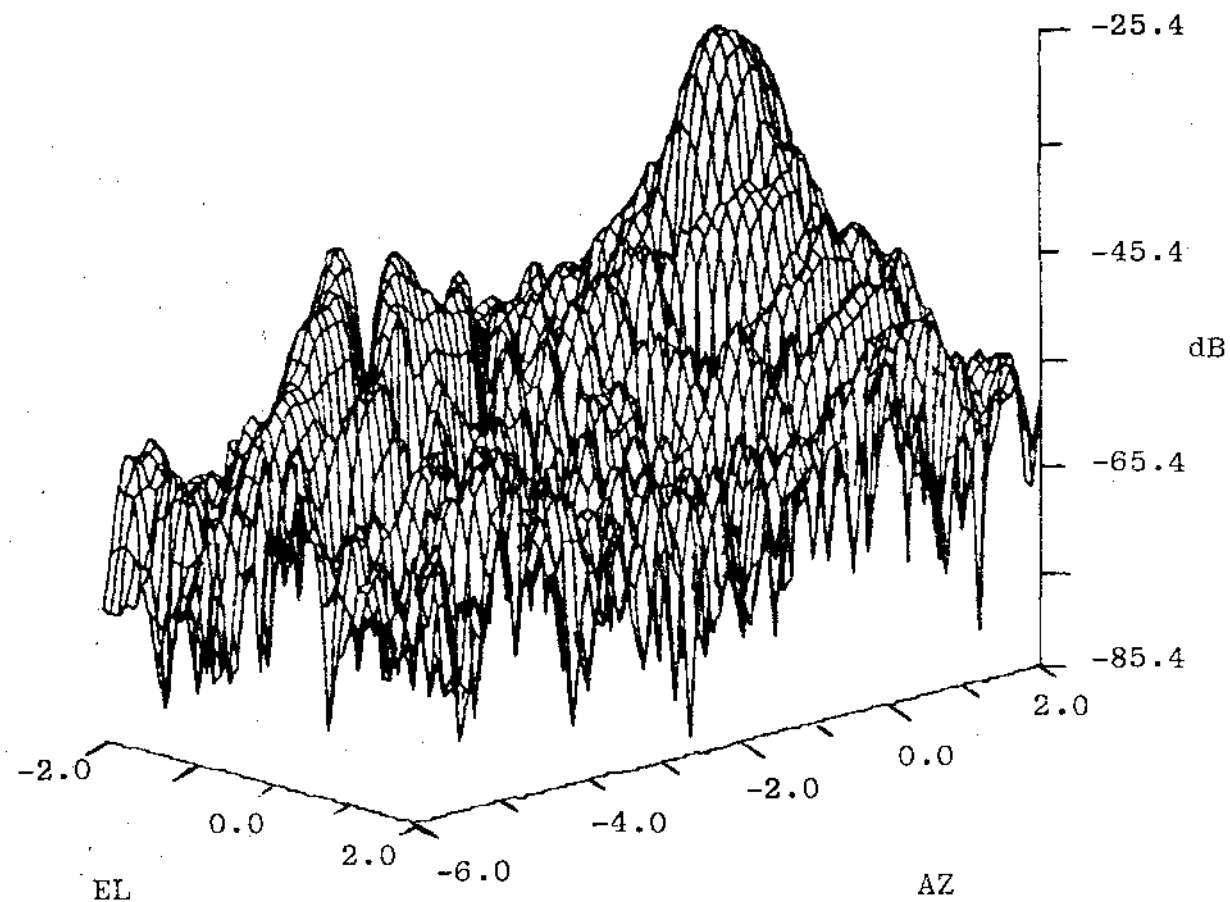
VRIGH--29.9000  
LSC--87.1000  
CEILING--20.0000  
FLOOR--30.0000



6 dB HORN

SCAN: 4.5"

X-Pol. RASTER 16



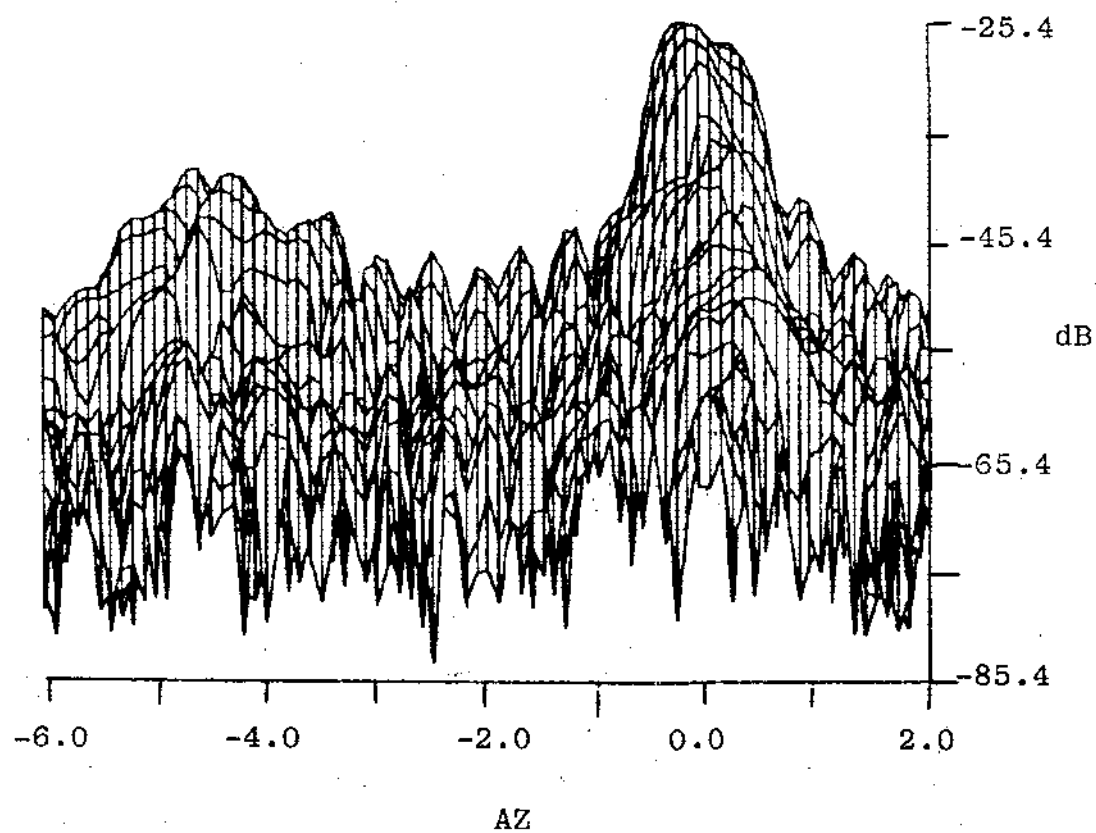
WIND--28.9000  
WLOU--87.1000  
CEILING--20.0000  
FLOOR--50.0000



6 dB HORN

SCAN: 4.5"

X-Pol. RASTER 16



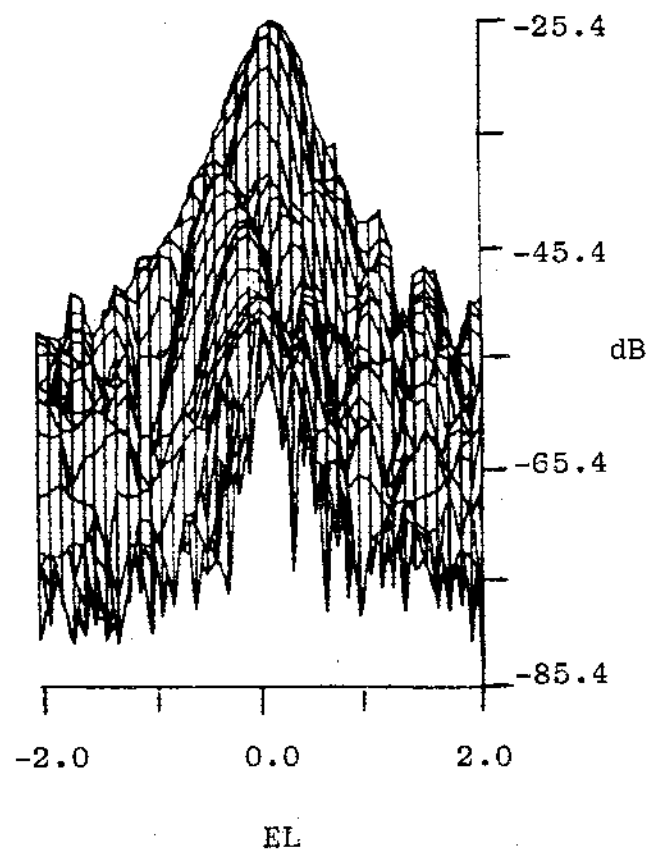
YHIGH=-28.9000  
YLOW=-57.1000  
CEILING=-20.0000  
FLOOR=-30.0000



6 dB HORN

SCAN: 4.5"

X-Pol. RASTER 16



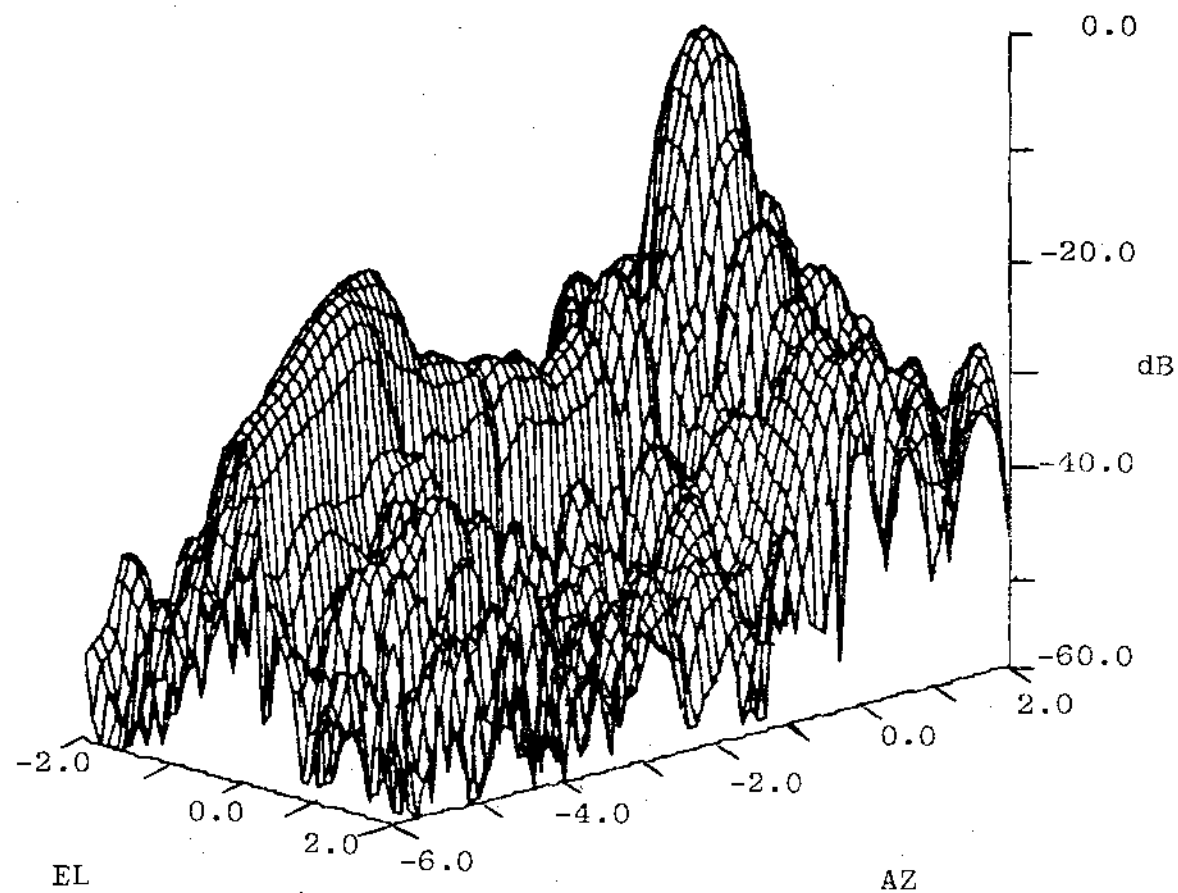
VHIGH- -2.2000  
VLOW- -80.3000  
CEILING- 0.0000  
FLOOR- -60.0000



6 dB HORN

SCAN: 0.0"

Co-Pol. RASTER 35



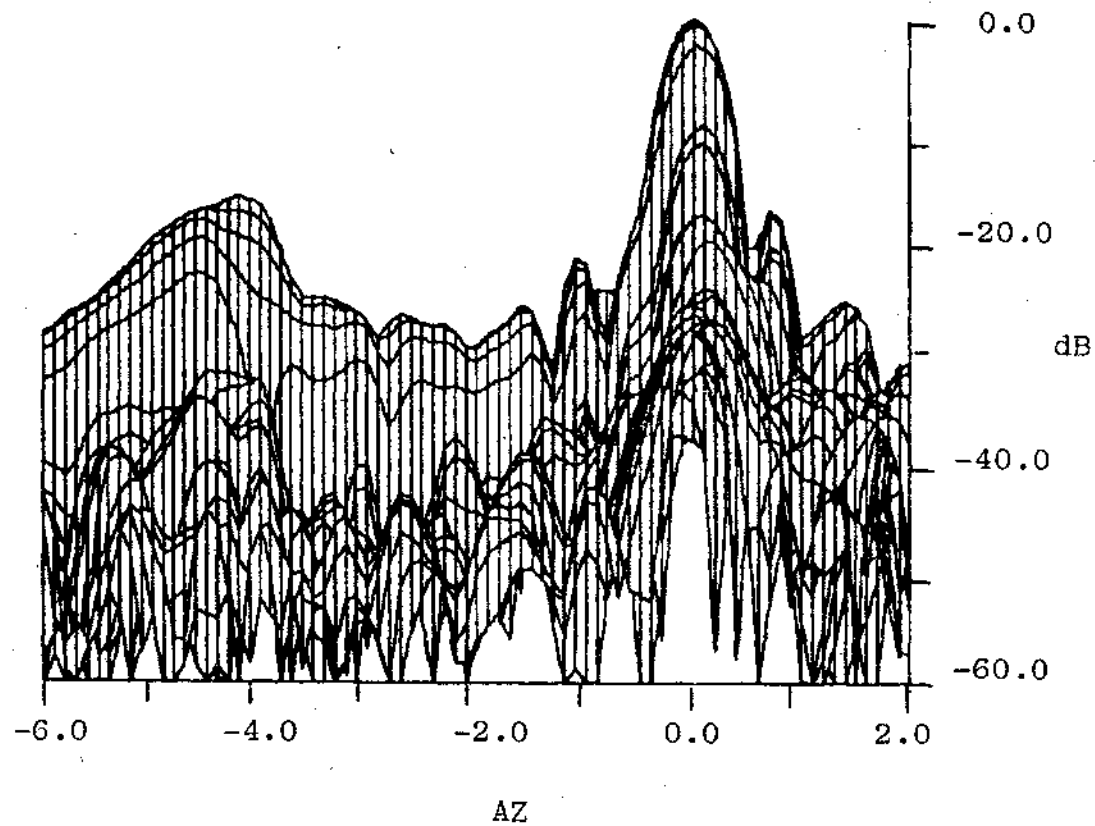
YHIGH\*-2.2000  
YLOW\*-80.3000  
CEILING\* 0.0000  
FLOOR\*-60.0000



6 dB HORN

SCAN: 0.0"

Co-Pol. RASTER 35



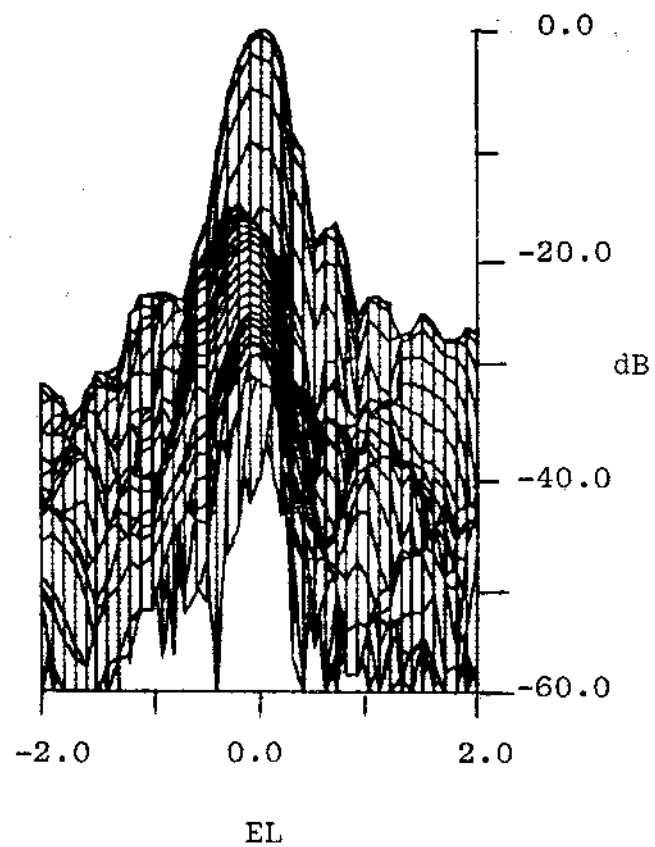
YHIGH= -2.2000  
YLOW= -80.3000  
CEILING= 0.0000  
FLOOR= -60.0000



6 dB HORN

SCAN: 0.6"

Co-Pol. RASTER 35



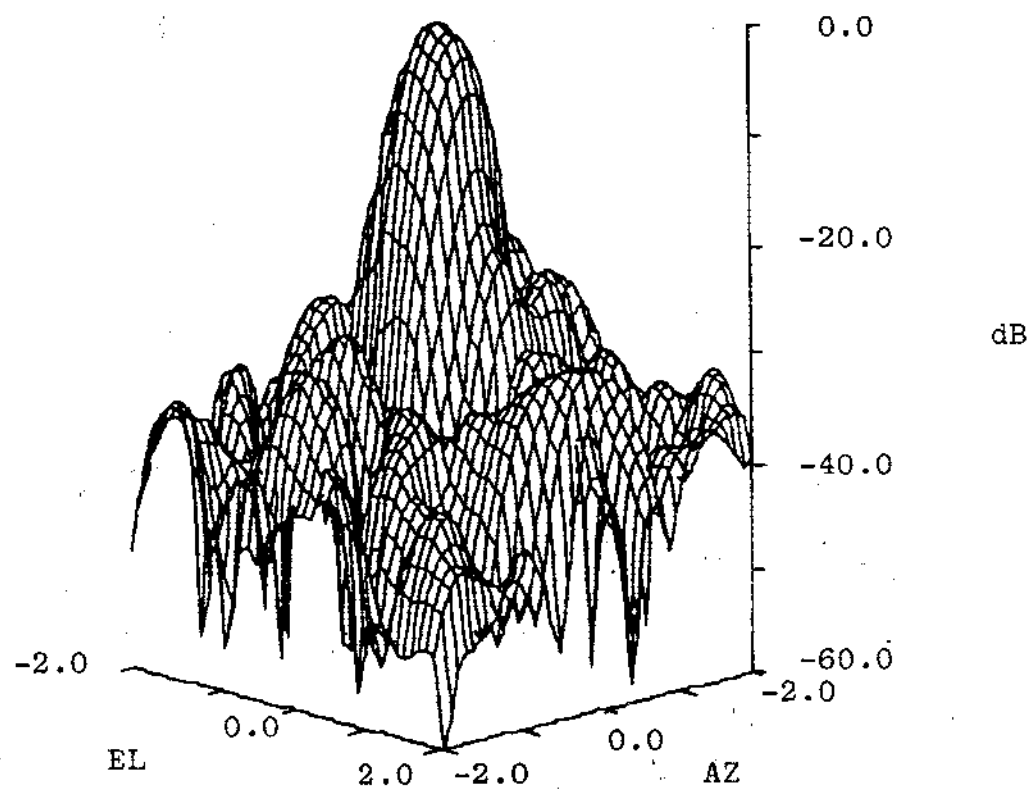
PMHGH: -2.2000  
VLOW: -73.3000  
TEILING: 0.0000  
FLOOR: -60.0000



14 dB HORN

Scan: 0.0"

Co-Pol. RASTER 01





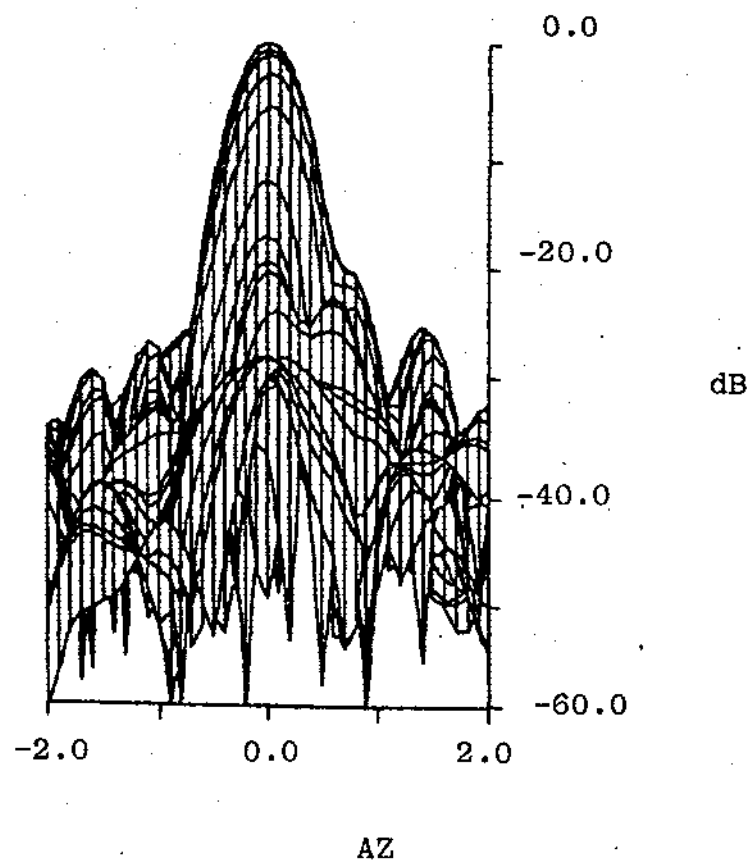
YHIGH- -2.2000  
YLOW- -73.3000  
CEILING- 0.0000  
FLOOR- -60.0000



14 dB HORN

Scan: 0.0"

Co-Pol RASTER 01



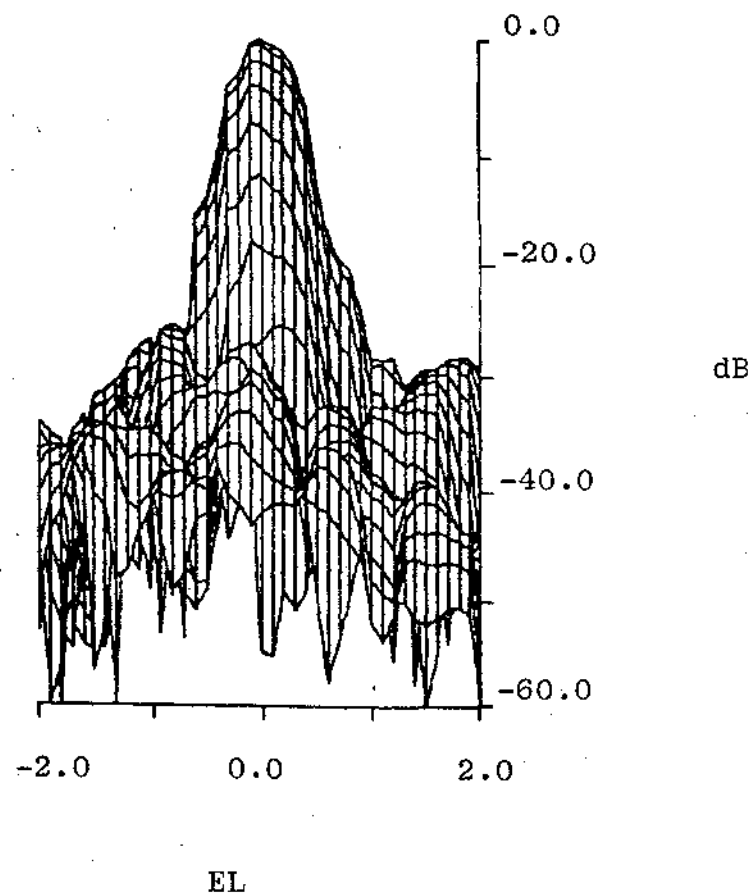
YHIGH\* -2.3400  
YLOW\* -73.3000  
CEILING\* 0.0000  
FLOOR\* -60.0000



14 dB HORN

Scan: 0.0"

Co-Pol. Raster 01



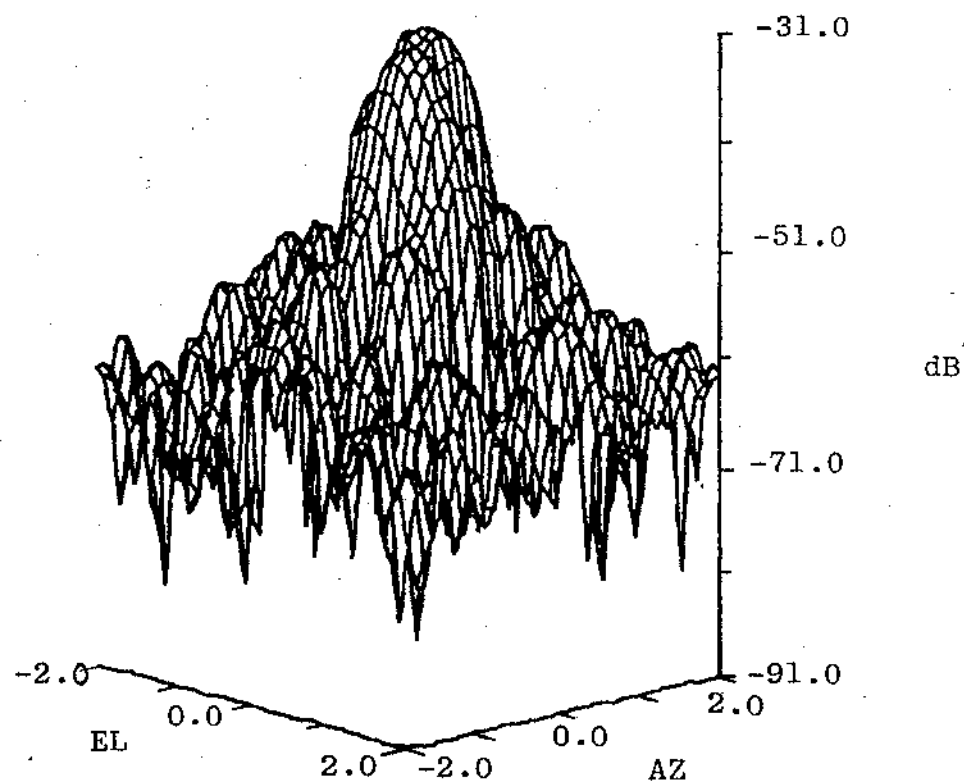
YMICH--33.2000  
YLOW--84.4000  
CEILING--20.0000  
FLOOR--50.0000



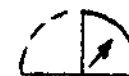
14 dB HORN

Scan: 0.0"

X-Pol RASTER 02



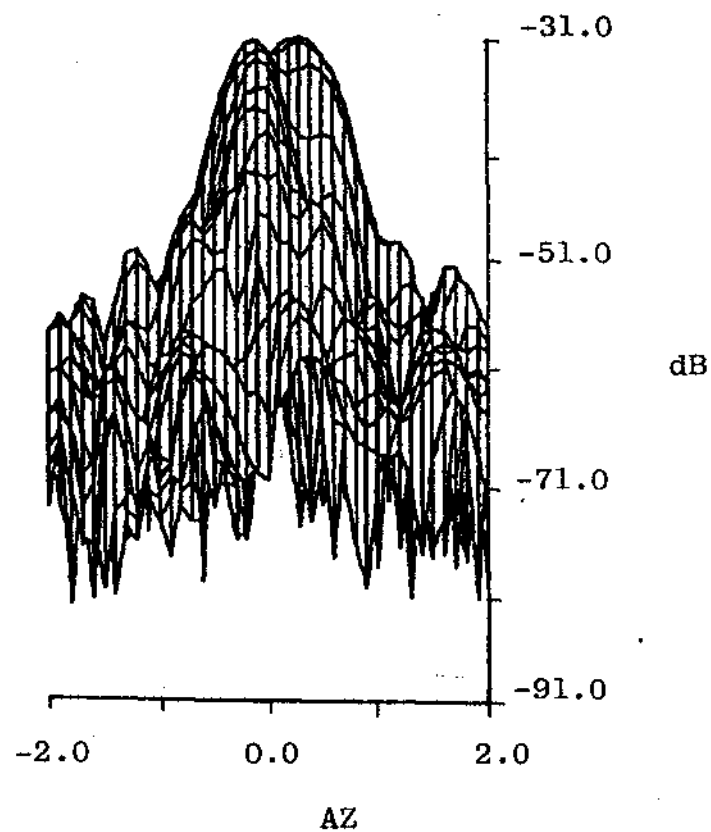
VHIGH--33.2000  
VLOW--34.4000  
CEILING--20.0000  
FLOOR--30.0000



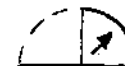
14 dB HORN

Scan: 0.0"

X-Pol RASTER 02



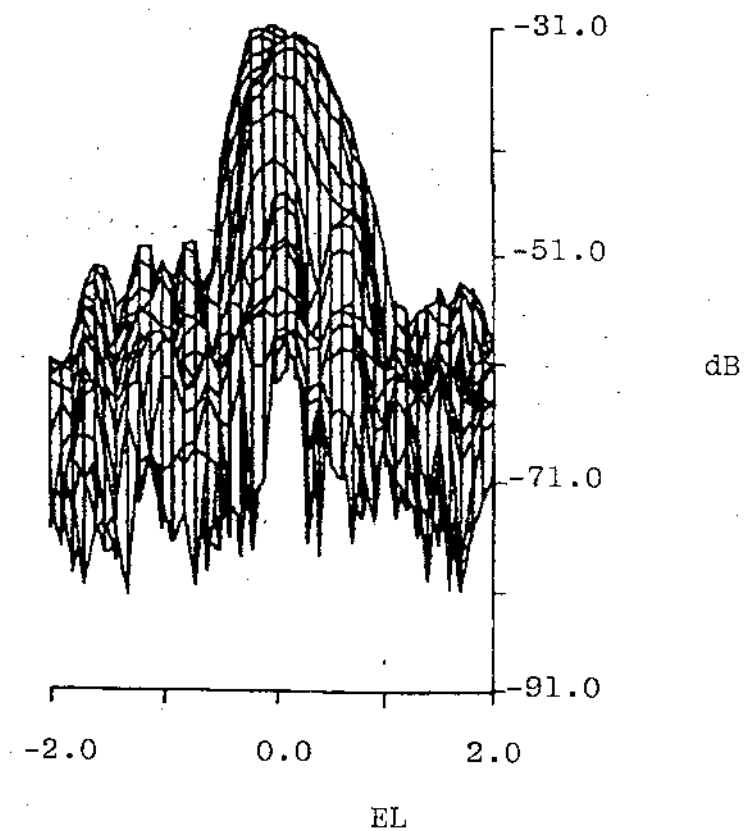
YHIGH--33.2000  
YLOW--54.4000  
CEILING--20.0000  
FLOOR--80.0000



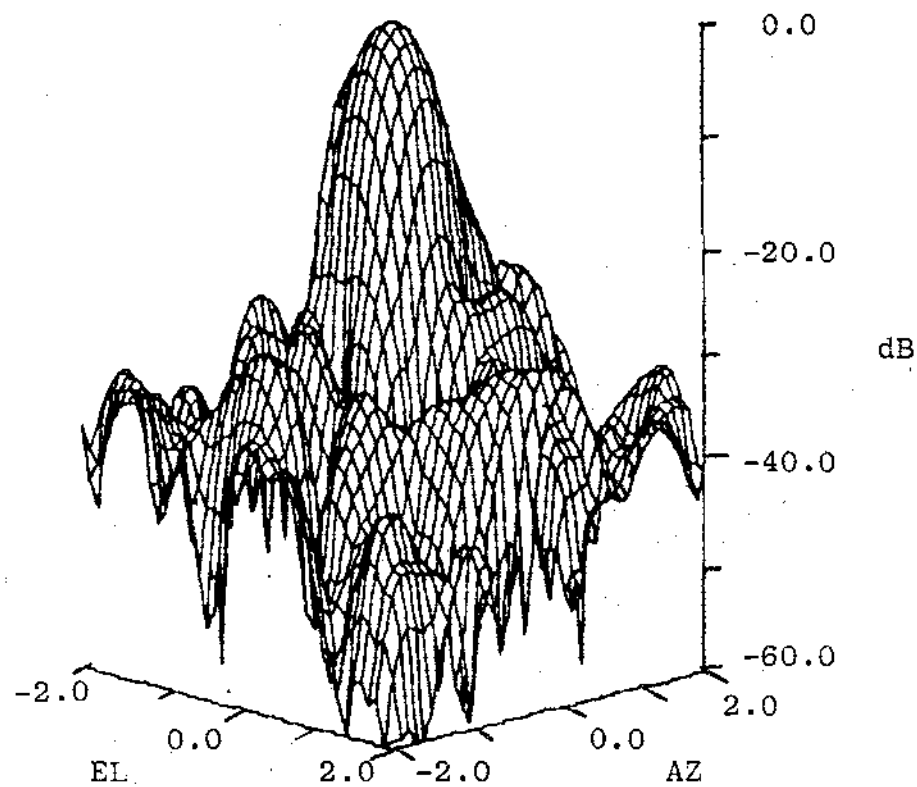
14 dB HORN

Scan: 0.0"

X-Pol RASTER 02



YHIGH=-2.5000  
YLOW=-89.5000  
CEILING= 0.0000  
FLOOR=-60.0000



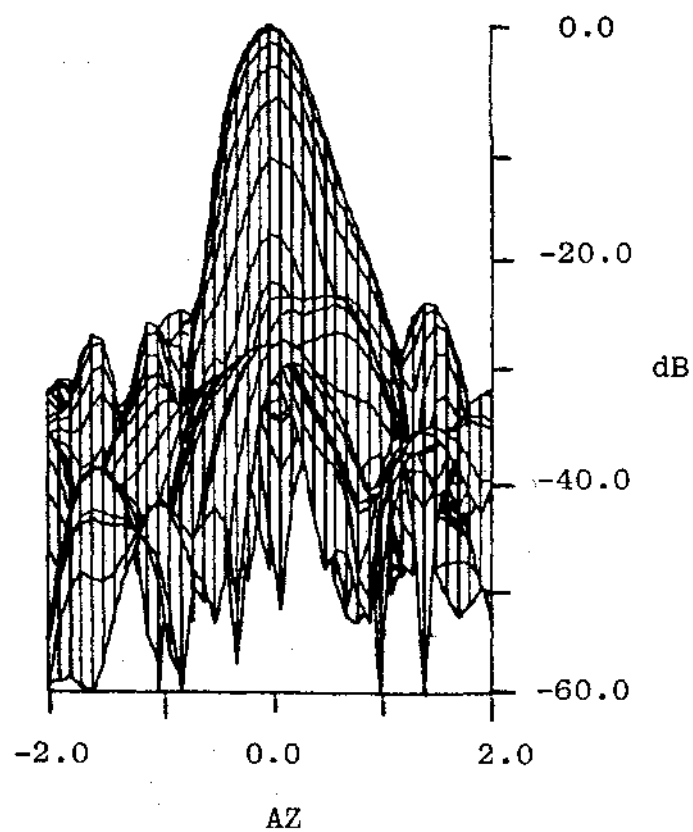
VHIGH+ -2.5000  
VLOW+ -69.5000  
CELLING+ 0.0000  
FLOOR+ -60.0000



14 dB HORN

SCAN: 4.5"

Co-Pol. RASTER 05





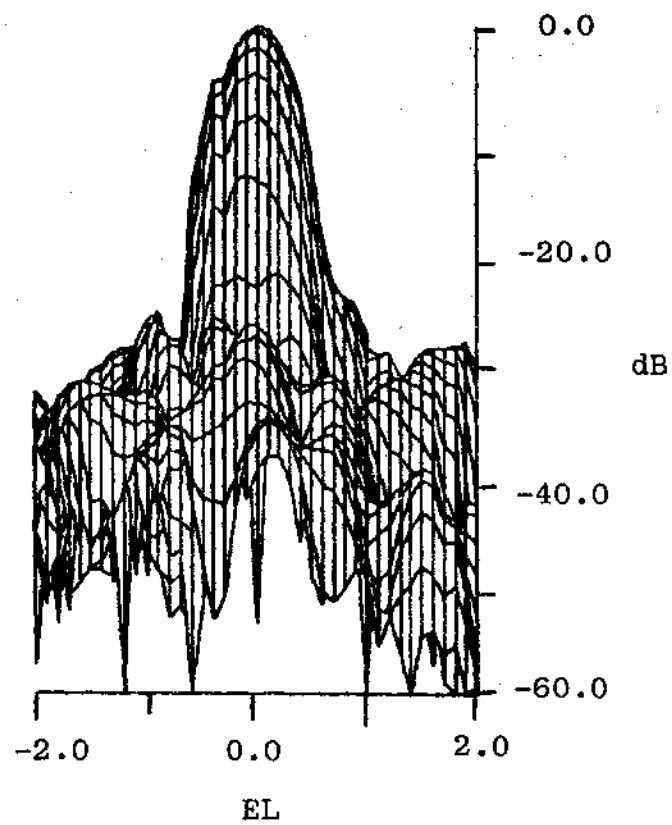
VHIGH= -2.5000  
YLOW= -69.5000  
CEILING= 0.0000  
FLOOR= -60.0000



14 dB HORN

SCAN: 4.5"

Co-Pol. RASTER 05



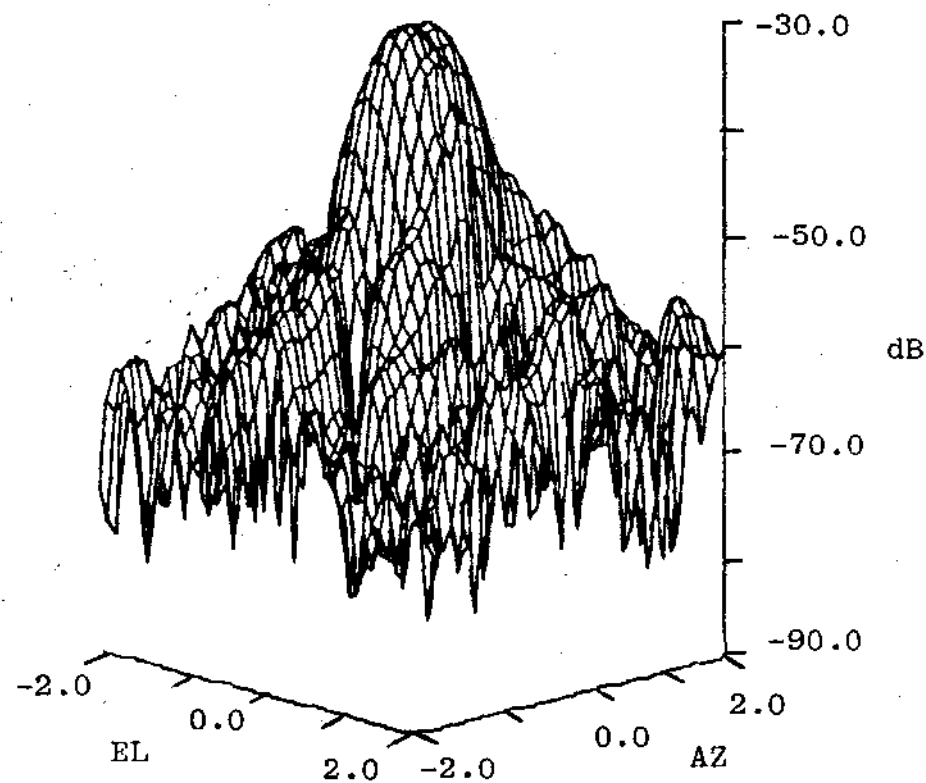
YHIGH--32.5000  
YLOW--85.9000  
CEILING--20.0000  
FLOOR--80.0000



14 dB HORN

SCAN: 4.5"

X-Pol. RASTER 06



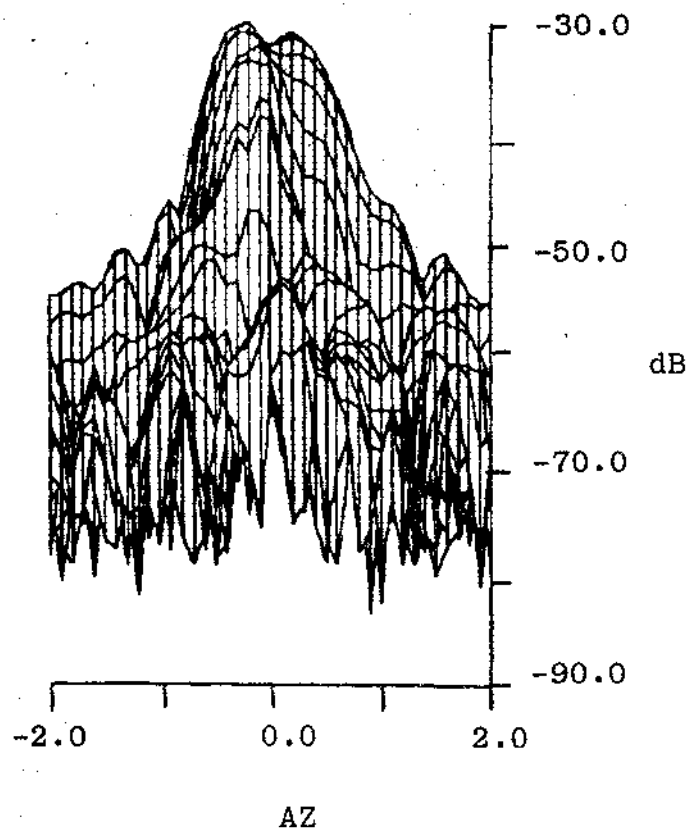
VHIGH--32.5000  
VLOW--85.9000  
CEILING--20.0000  
FLOOR--80.0000



14 dB HORN

SCAN: 4.5"

X-Pol. RASTER 06



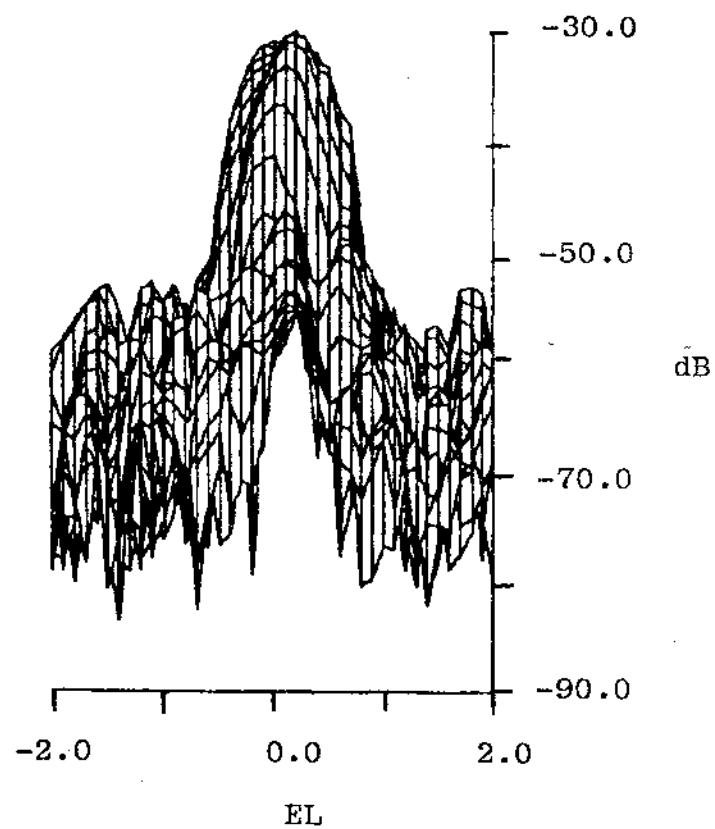
YHIGH=-32.5000  
YLOW=-85.9000  
CEILING=-20.0000  
FLOOR=-80.0000



14 dB HORN

SCAN: 4.5"

X-Pol. RASTER 06



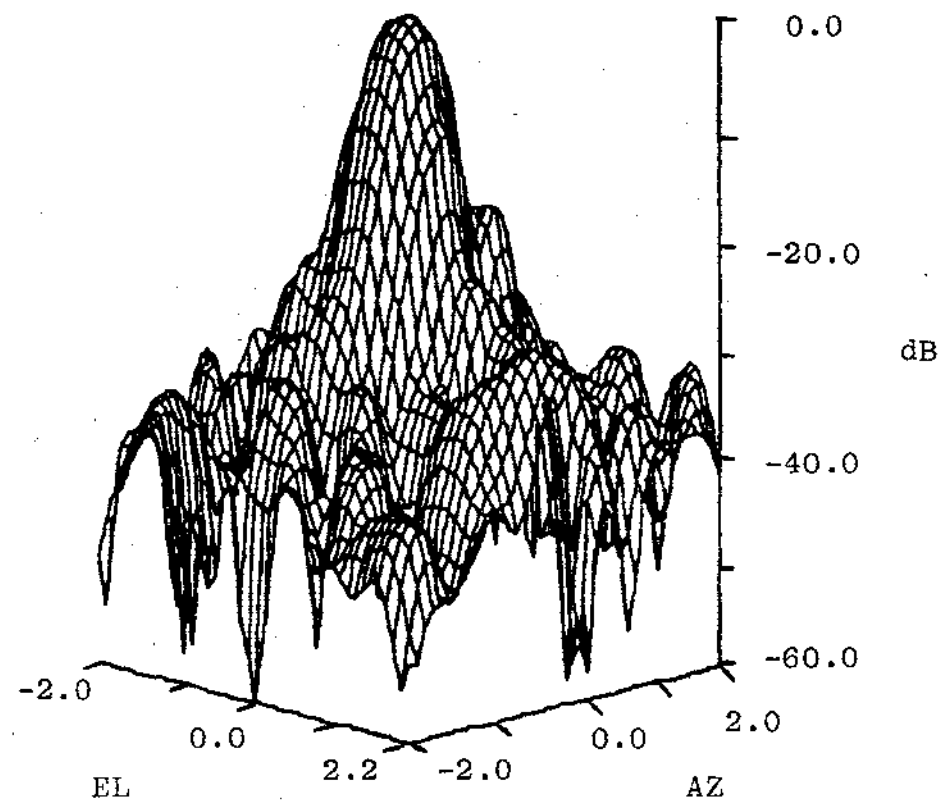
YNIGH= -2.4000  
YLOW= -76.9000  
CEILING= 0.0000  
FLOOR= -60.0000



14 dB HORN

SCAN: 6.5"

Co-Pol. RASTER 03

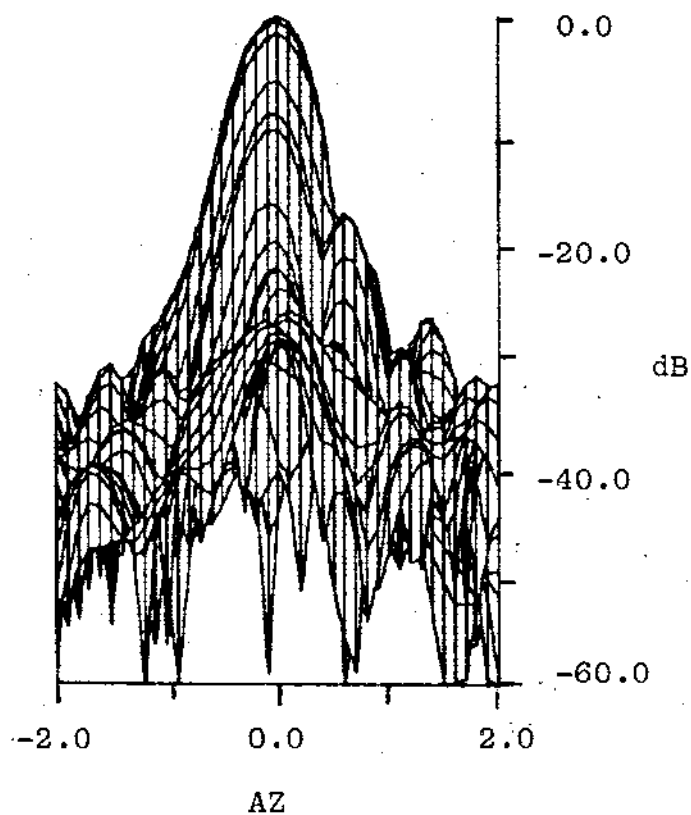


VHIGH\* -2.4000  
VLOW\* -76.9000  
CEILING\* 0.0000  
FLOOR\* -60.0000

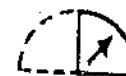


14 dB HORN  
SCAN: 6.5"

Co-Pol. RASTER 03



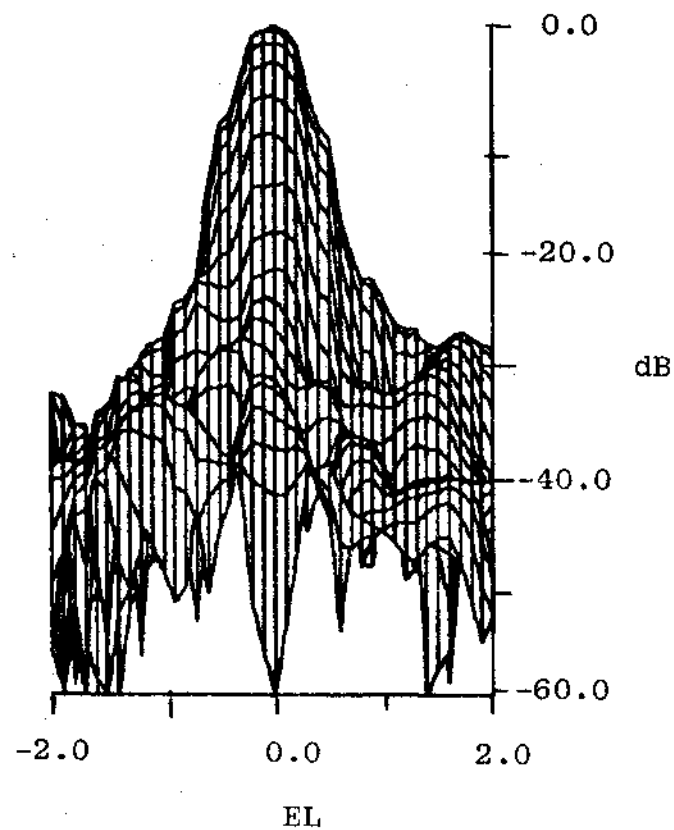
YHIGH- -2.4000  
YLOW--76.0000  
CEILING- 8.0000  
FLOOR--68.0000



14 dB HORN

SCAN: 6.5"

Co-Pol. RASTER 03



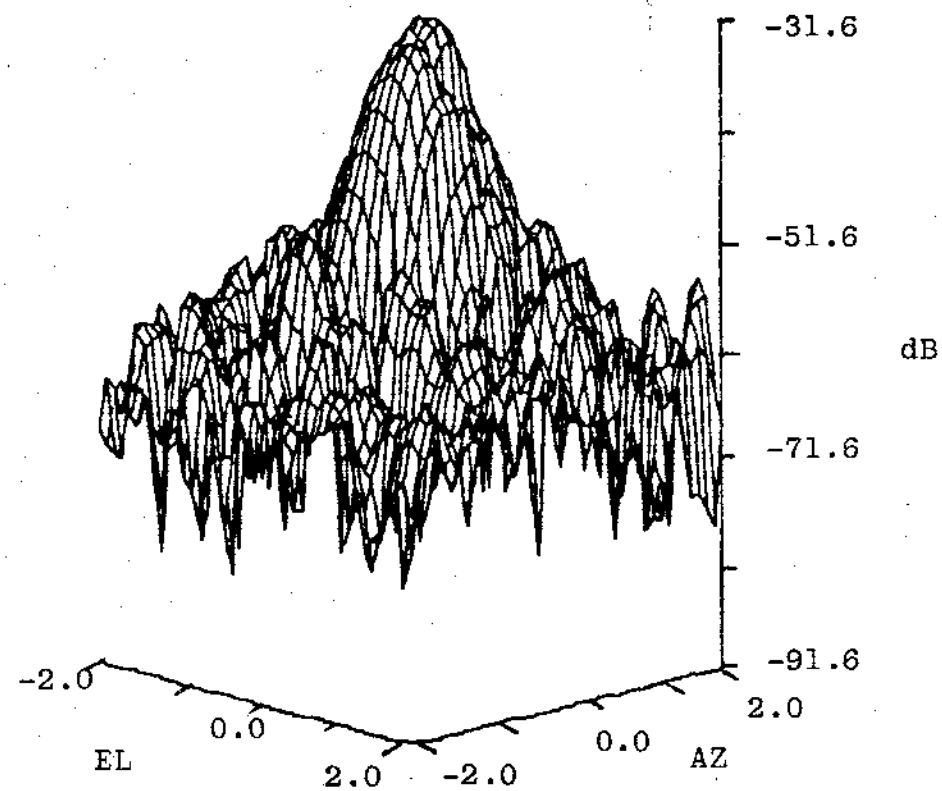
YHIGH=-34.0000  
YLOW=-85.5000  
CEILING=-20.0000  
FLOOR=-80.0000



14 dB HORN

SCAN: 6.5"

X Pol. RASTER 04





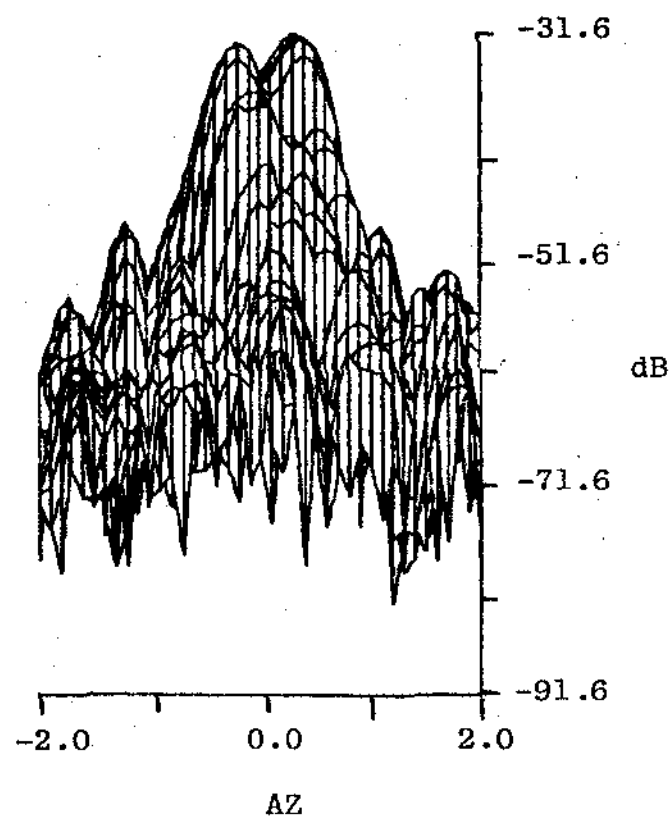
YHIGH\*-34.0000  
YLOW\*-55.5000  
CEILING\*-20.0000  
FLOOR\*-50.0000



14 dB HORN

SCAN: 6.5"

X-Pol. RASTER 04



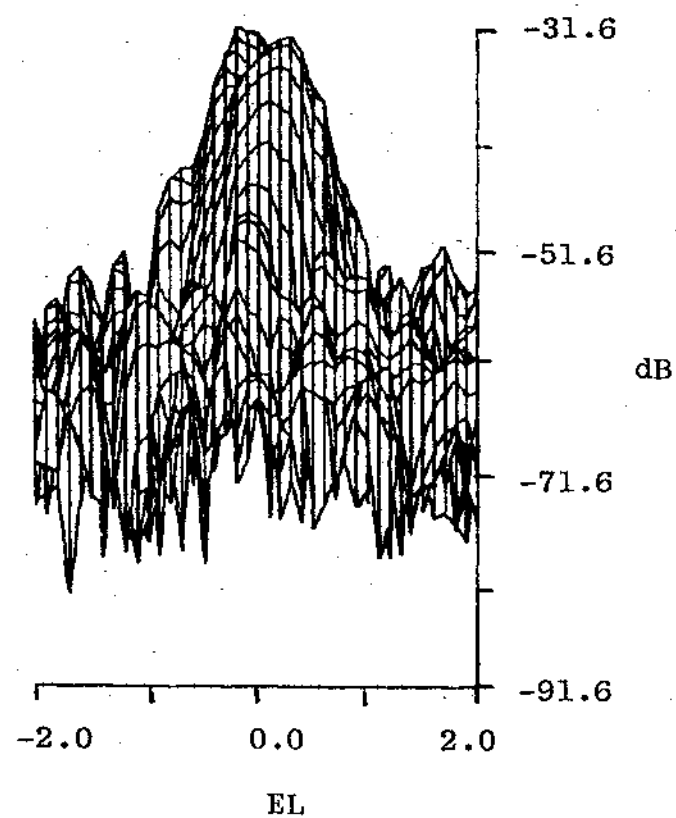
YHIGH=-34.0000  
YLOW=-85.5000  
CEILING=-20.0000  
FLOOR=-80.0000



14 dB HORN

SCAN: 6.5"

X Pol. RASTER 04

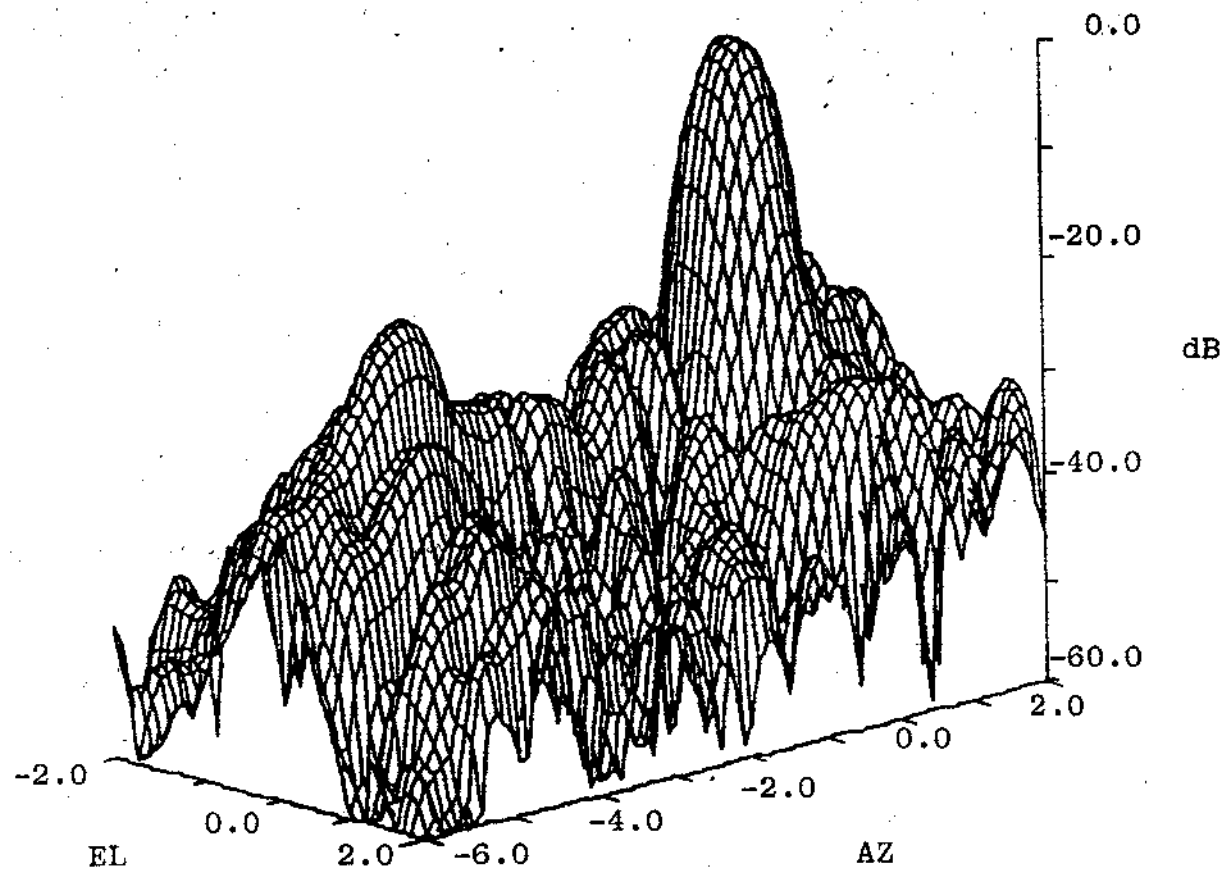


VMICH- -3.4000  
VLOW- -32.6000  
CEILING- 0.0000  
FLOOR- -60.0000



14 dB HORN  
Scan: 0.0"

Co-Pol RASTER 11



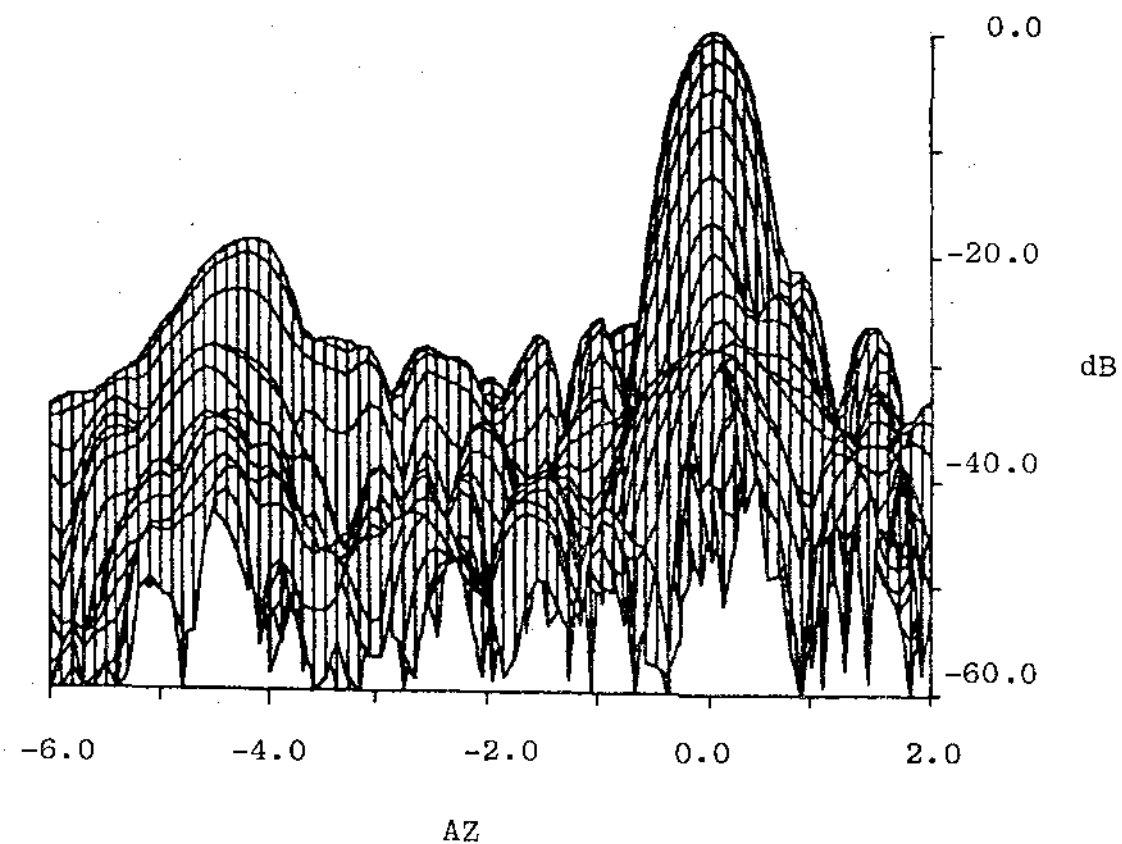
YHIGH- -3.4000  
YLOW--82.6000  
CEILING- 0.0000  
FLOOR--60.0000



14 dB HORN

Scan: 0.0"

Co-Pol RASTER 11



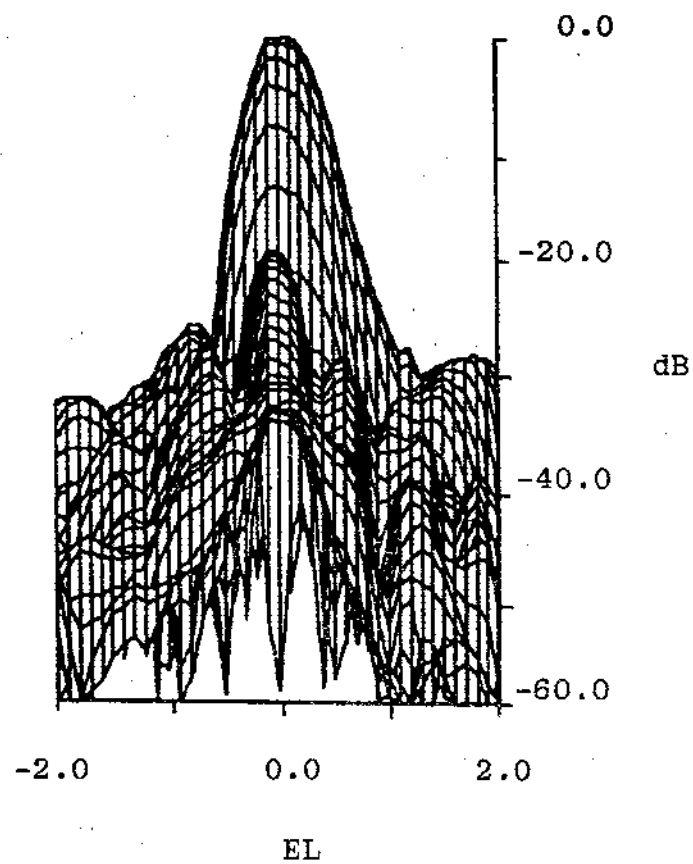
YHIGH= -3.4000  
YLOW= -82.6000  
CEILING= 0.0000  
FLOOR= -60.0000



14 dB HORN

Scan: 0.0"

Co-Pol RASTER 11



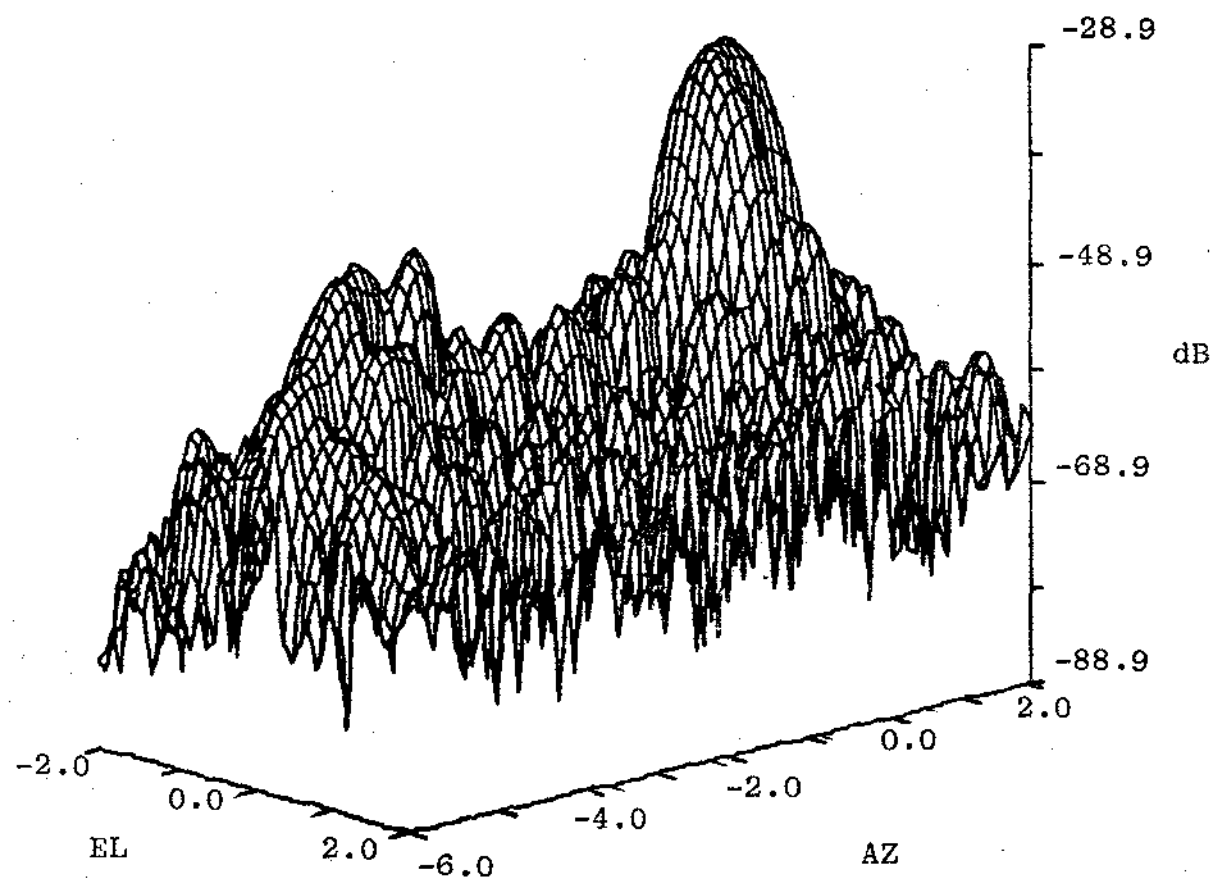
WIND--32.3000  
VLOW--86.4000  
CEILING--20.0000  
FLOOR--80.0000



14 dB HORN

Scan: 0.0"

X-Pol RASTER 12



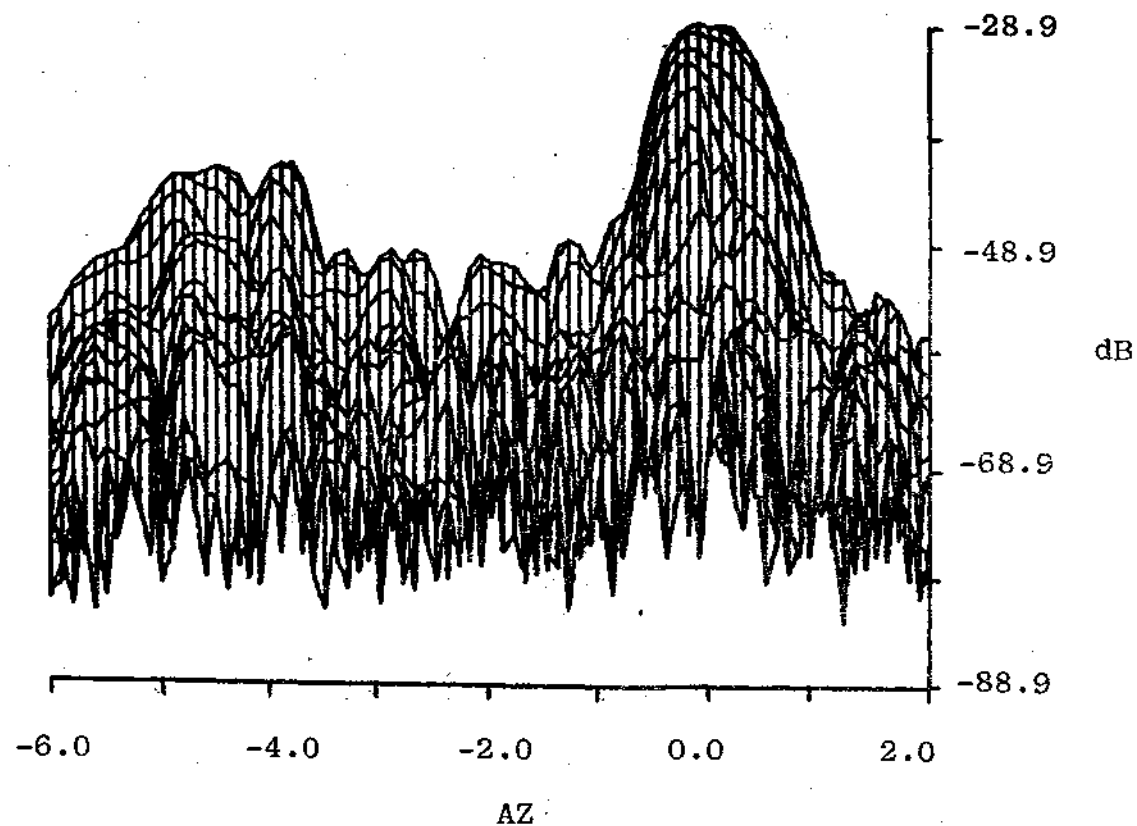
YNICH--32.3000  
YLOW--86.4000  
CEILING--20.0000  
FLOOR--80.0000



14 dB HORN

Scan: 0.0"

X-Pol RASTER 12



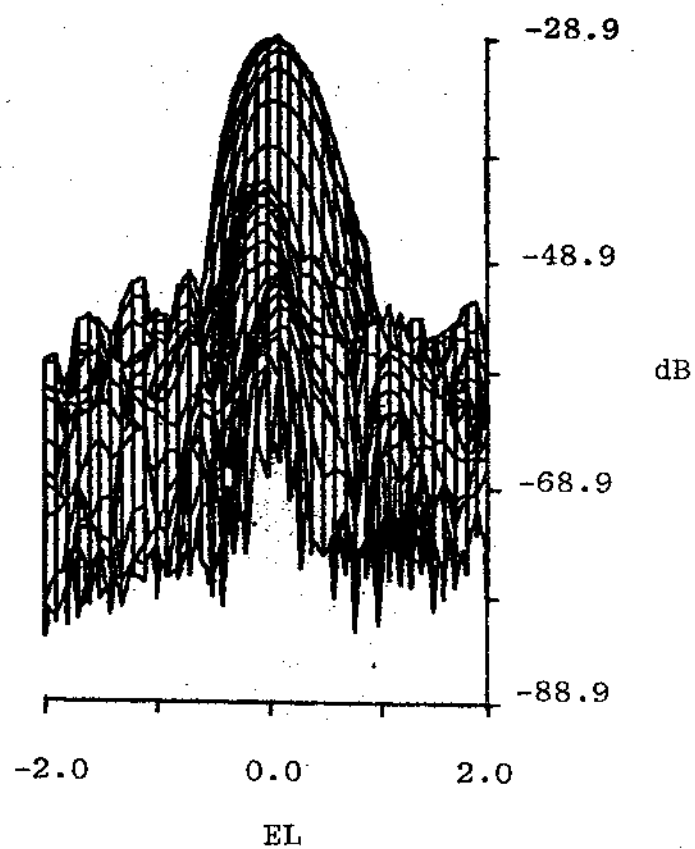
YHIGH--32.3000  
YLOW--26.4000  
CEILING--20.0000  
FLOOR--20.0000



14 dB HORN

Scan: 0.0"

X-Pol RASTER 12





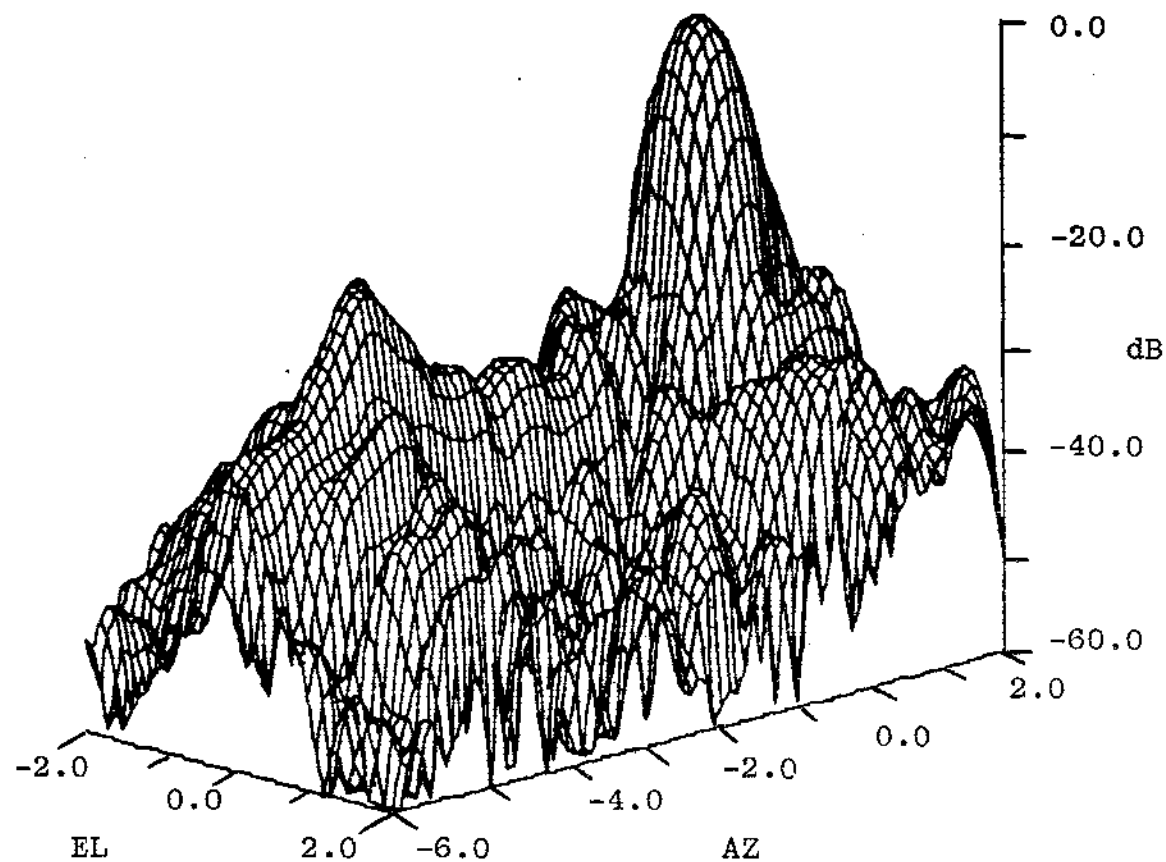
YNICH= -3.5000  
YLOW=-83.4000  
CEILING= 0.0000  
FLOOR=-60.0000



14 dB HORN

SCAN: 4.5"

Co-Pol. RASTER 13



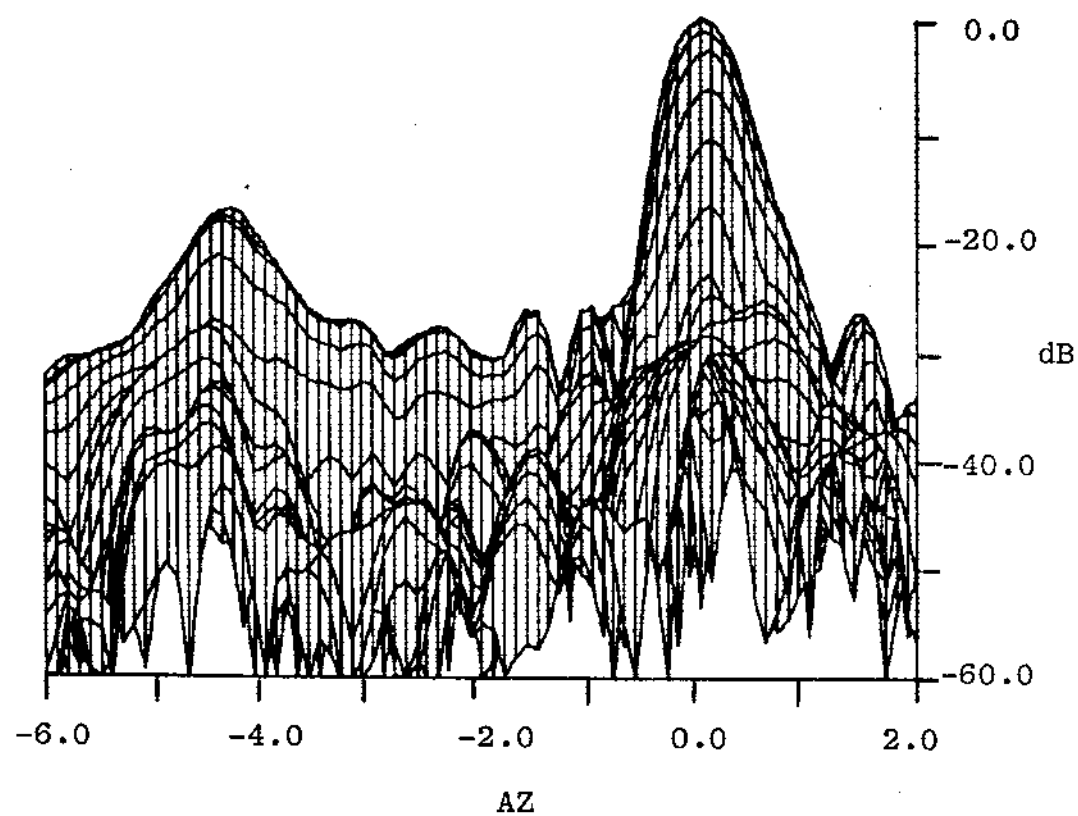
YMIGH= -3.5000  
YLOW= -83.4000  
CEILING= 0.0000  
FLOOR= -60.0000



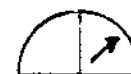
14 dB HORN

SCAN: 4.5"

Co-Pol. RASTER 13



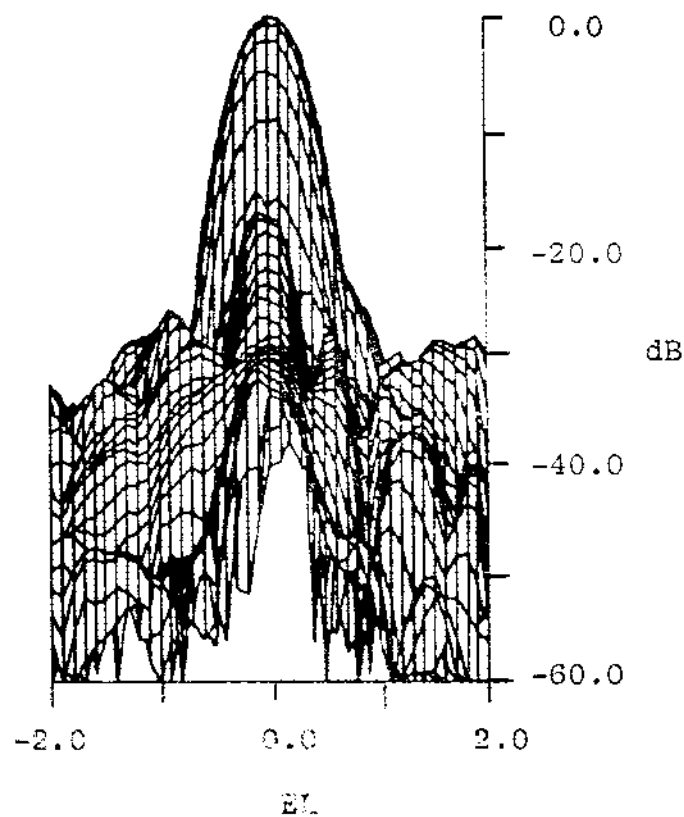
VMIGH= -3.5000  
VLOW= -83.4000  
CEILING= 0.0000  
FLOOR= -60.0000



14 dB HORN

SCAN: 4.5°

Co-Pol. RASTER 13



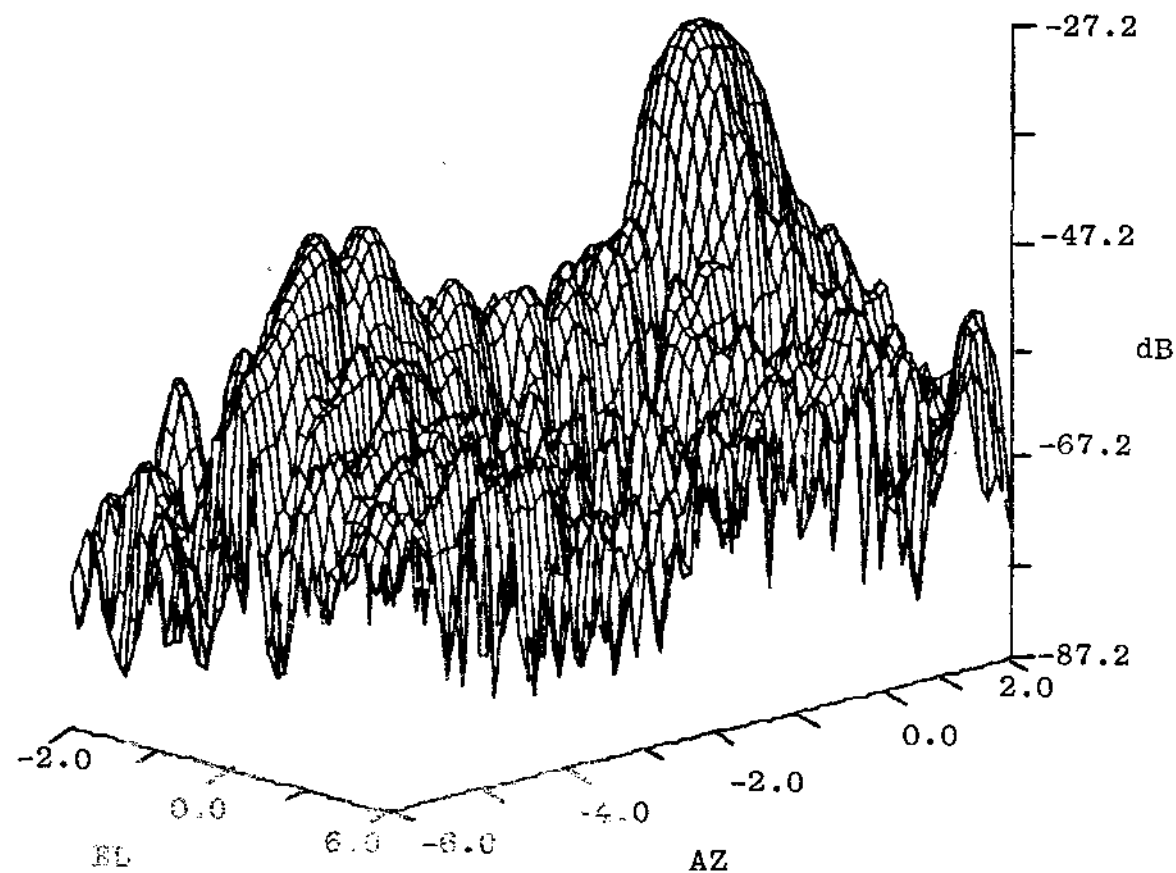
VHIGH=-30.7000  
YLOW=-85.0000  
CEILING=-20.0000  
FLOOR=-80.0000



14 dB HORN

SCAN: 4.5"

X-Pol. RASTER 14



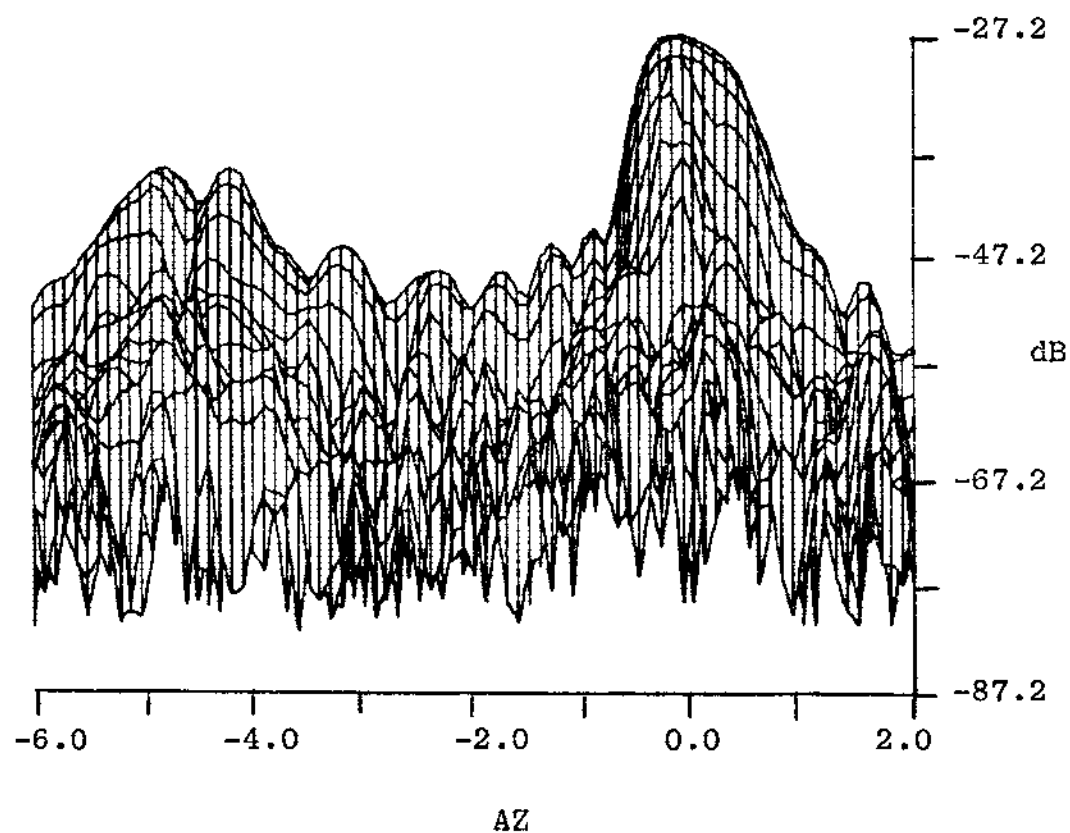
YHIGH--30.7000  
YLOW--85.0000  
CEILING--20.0000  
FLOOR--80.0000



14 dB HORN

SCAN: 4.5"

X-Pol. RASTER 14



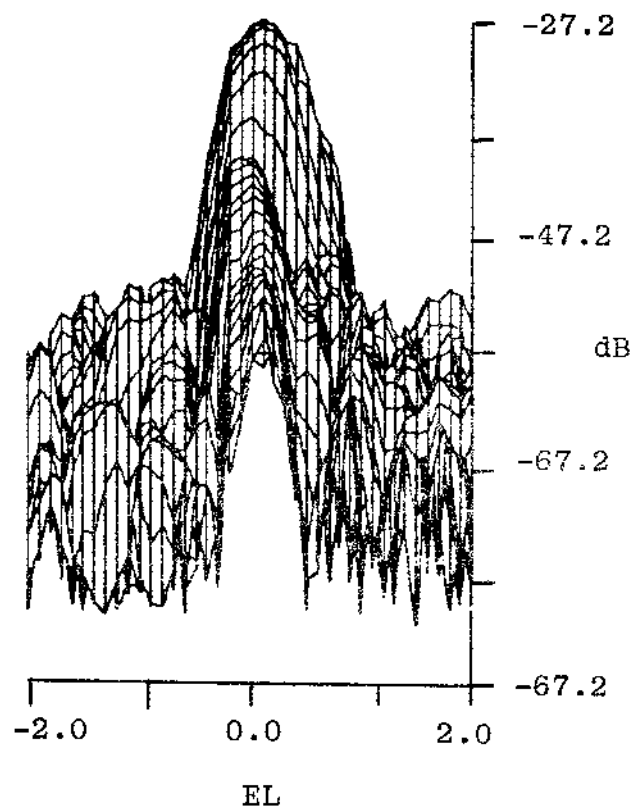
YHIGH=-30.7000  
YLOW=-85.0000  
CEILING=-20.0000  
FLOOR=-90.0000



14 dB HORN

SCAN: 4.5"

X-Pol. RASTER 14



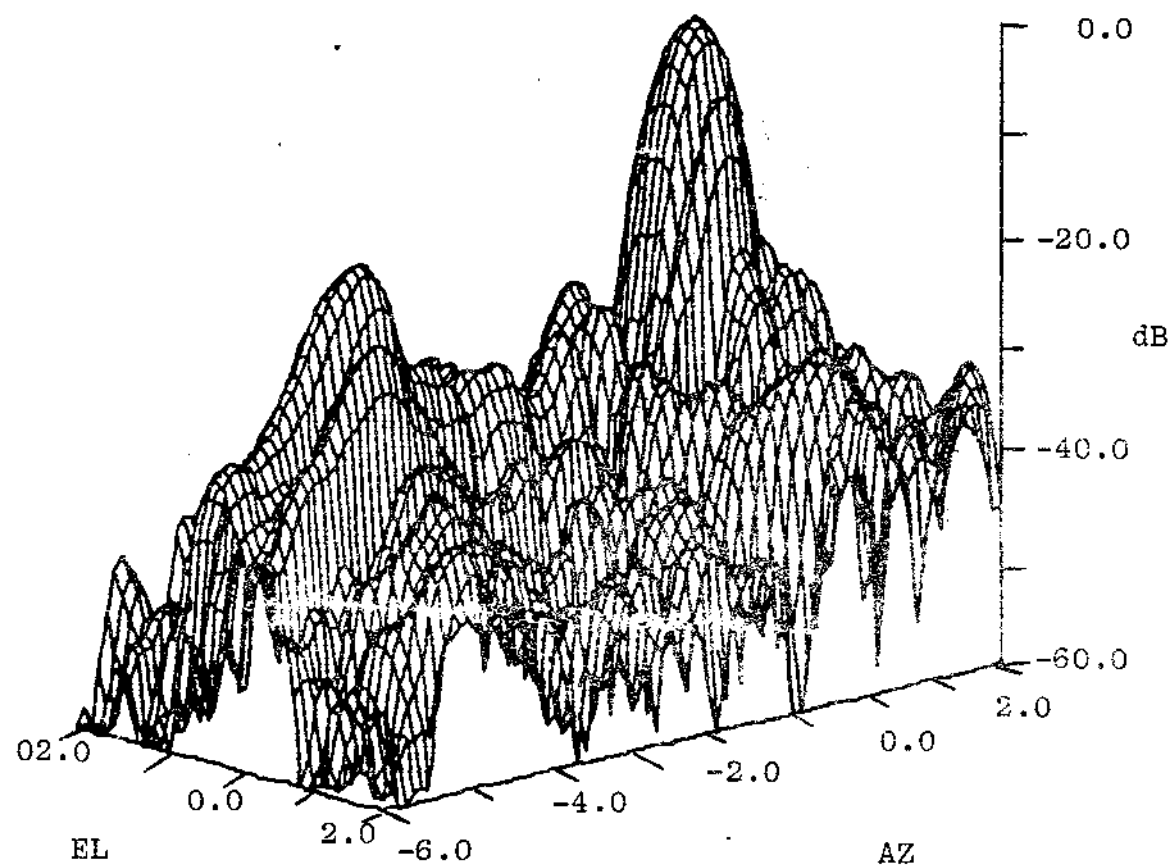
VHIGH- -3.0000  
VLOW- -82.0000  
CEILING- -20.0000  
FLOOR- -80.0000



14 dB HORN

SCAN: 0.0"

Co-Pol. RASTER 36



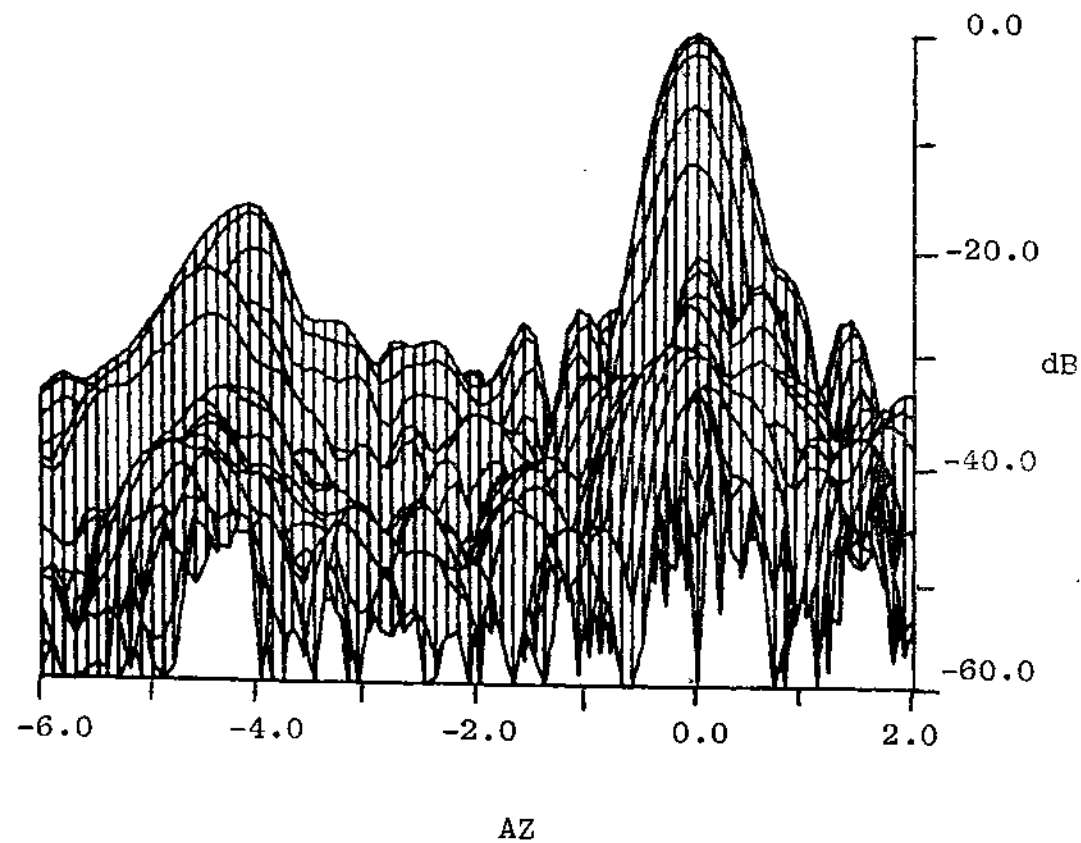
VHIGH- -3.0000  
VLOW- -82.0000  
CEILING- -20.0000  
FLOOR- -80.0000



14 dB HORN

SCAN: 0.0"

Co-Pol. RASTER 36





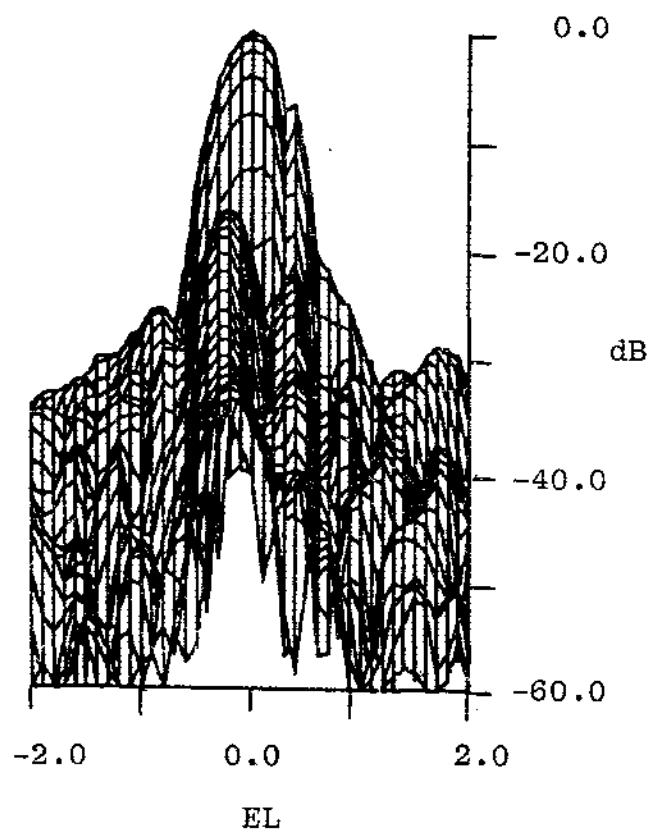
YHIGH- -3.0000  
YLOW- -82.0000  
CEILING- -20.0000  
FLOOR- -30.0000



14 dB HORN




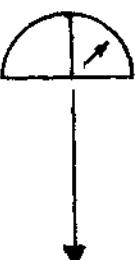
SCAN: 0.0"

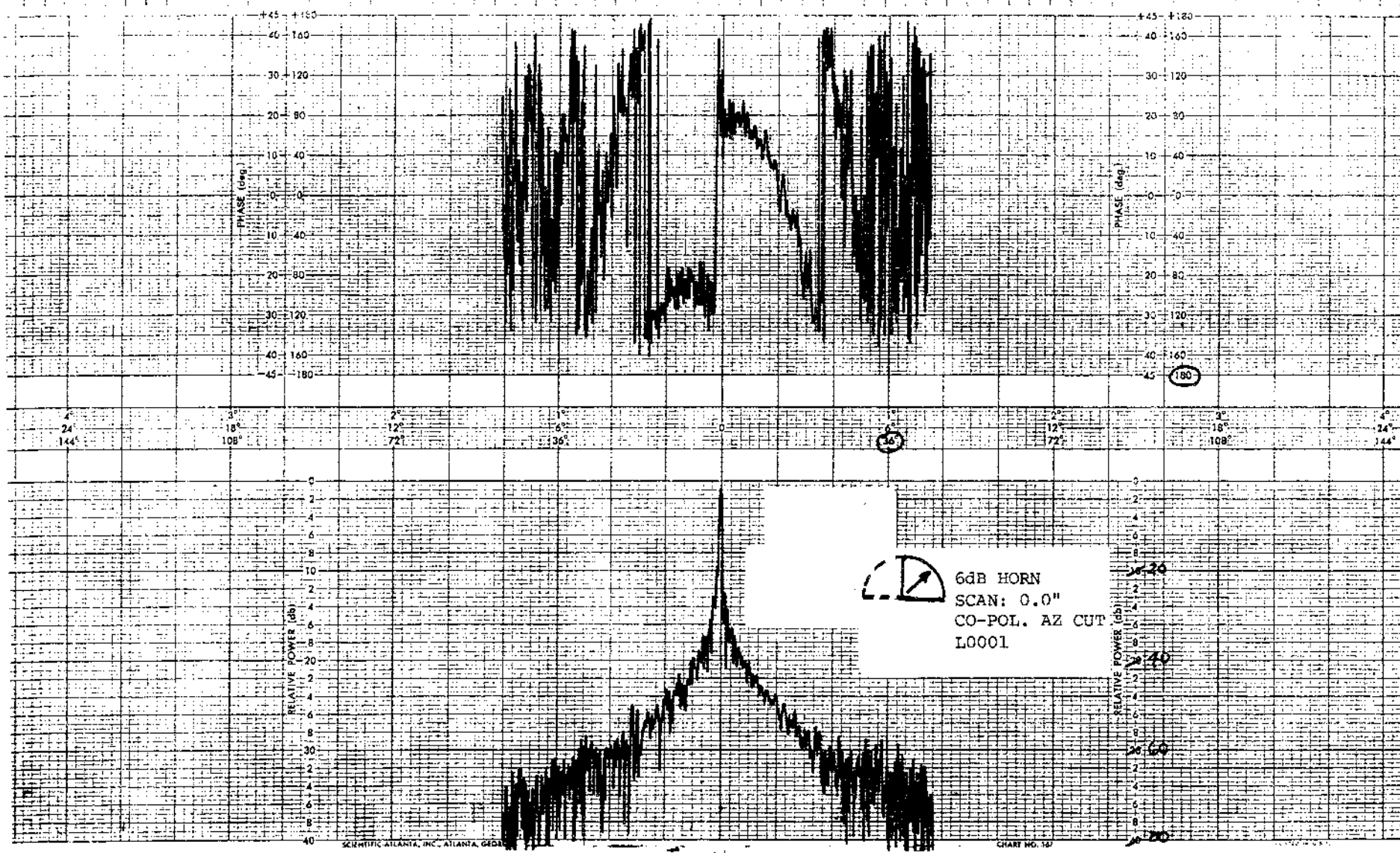
Co-Pol. RASTER 36

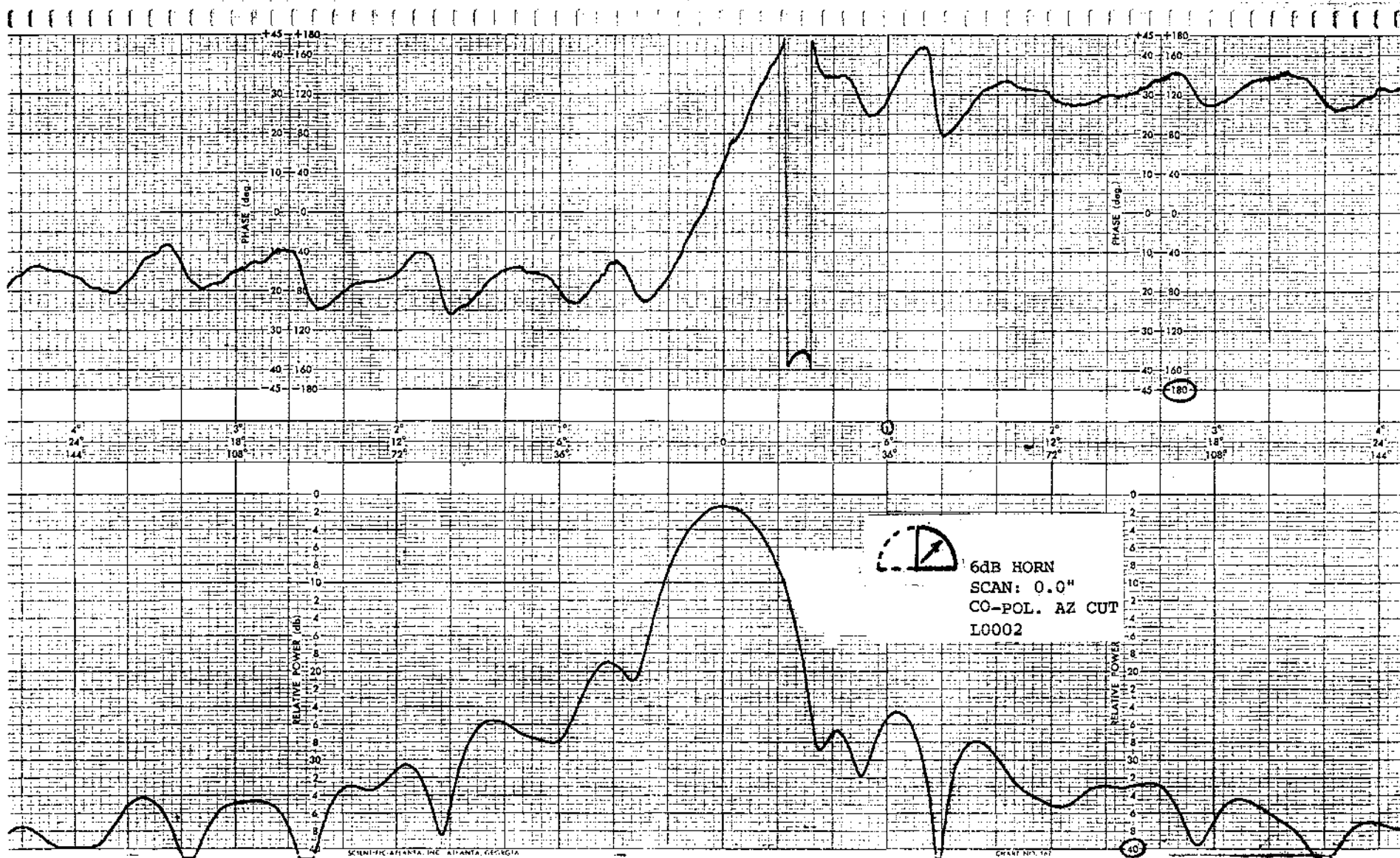


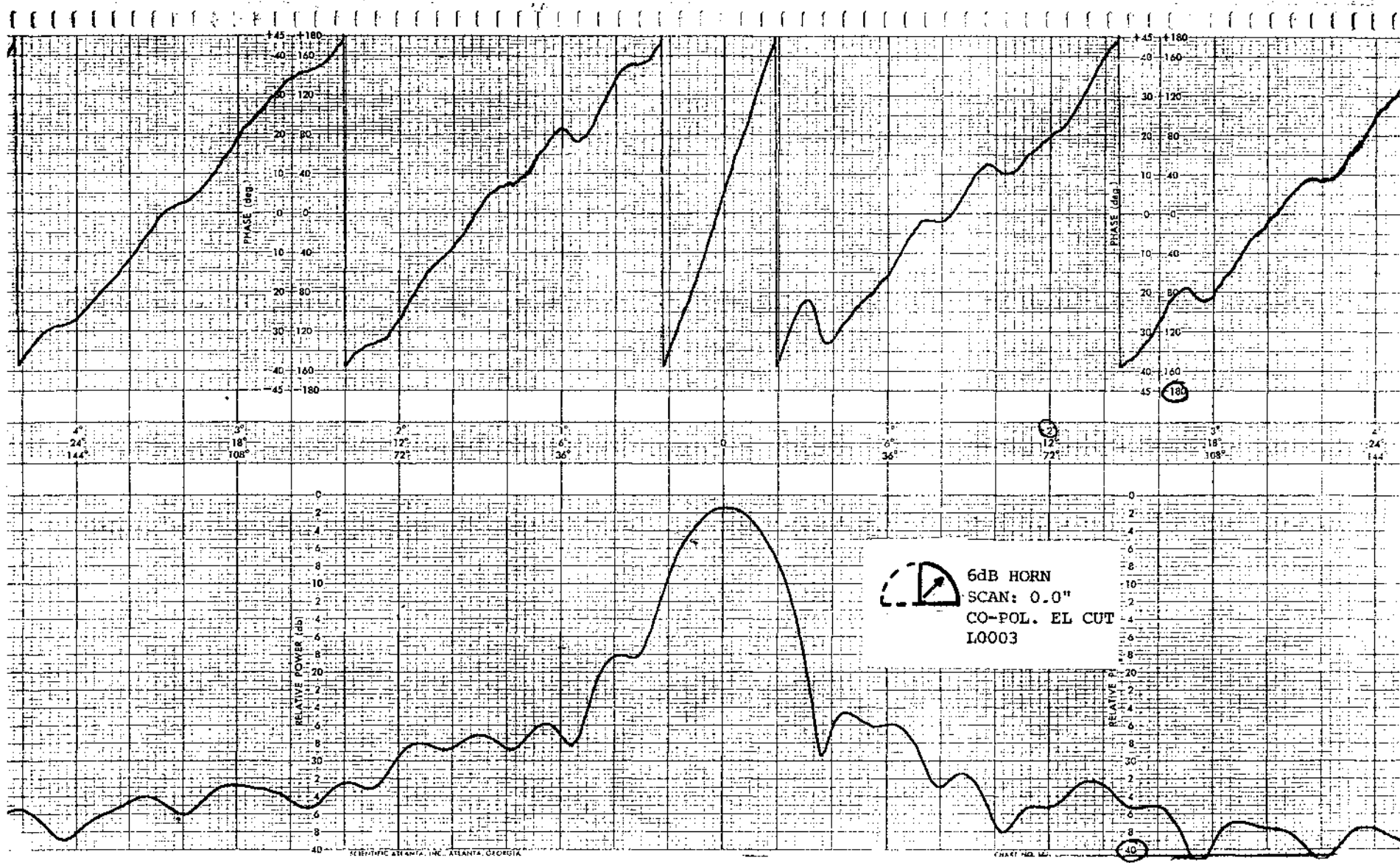
LSST - IV

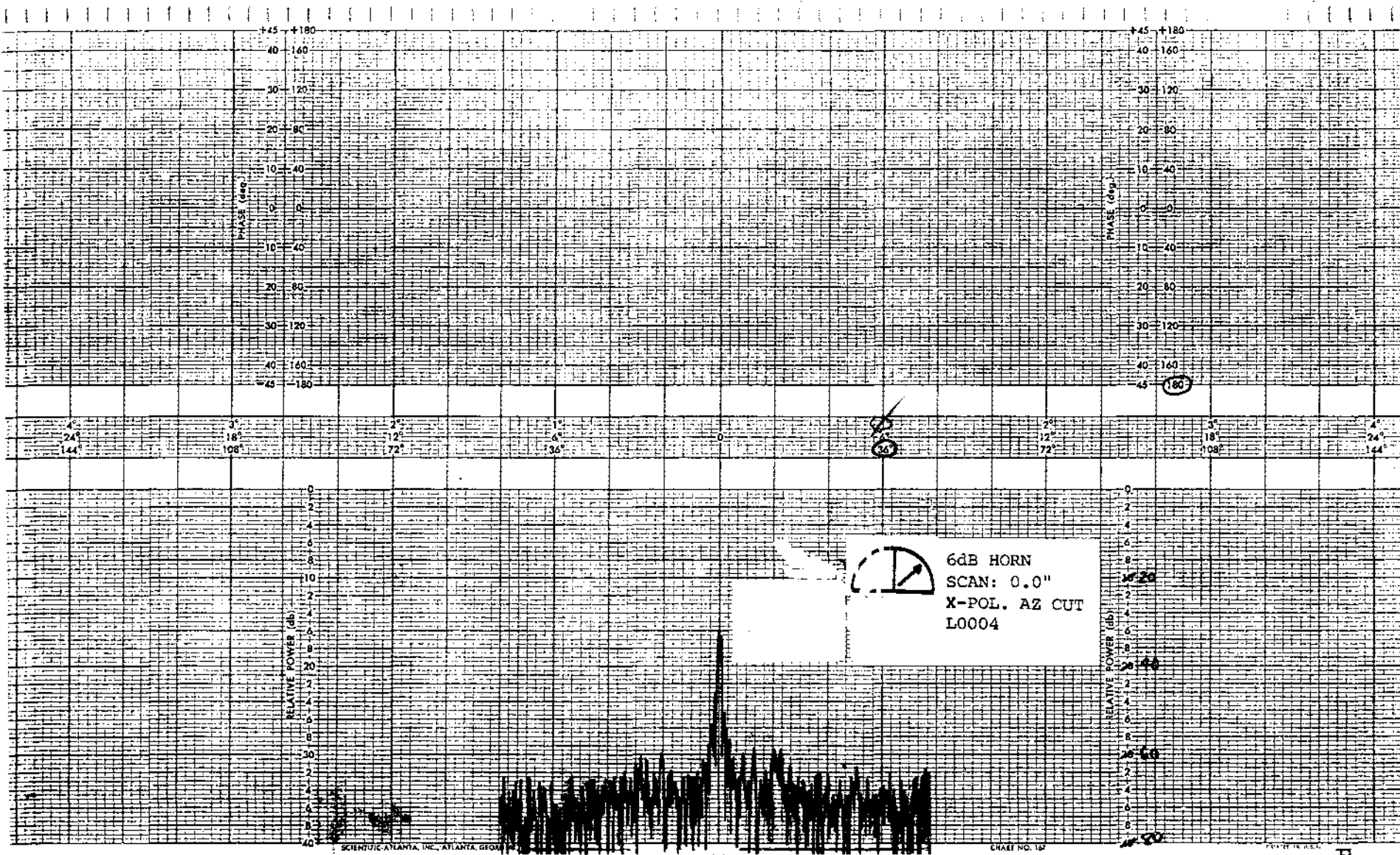
SECONDARY PATTERN LOG

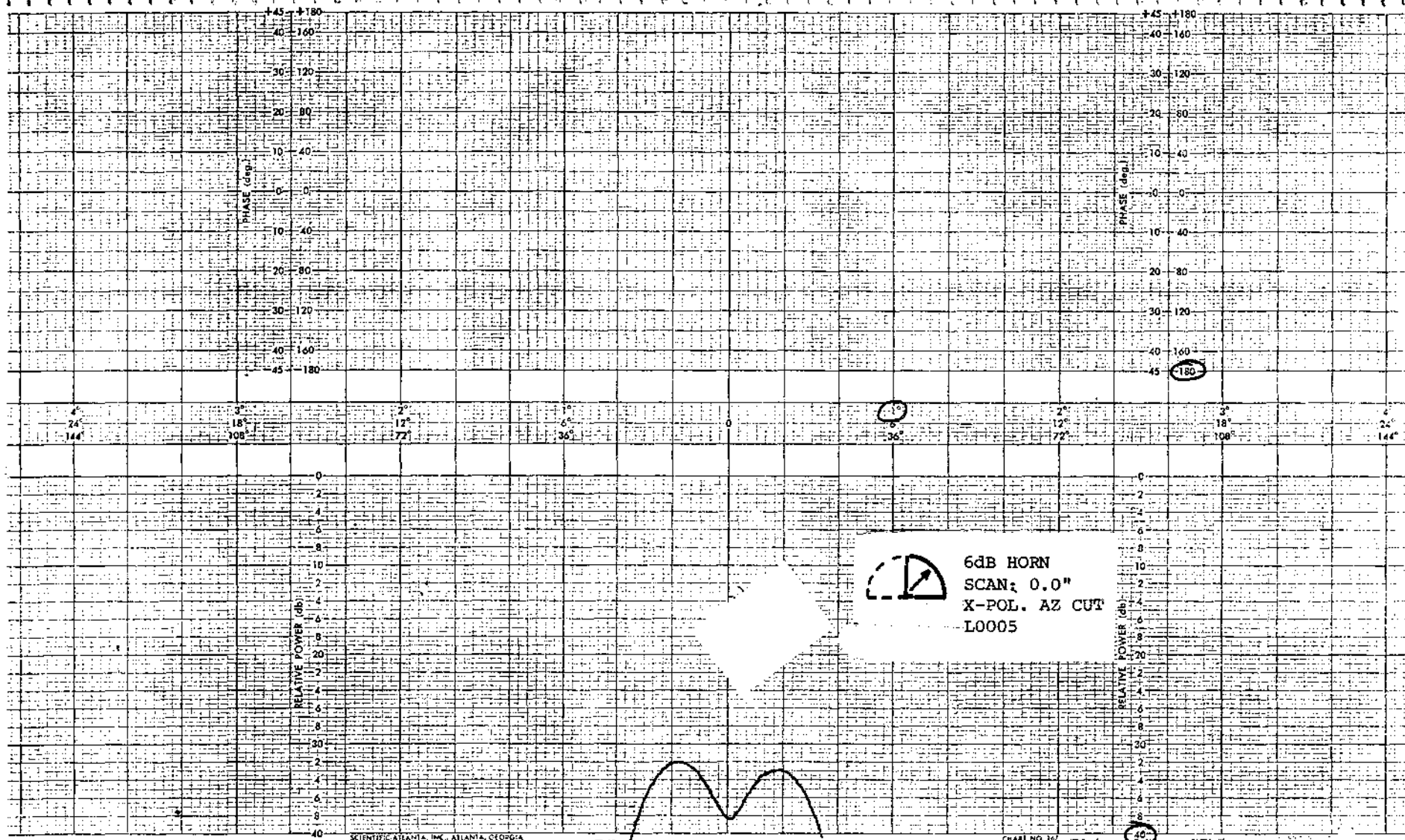
<u>CONFIGURATION</u>	<u>HORN</u>	<u>SCAN</u>	<u>POL.</u>	<u>PK. GAIN</u>	<u>PATTERN</u>	<u>FILE NAME</u>	<u>PAGE NUMBER</u>
	6 dB	0.0"	CO	50.85	+ 45° AZ	L0001	120
	"	"	CO	"	+ 5° AZ	L0002	121
	"	"	CO	"	+ 5° EL	L0003	122
	"	"	X	-	+ 45° AZ	L0004	123
	"	"	X	-	+ 5° AZ	L0005	124
	"	"	X	-	+ 5° EL	L0006	125
	6 dB	4.5"	CO	50.55	+ 45° AZ	L0027	126
	"	"	CO	"	+ 5° AZ	L0025	127
	"	"	CO	"	+ 5° EL	L0026	128
	"	"	X	-	+ 45° AZ	L0030	129
	"	"	X	-	+ 5° AZ	L0028	130
	"	"	X	-	+ 5° EL	L0029	131
	6 dB	0.0"	CO	35.25	+ 45° AZ	L0074	132
	"	"	CO	"	+ 5° AZ	L0073	133
	"	"	CO	"	+ 5° EL	L0075	134
	"	"	X	-	+ 45° AZ	L0078	135
	"	"	X	-	+ 5° AZ	L0077	136
	"	"	X	-	+ 5° EL	L0076	137
	6 dB	0.0"	CO	34.65	+ 45° AZ	L0079	138
	"	"	CO	"	+ 5° AZ	L0080	139
	"	"	CO	"	+ 5° EL	L0081	140
	"	"	X	-	+ 45° AZ	L0084	141
	"	"	X	-	+ 5° AZ	L0083	142
	"	"	X	-	+ 5° EL	L0082	143
	6 dB	0.0"	CO	50.75	+ 45° AZ	L0051	144
	"	"	CO	"	+ 5° AZ	L0049	145
	"	"	CO	"	+ 5° EL	L0050	146
	"	"	X	-	+ 45° AZ	L0054	147
	"	"	X	-	+ 5° AZ	L0052	148
	"	"	X	-	+ 5° EL	L0053	149



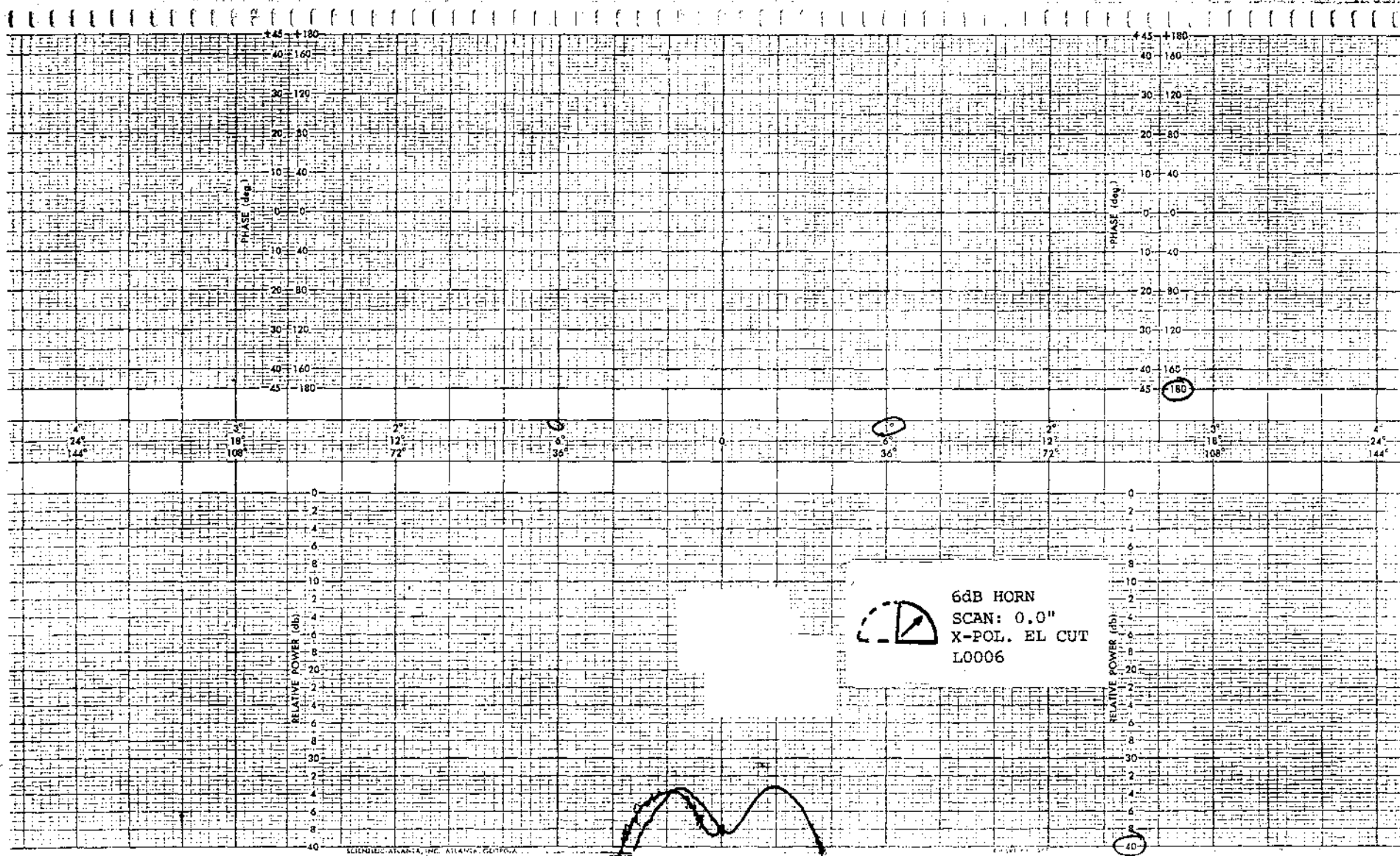




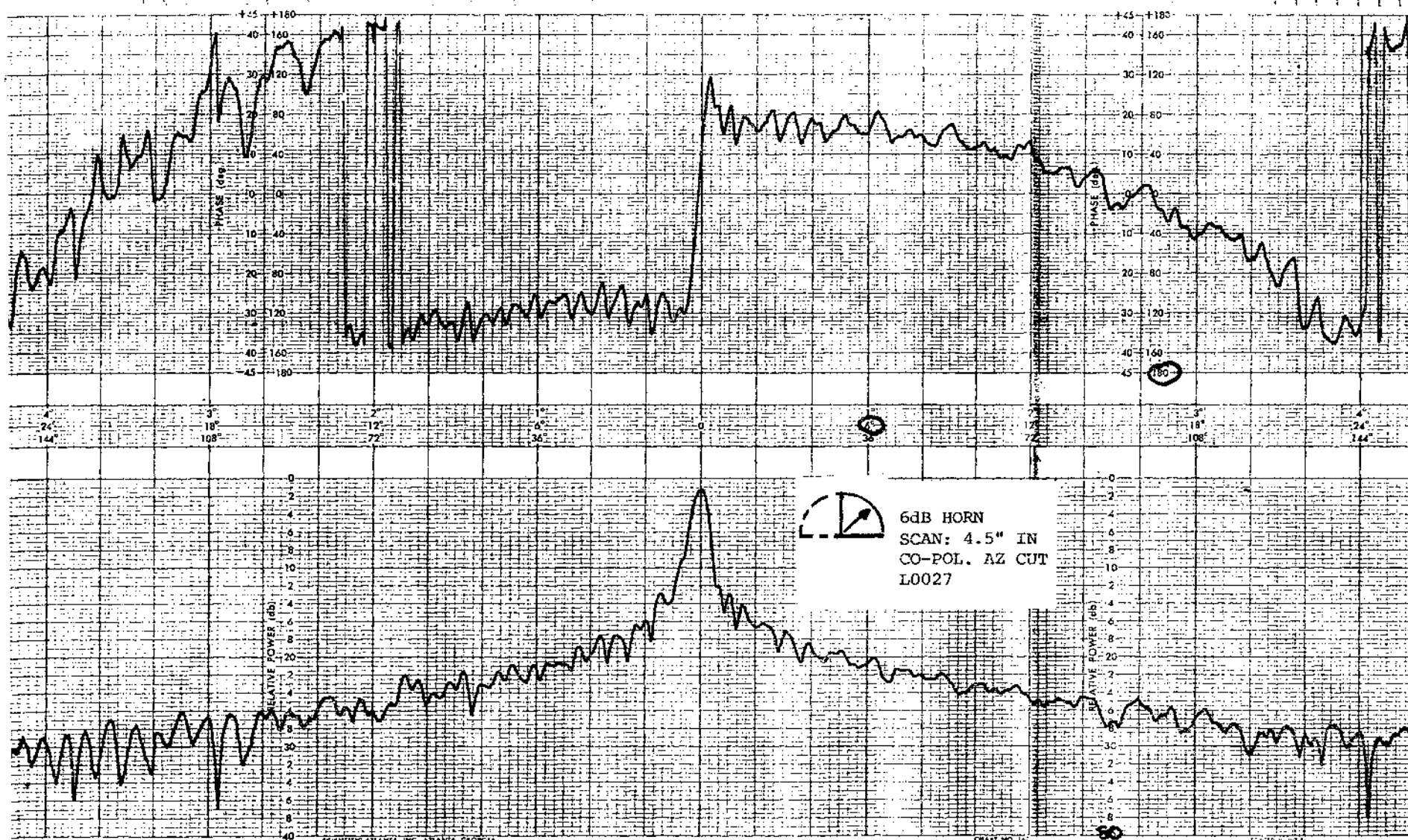


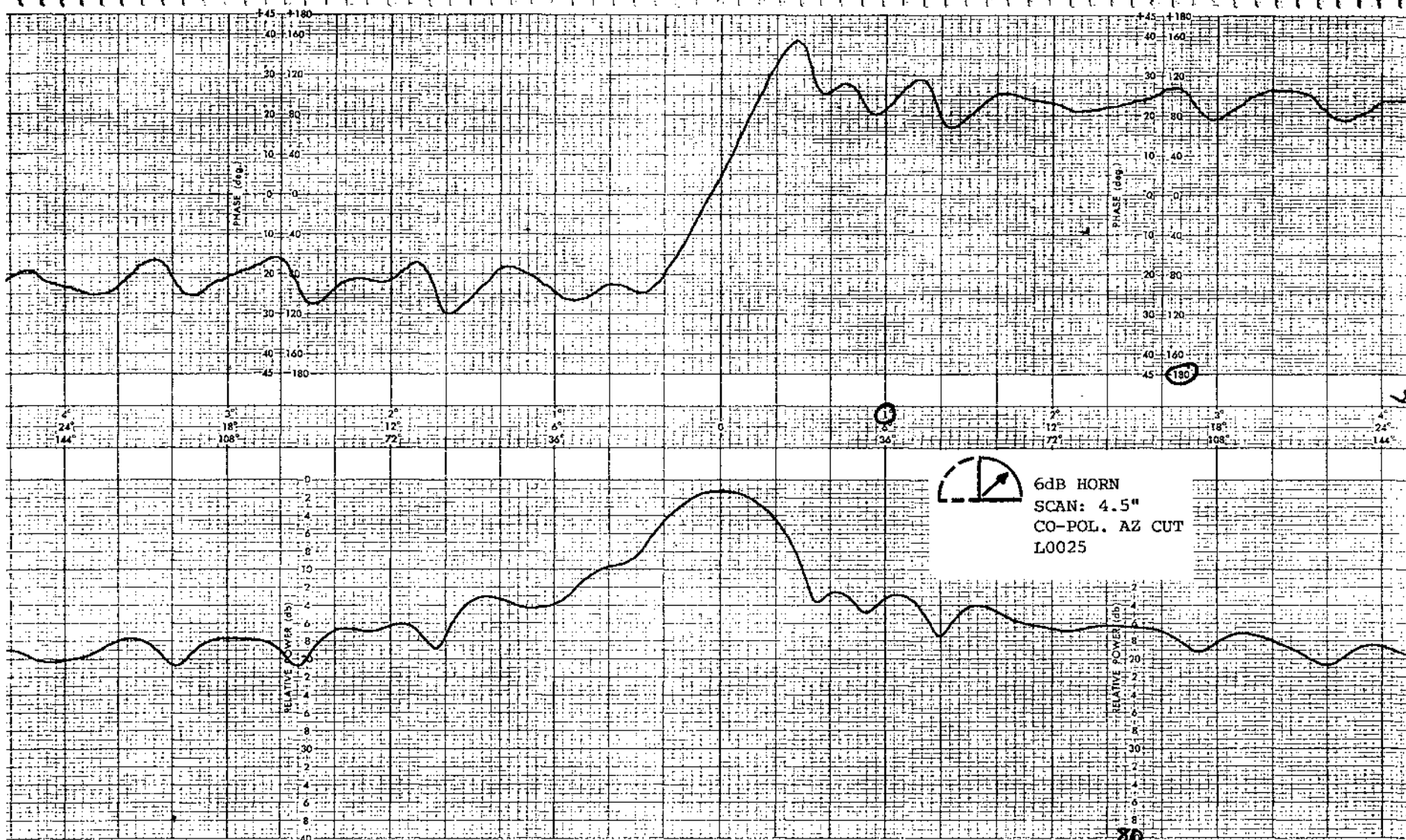


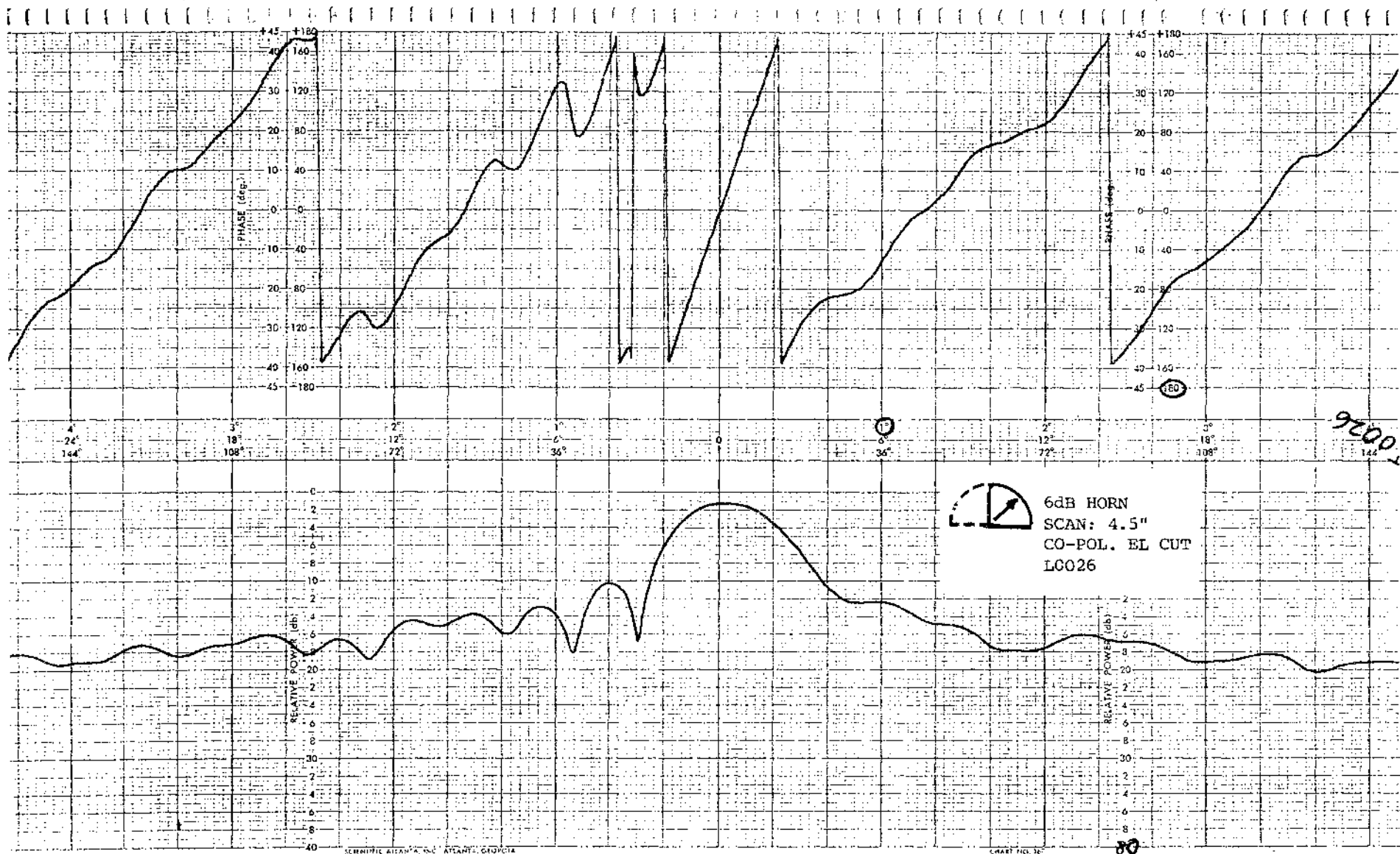


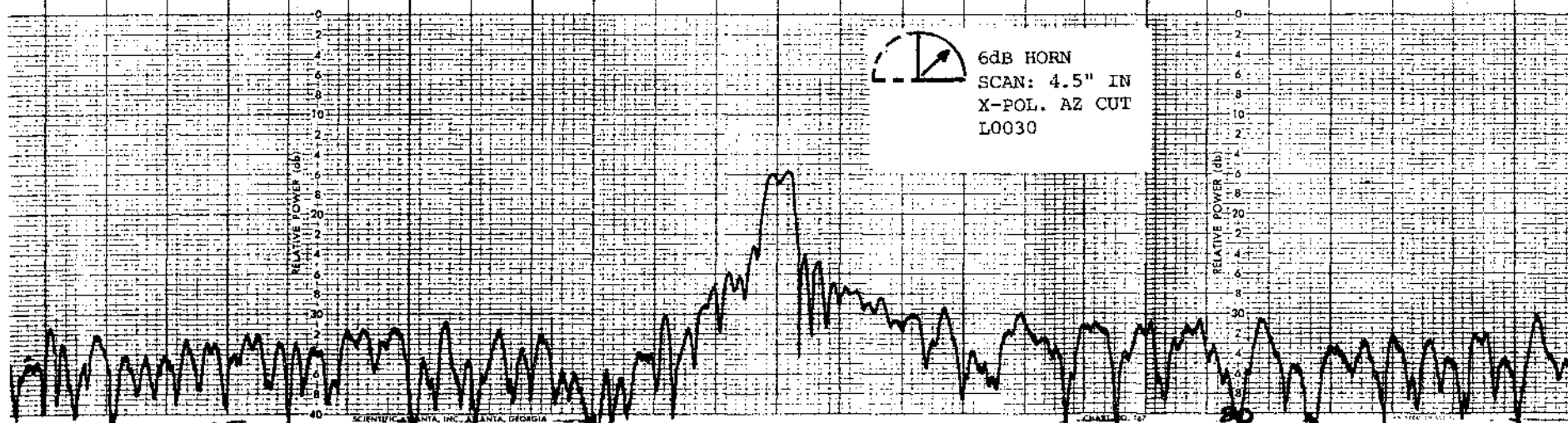
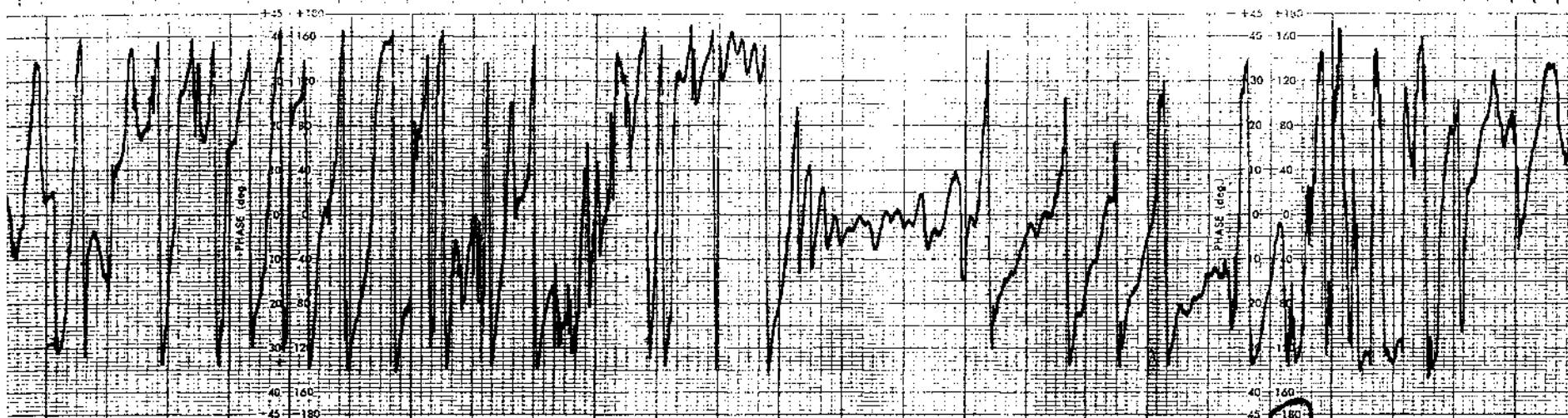


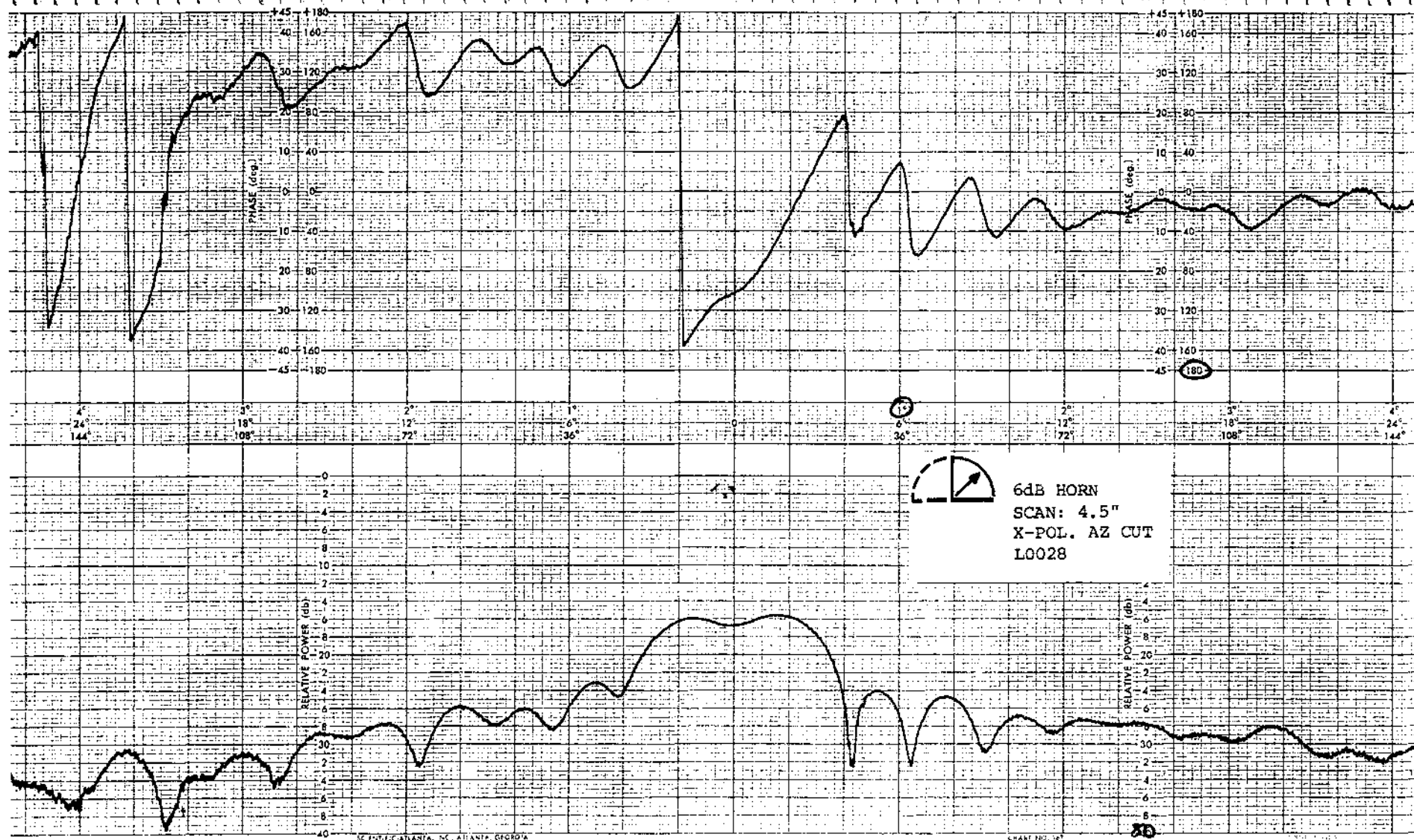


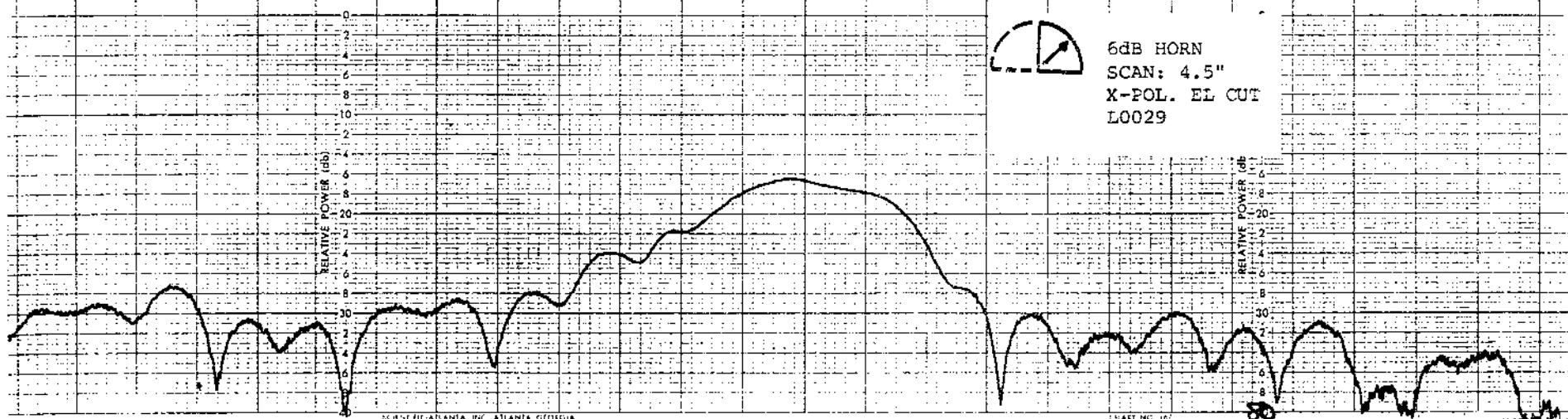
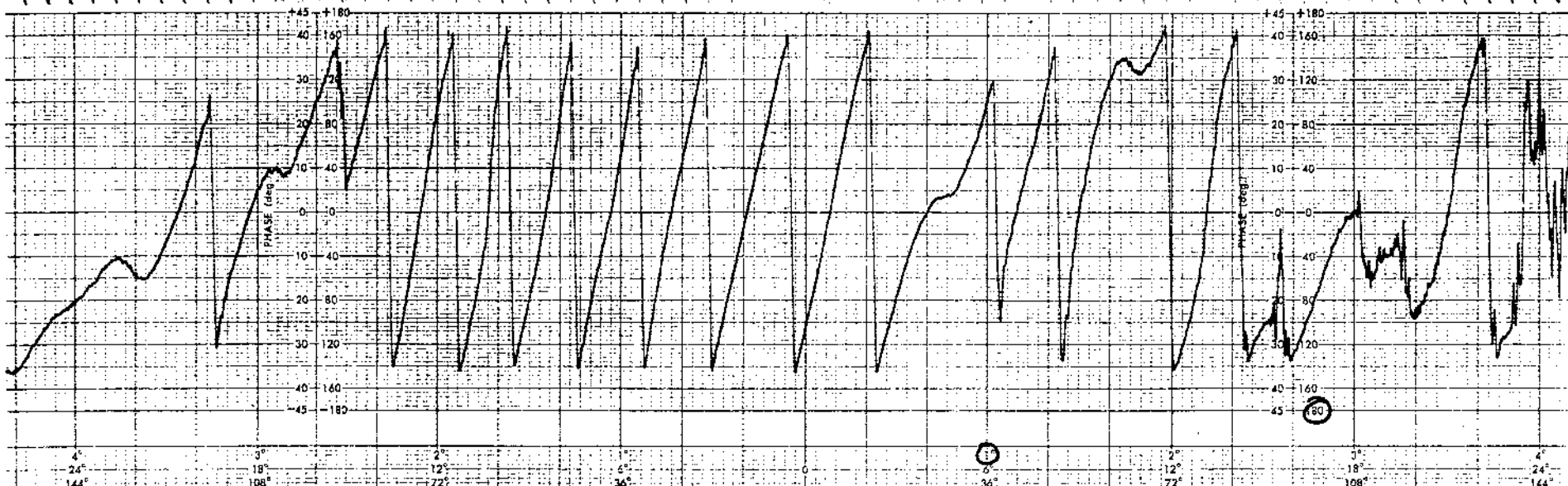










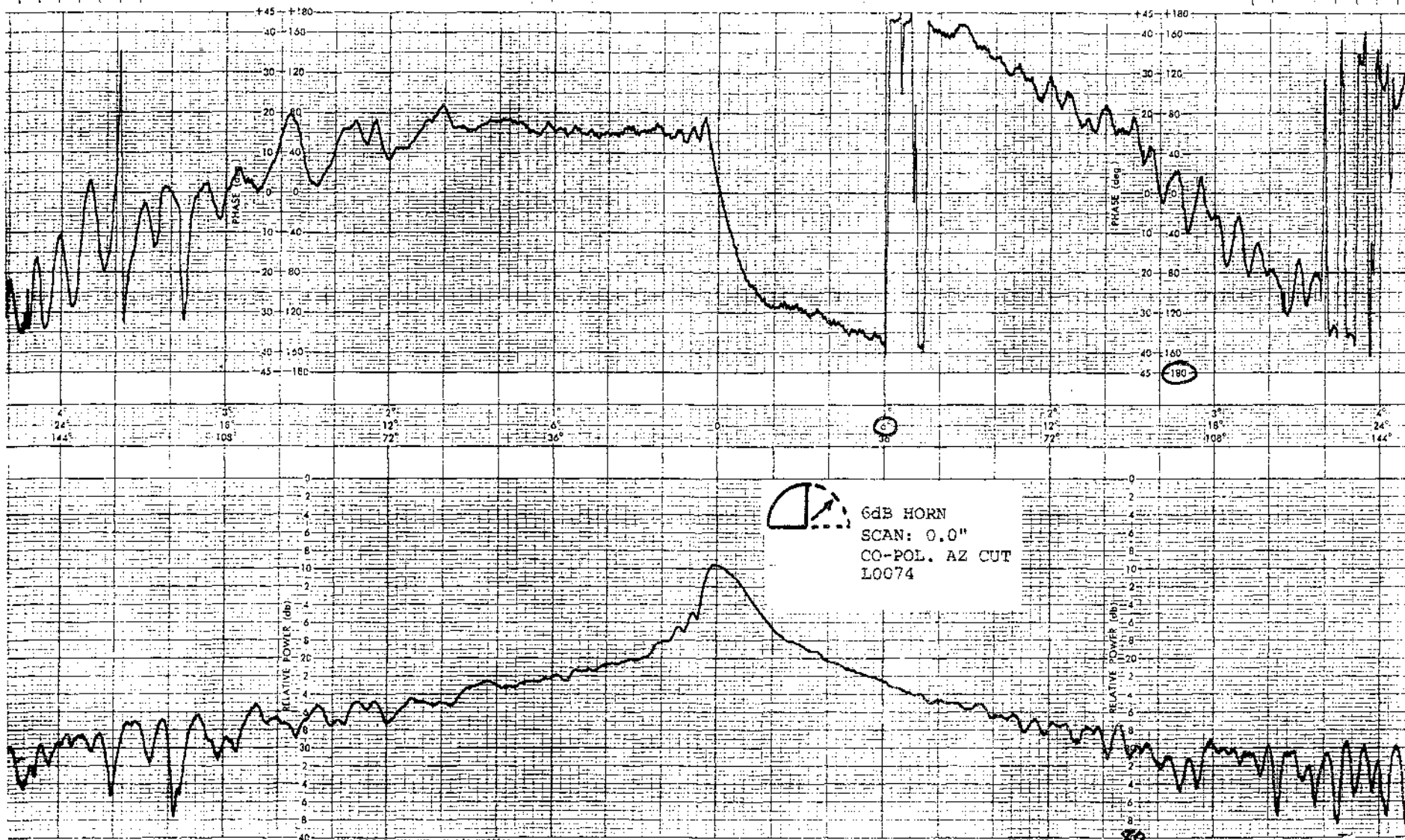


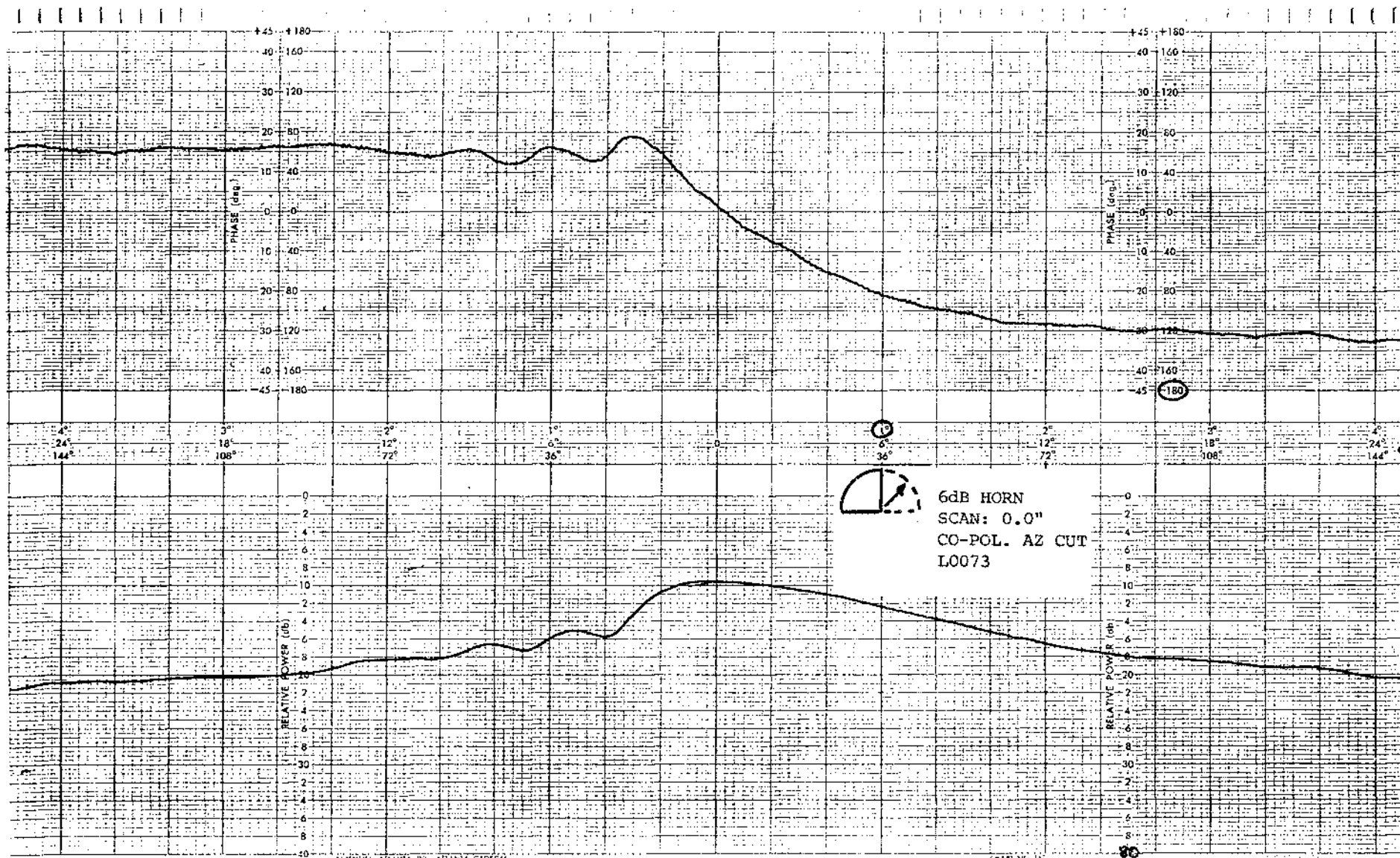
6dB HORN  
SCAN: 4.5"  
X-POL. EL CUT  
L0029

SCIENTIFIC ATLANTA, INC., ATLANTA, GEORGIA

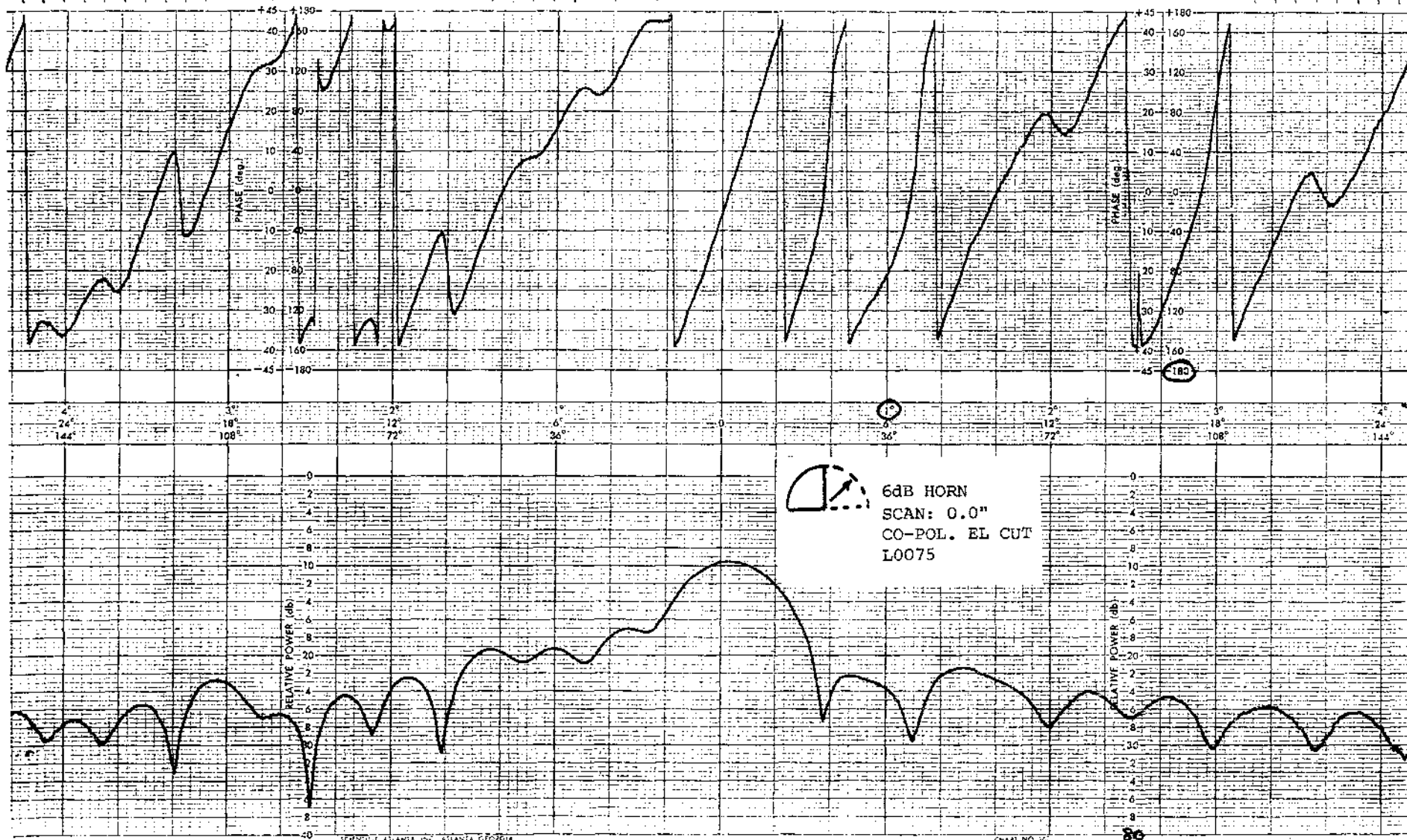
LINART INC. 197

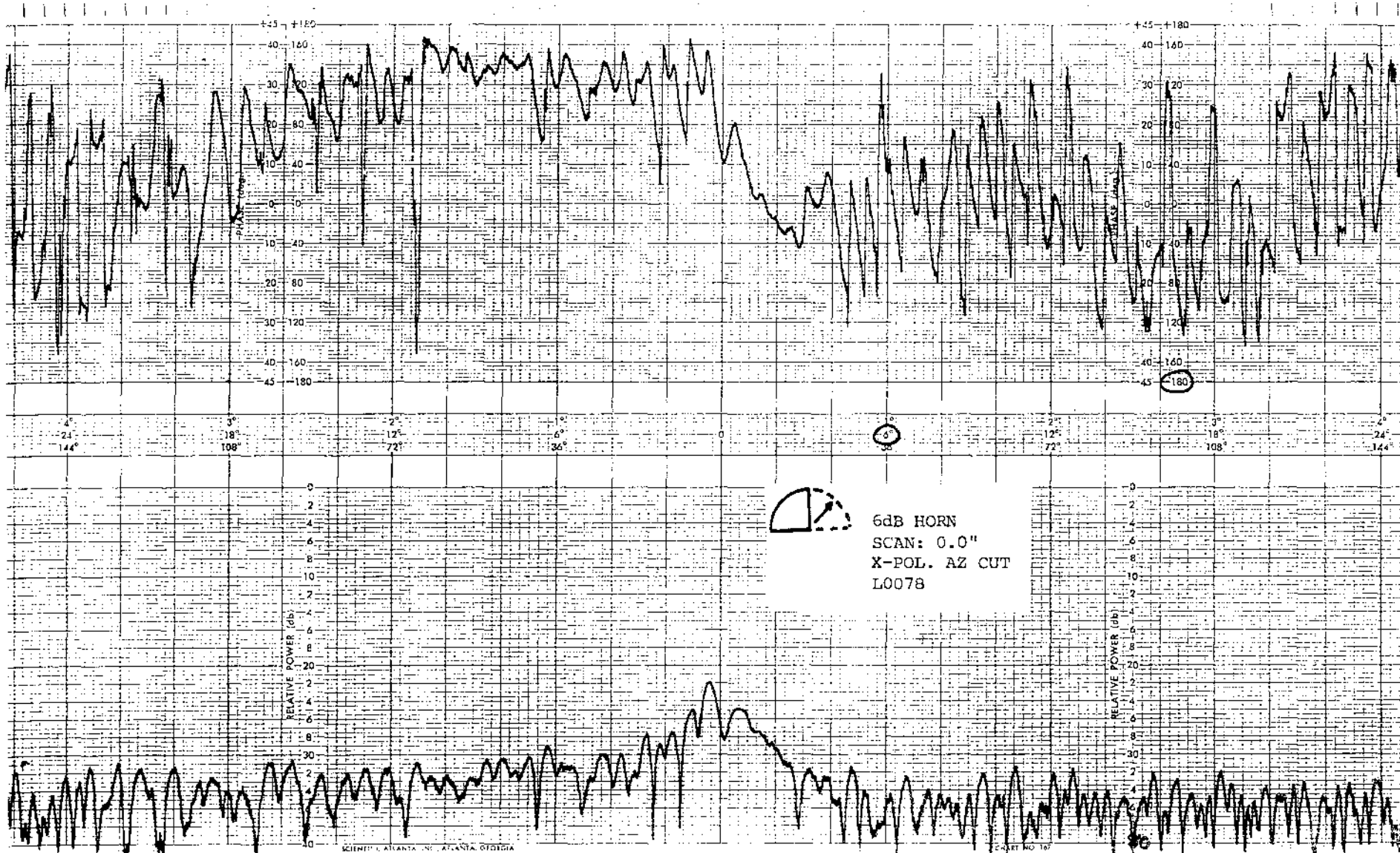


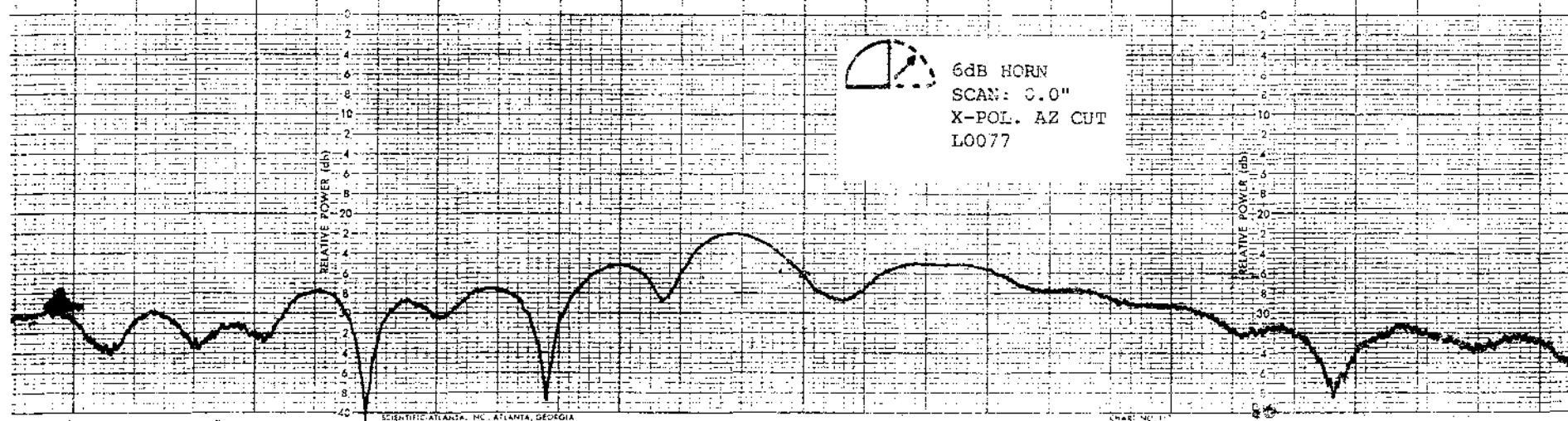
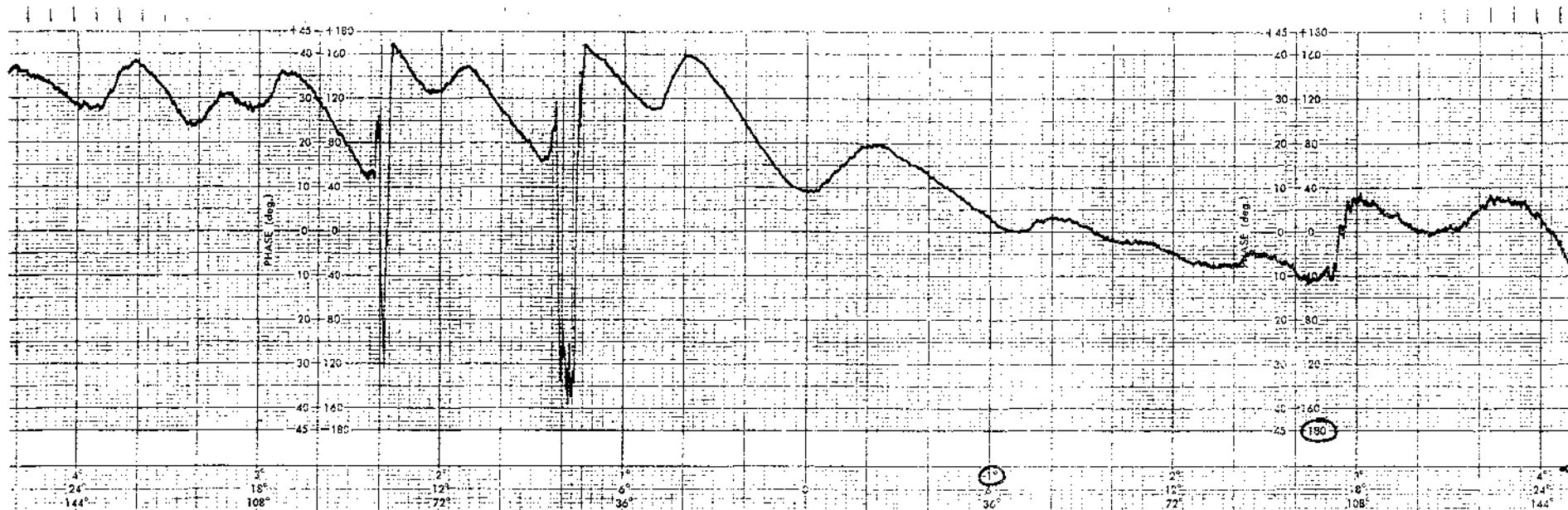


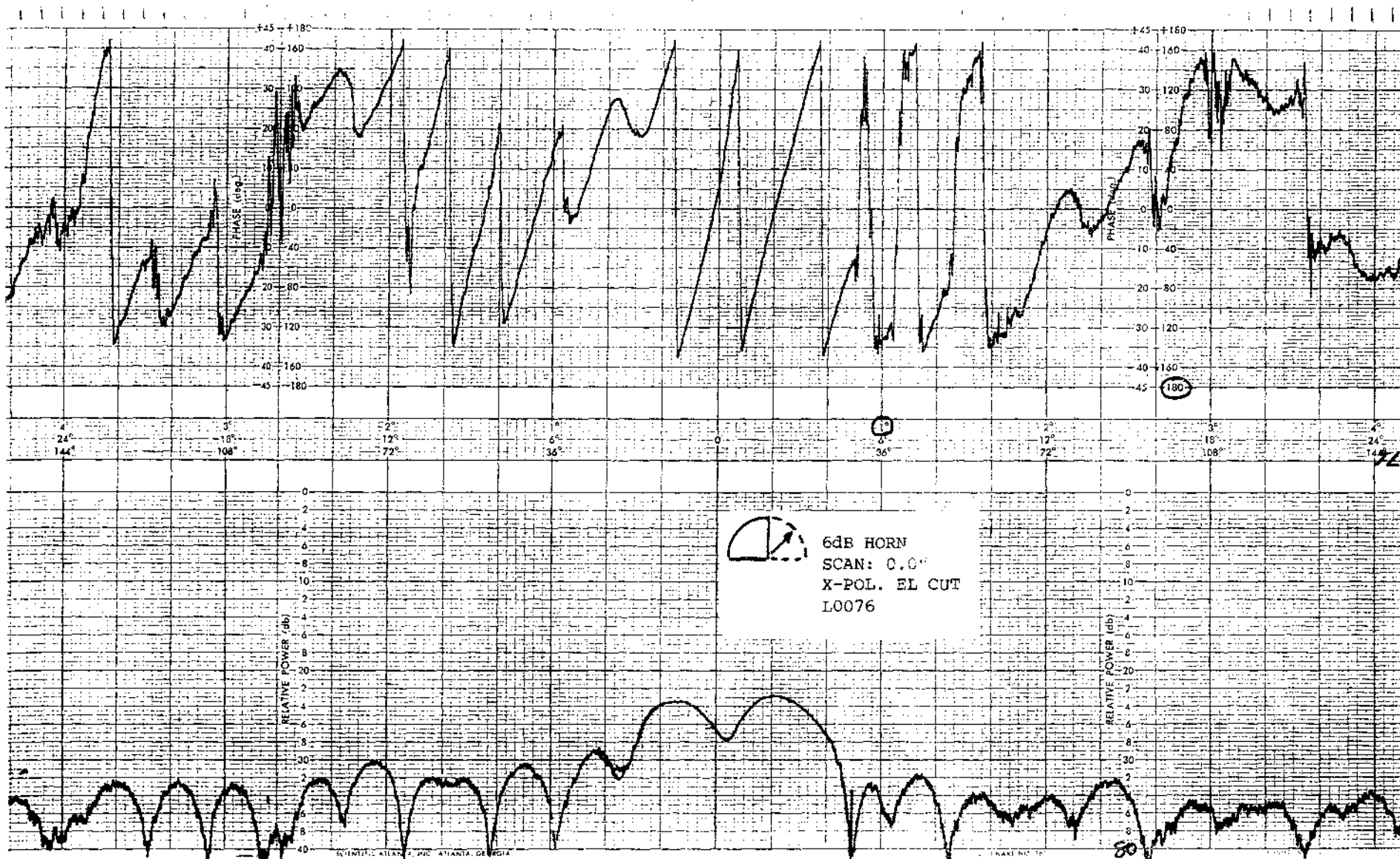


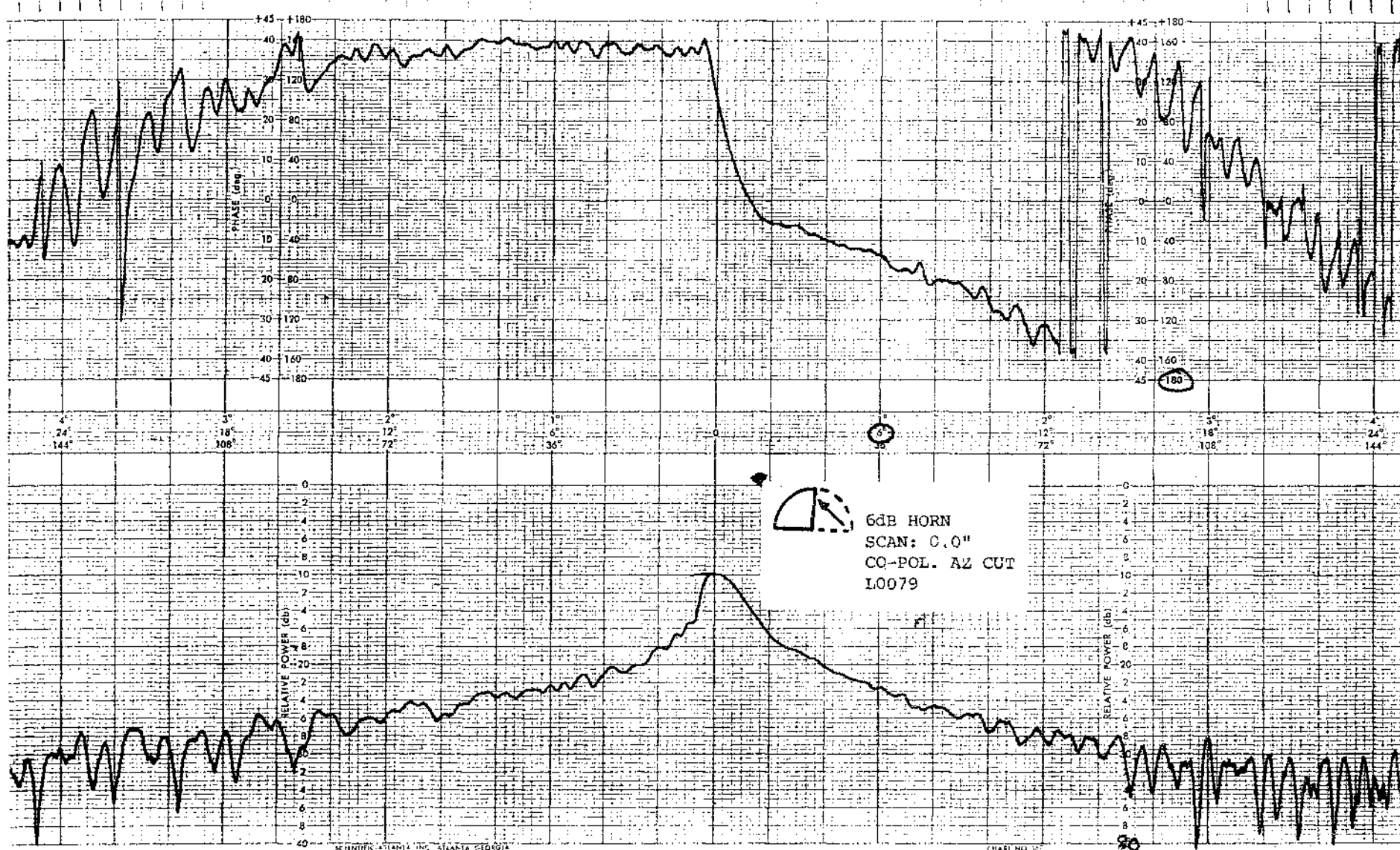


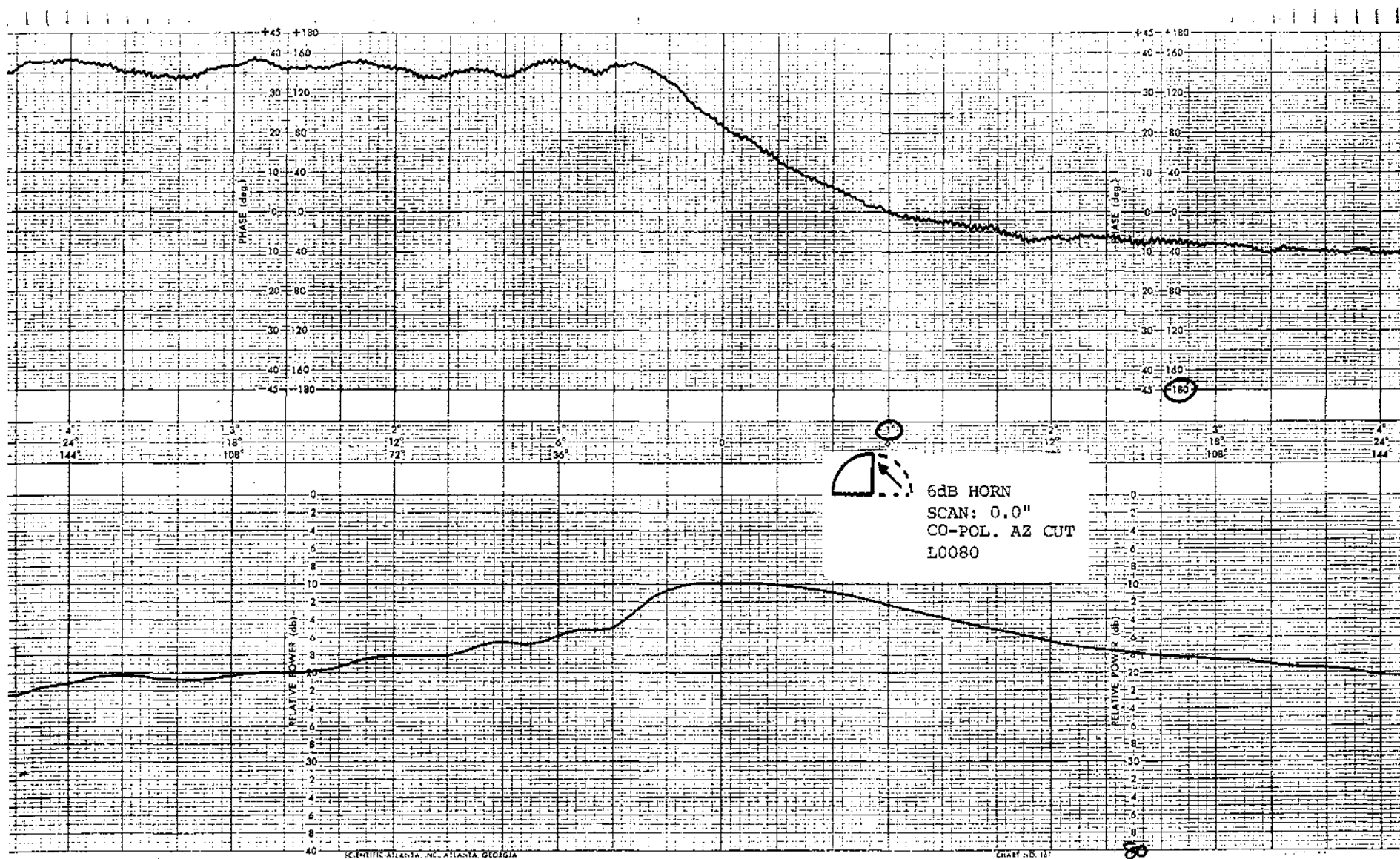




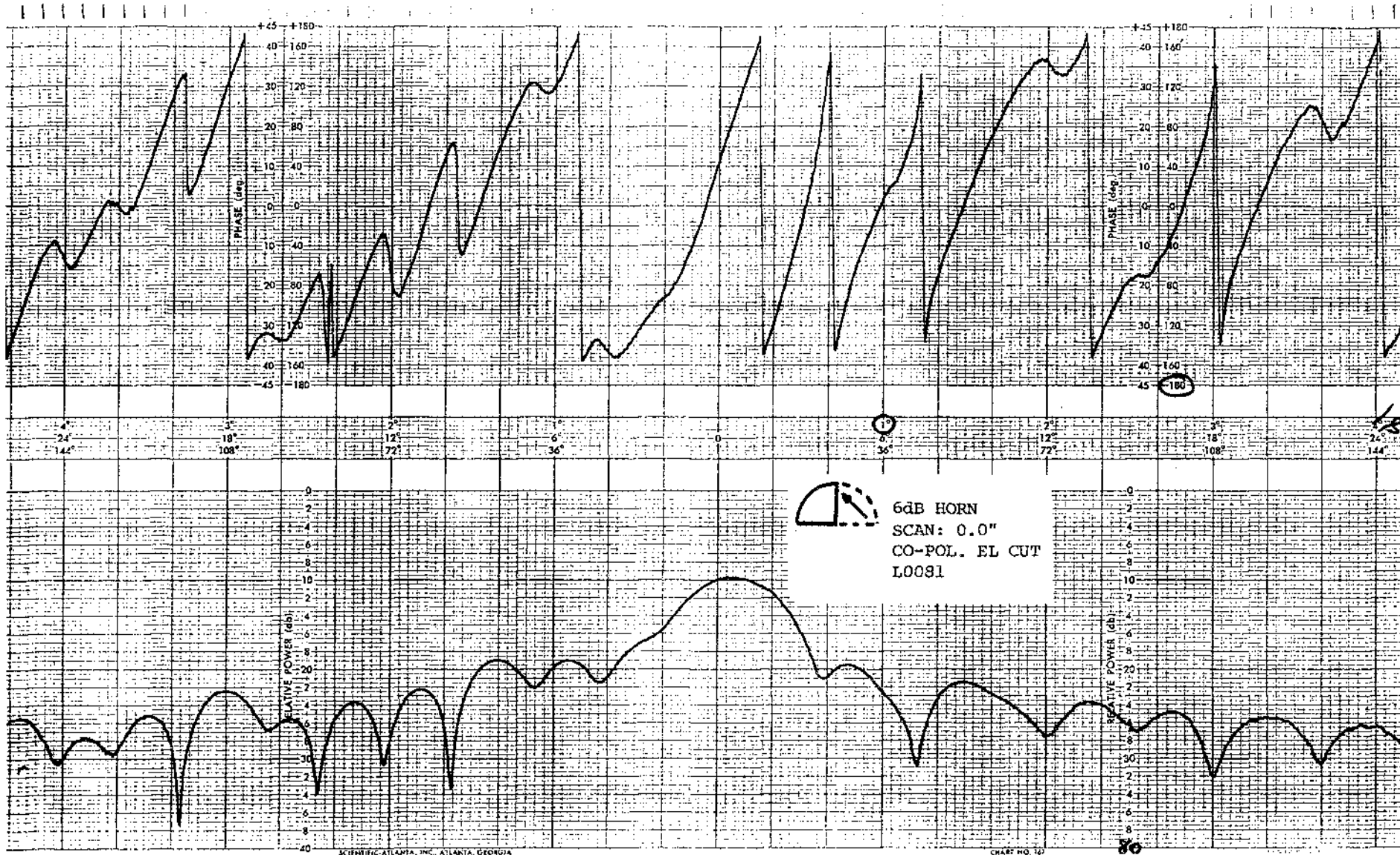


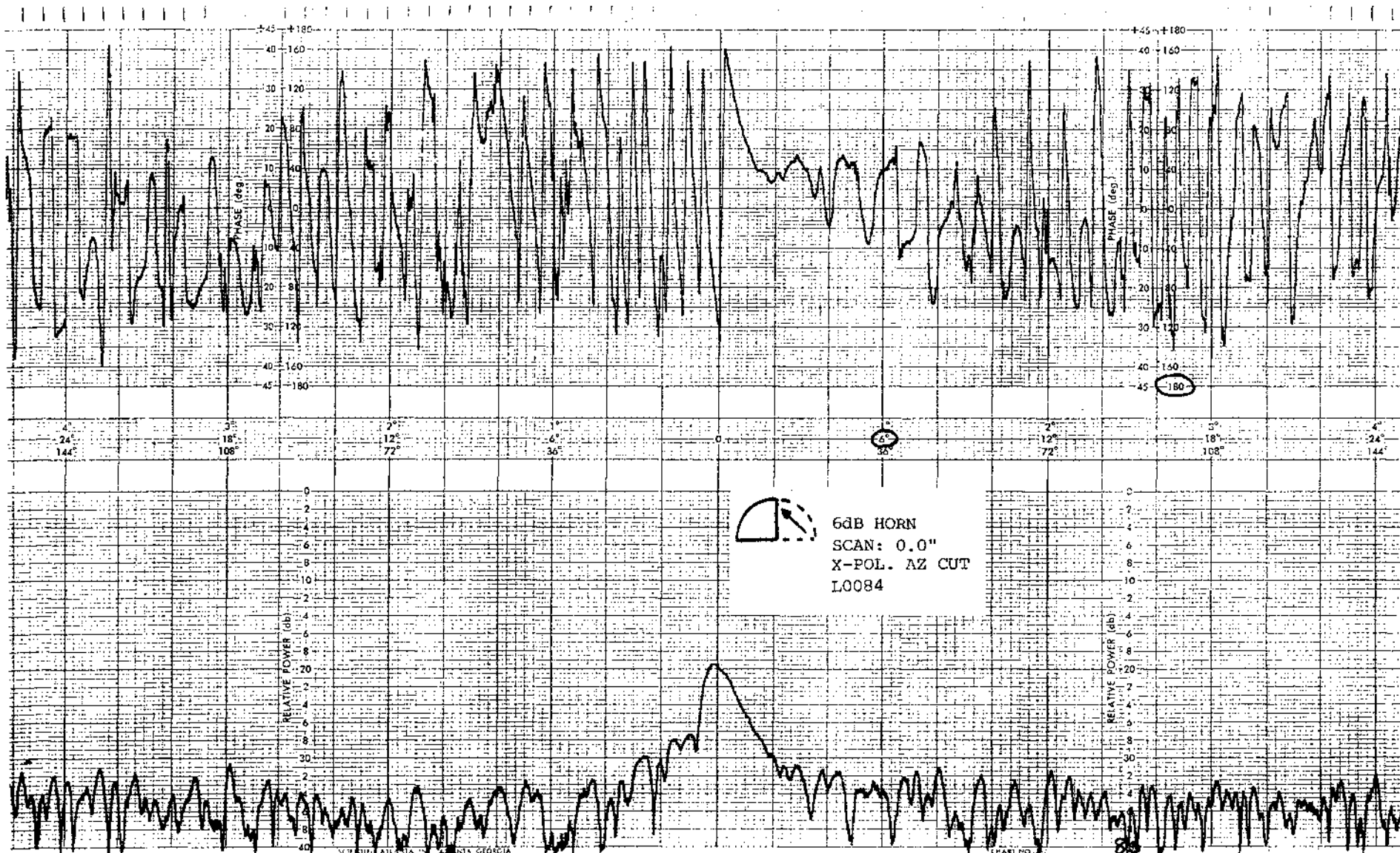




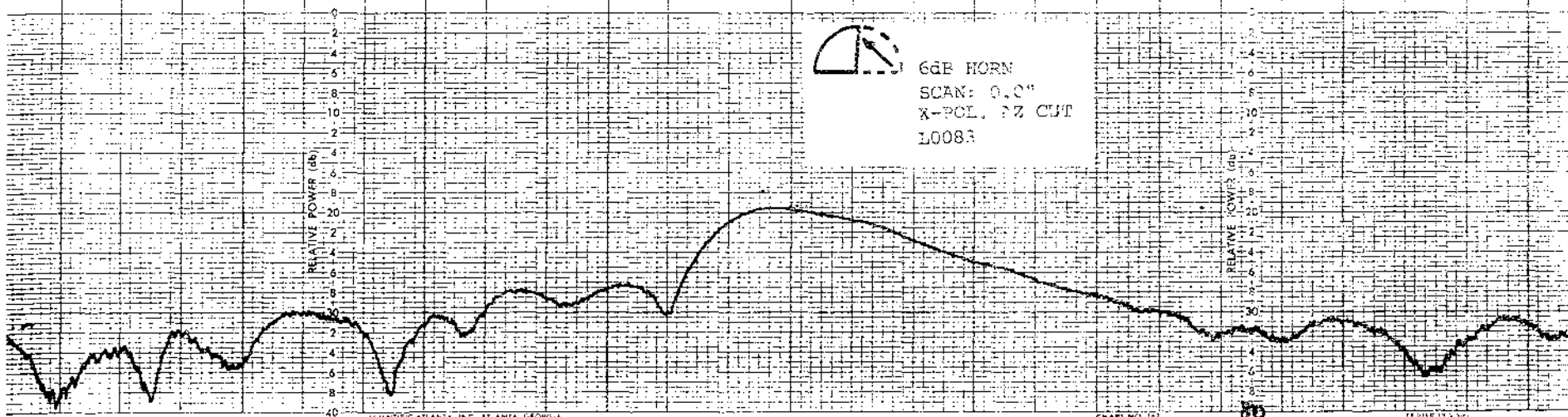
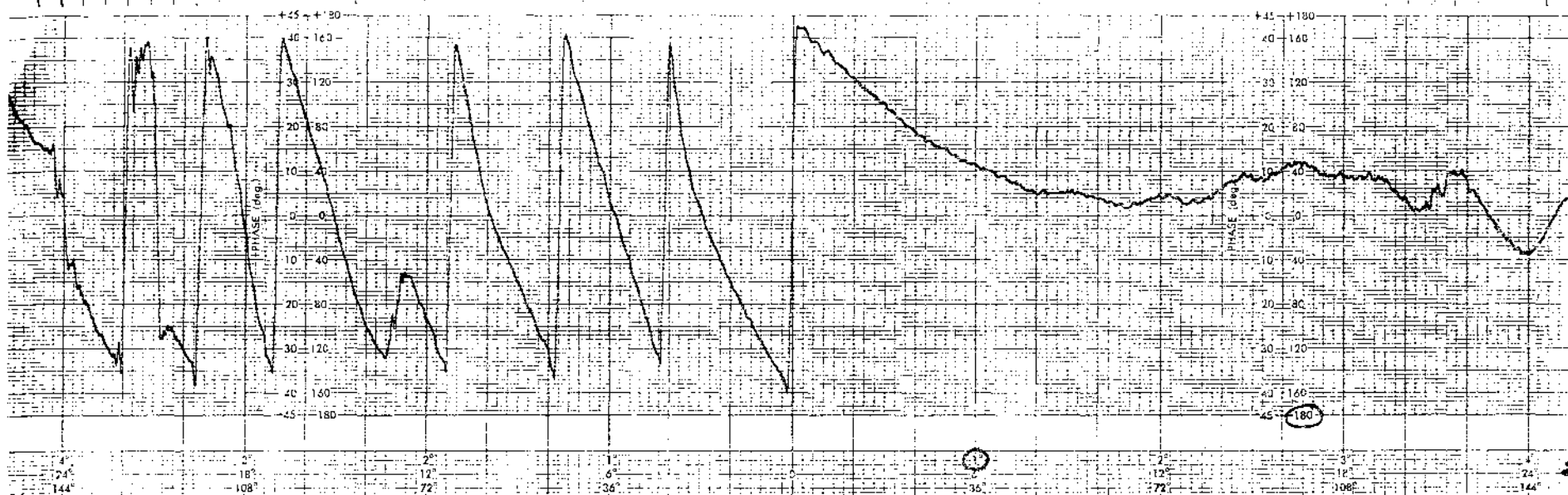








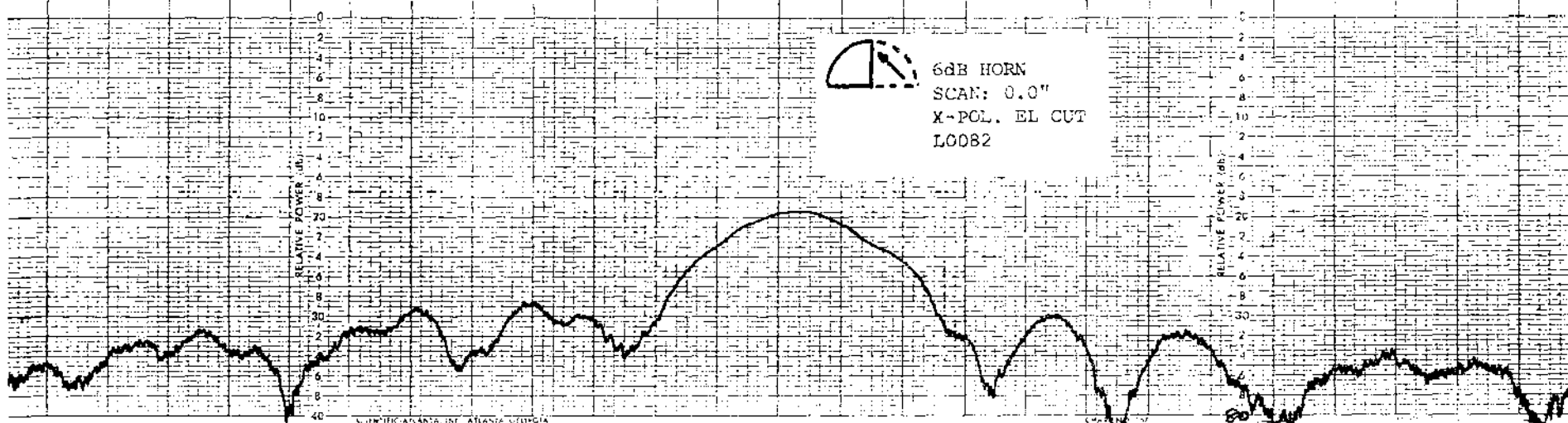
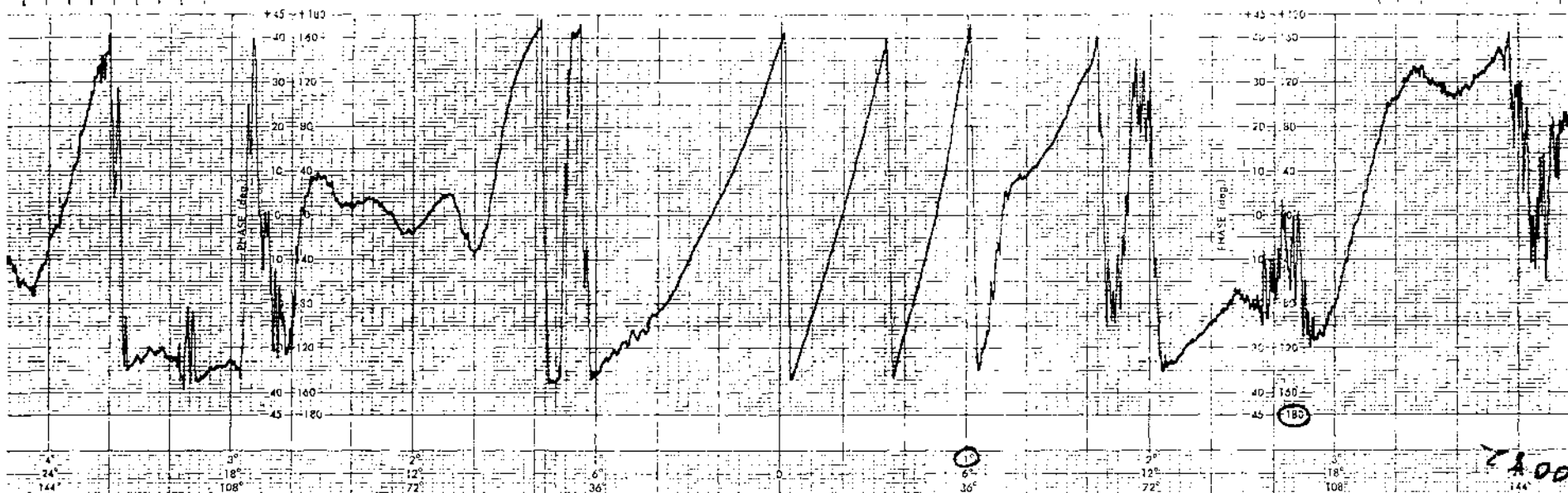


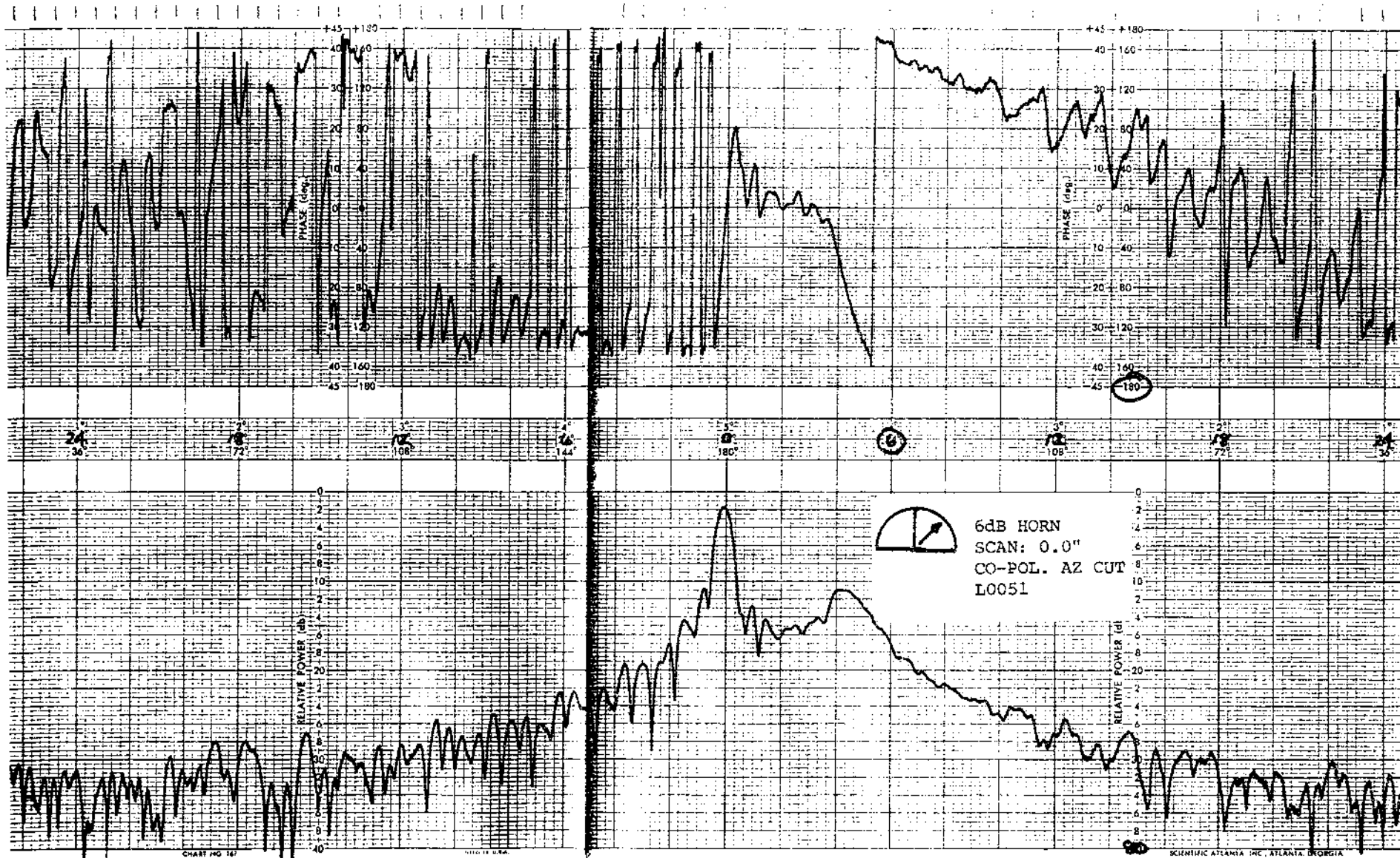


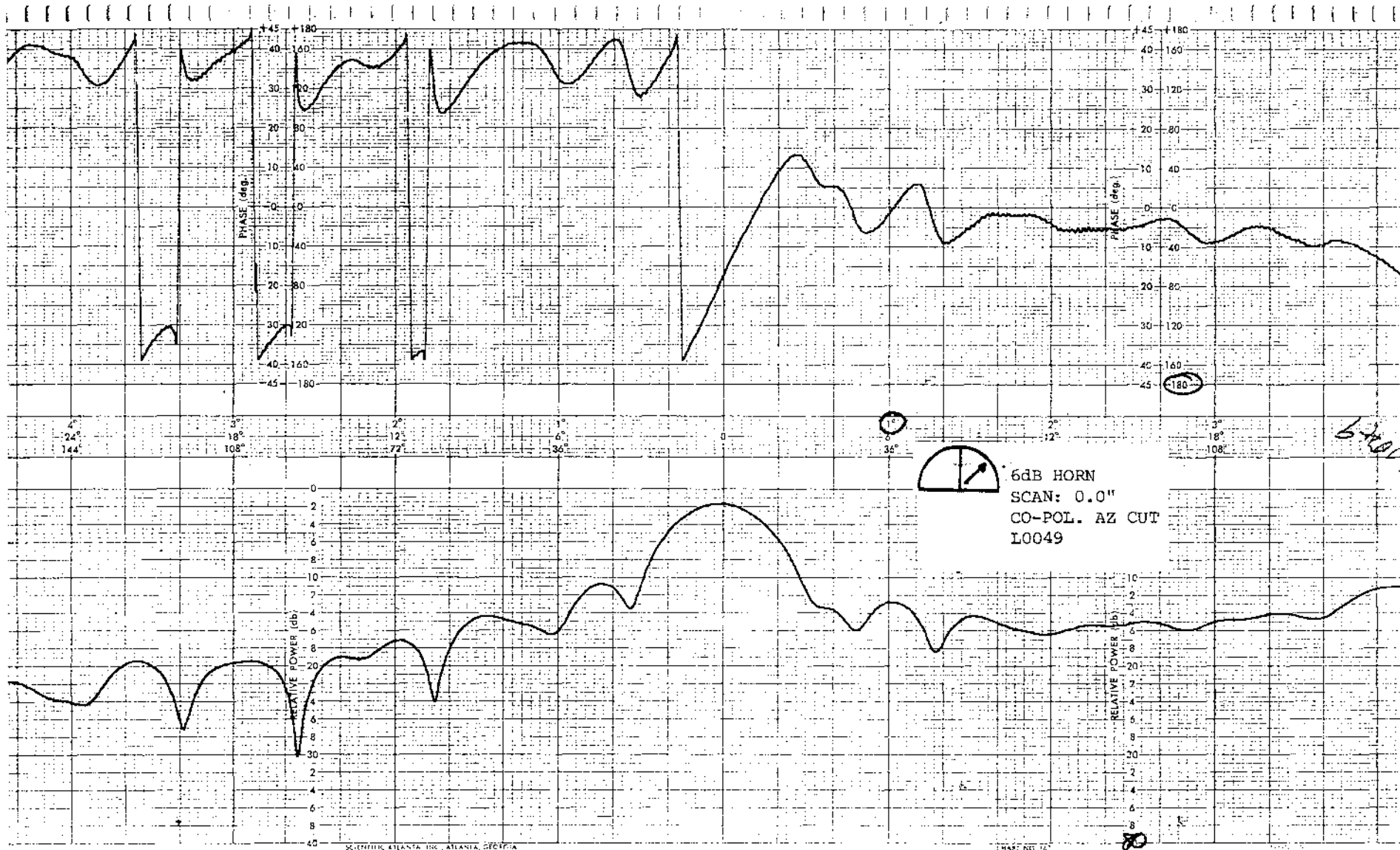
SCIENTIFIC ATLANTA INC. ATLANTA, GEORGIA

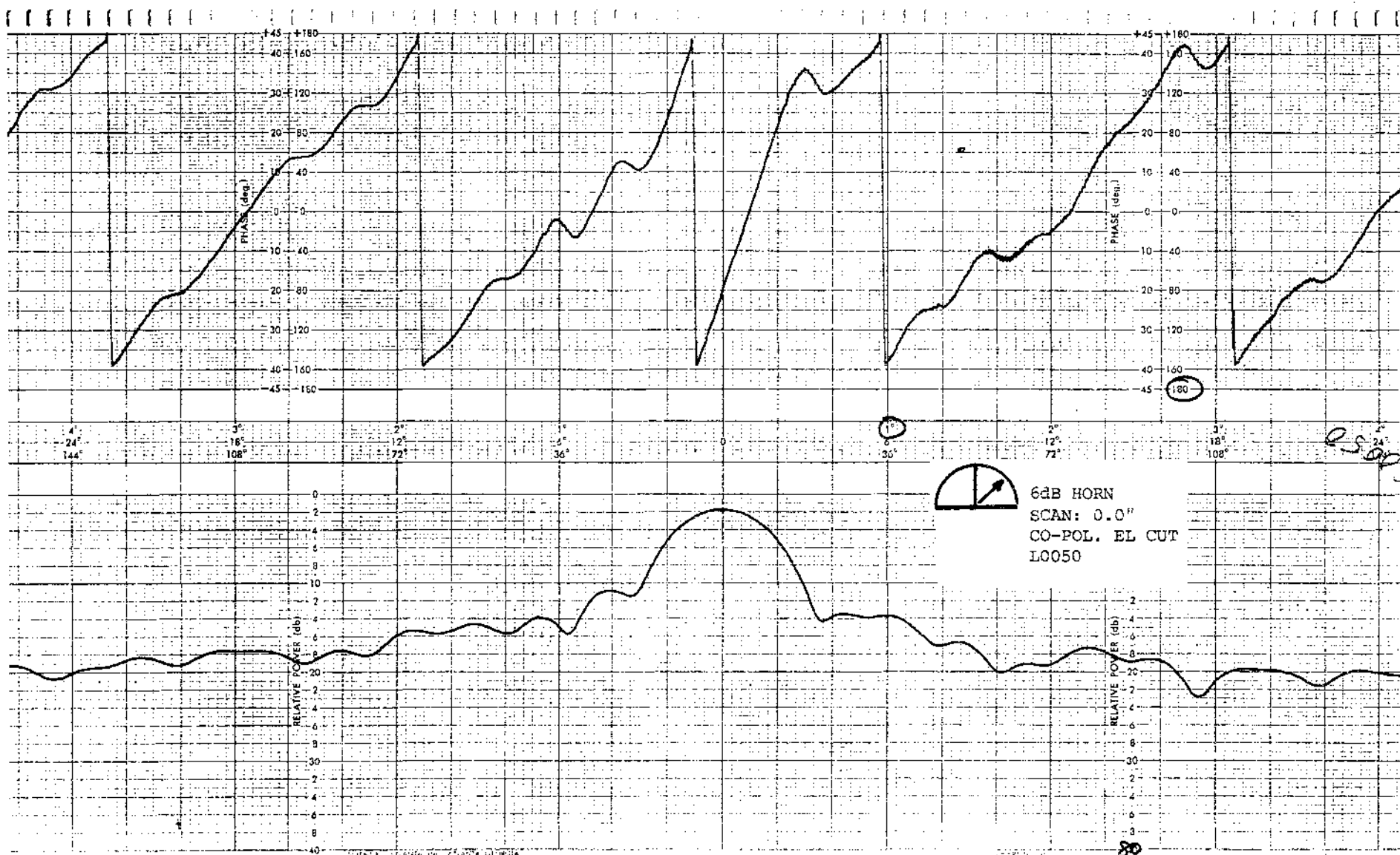
CHART NO. 157

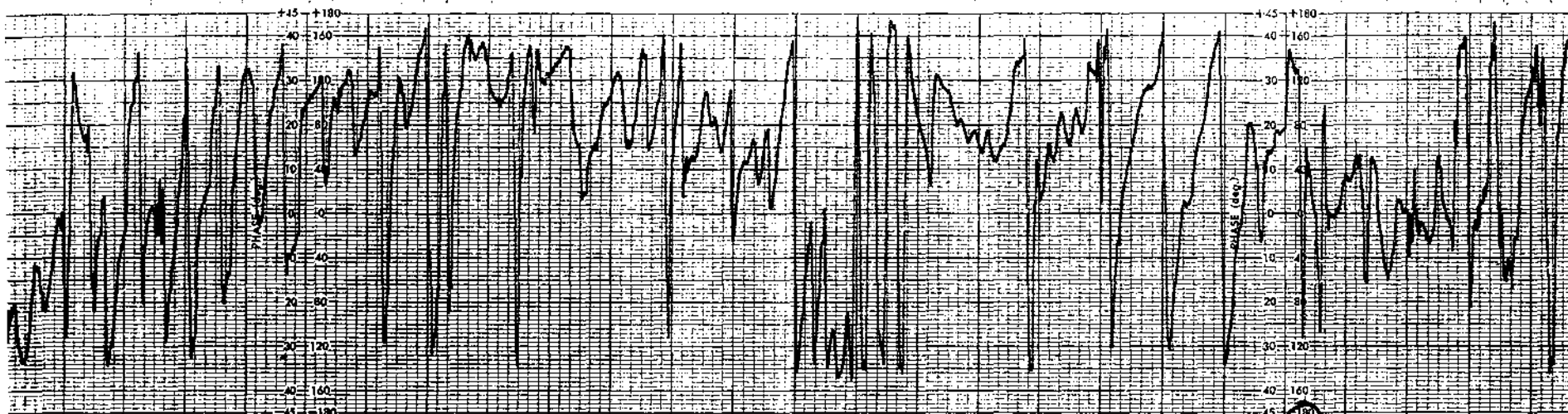
80



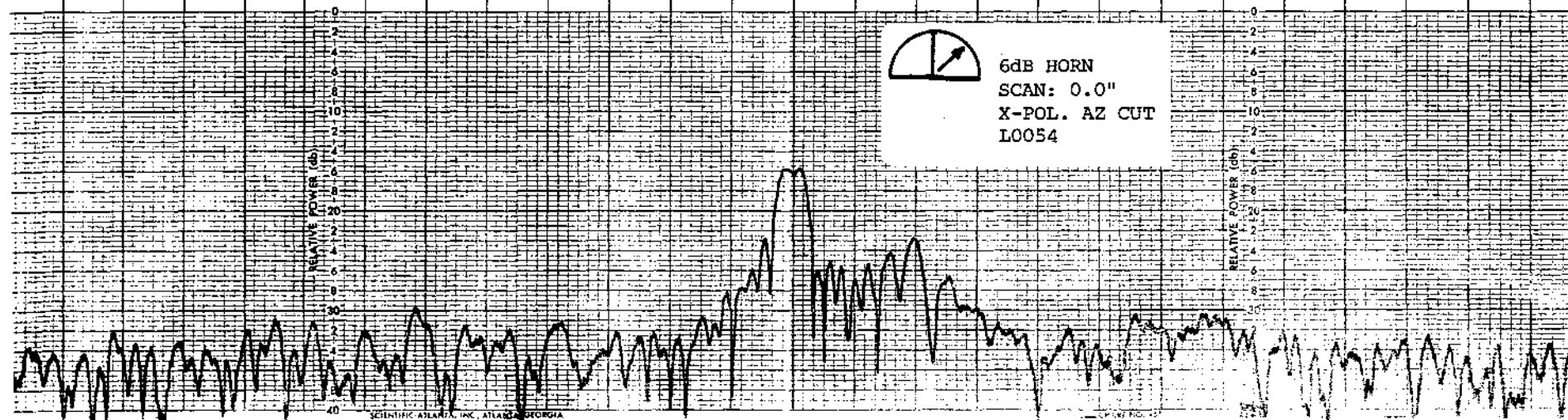




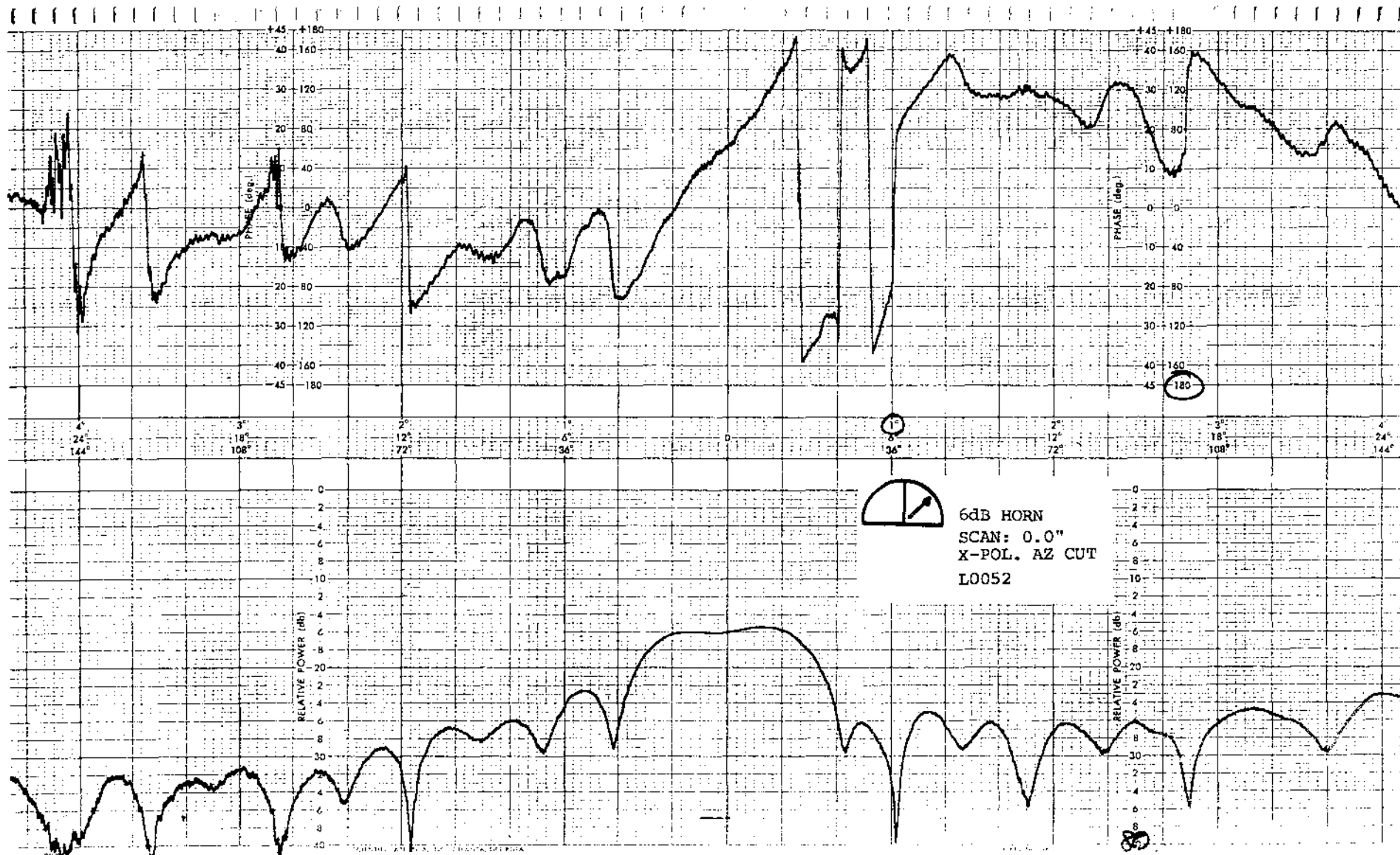


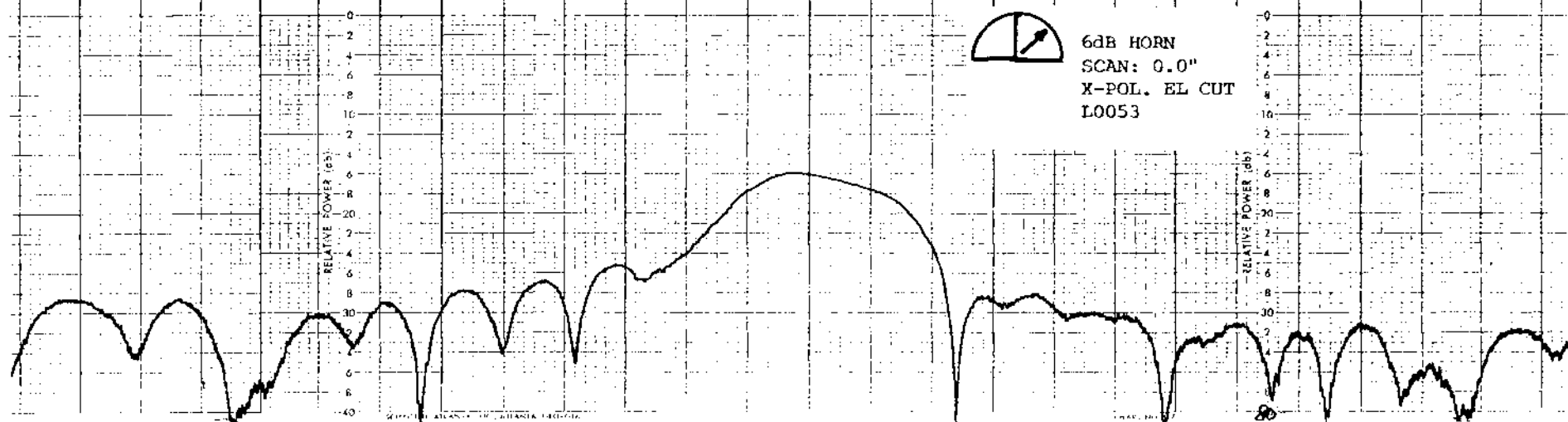
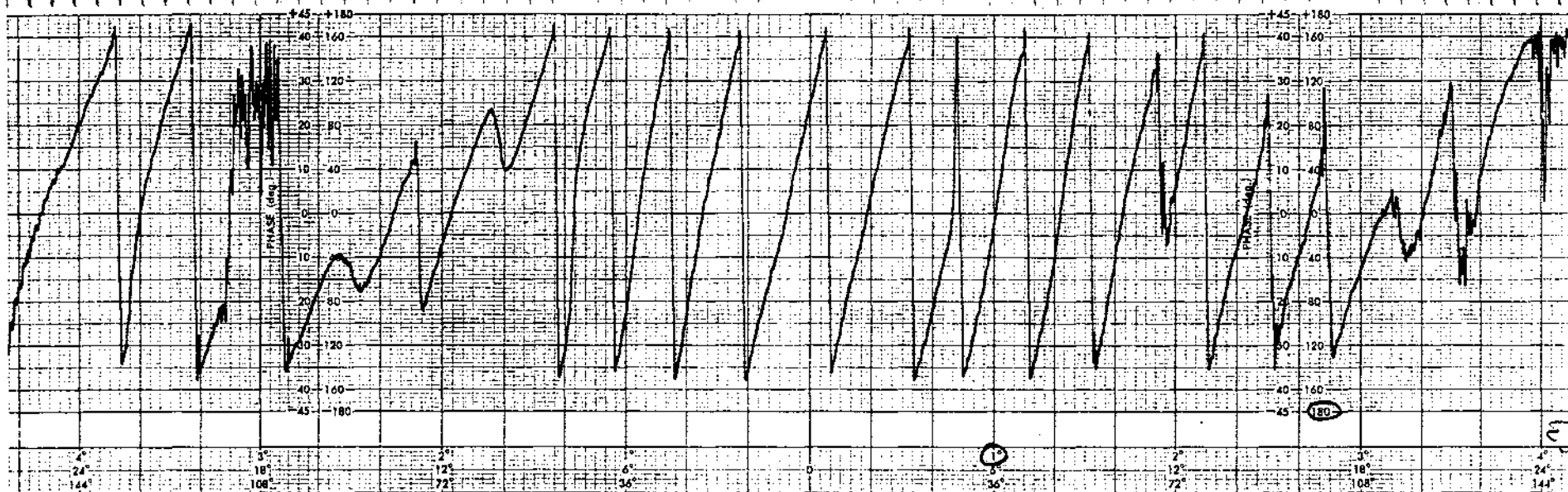


24° 18° 12° 6° 0° 6° 12° 18° 24°  
144° 108° 72° 36° 0° 36° 72° 108° 144°



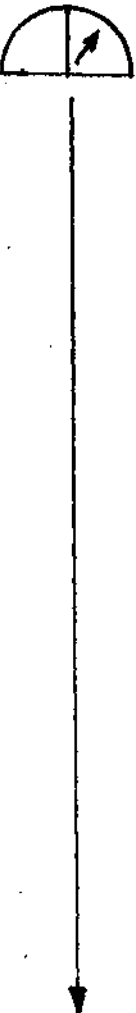



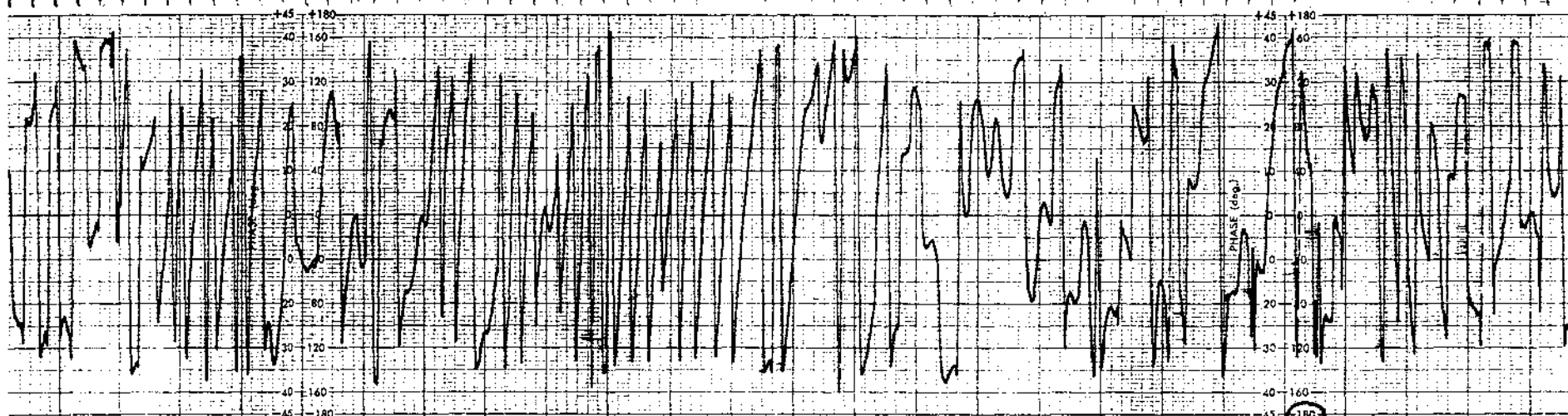




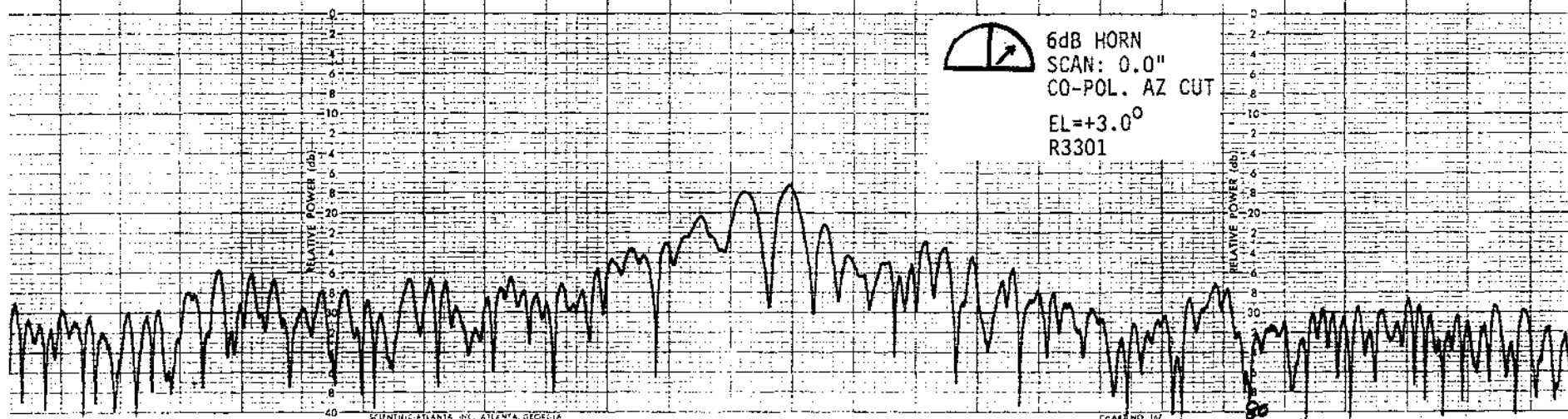


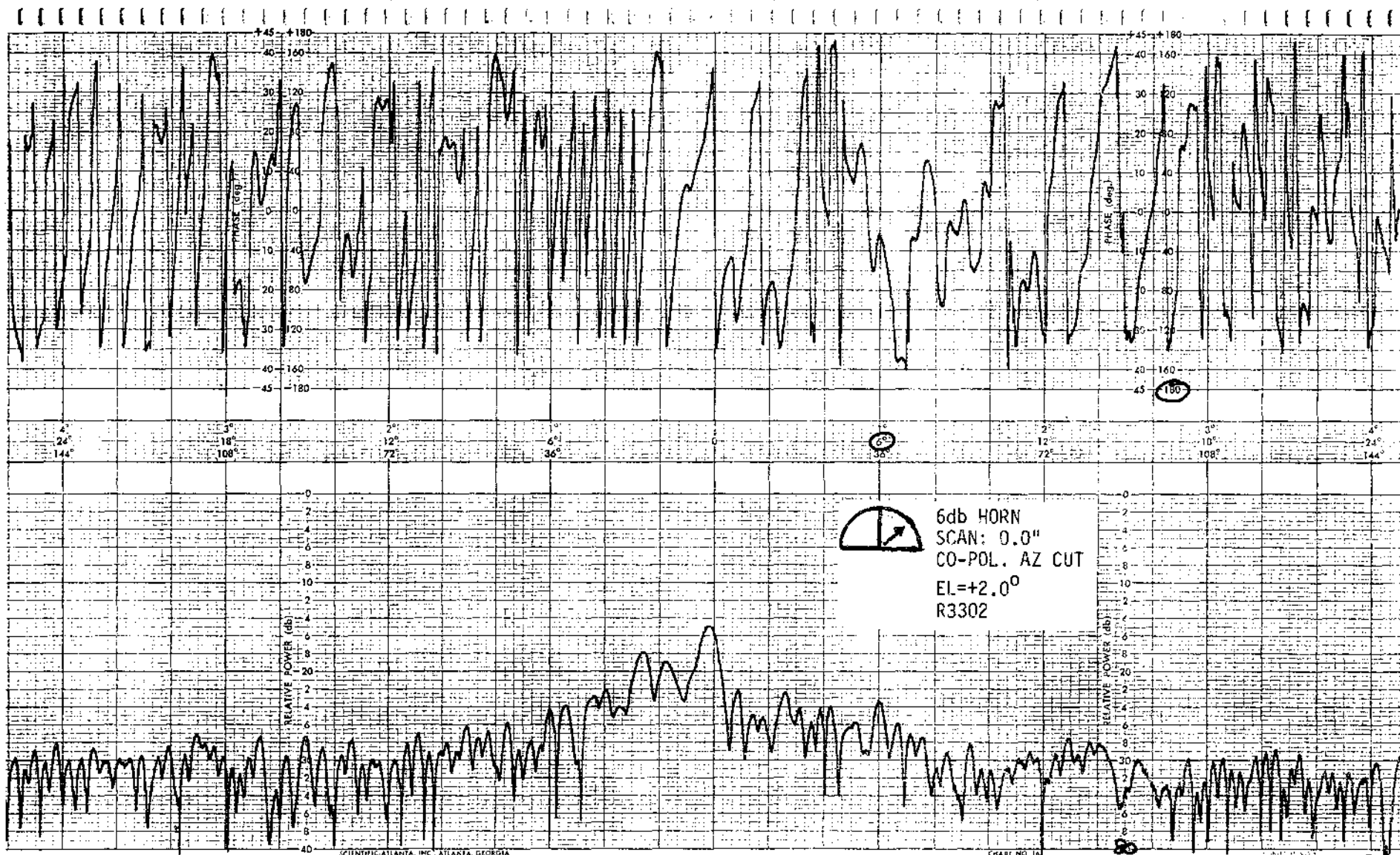
LSST - VSECONDARY PATTERN LOG

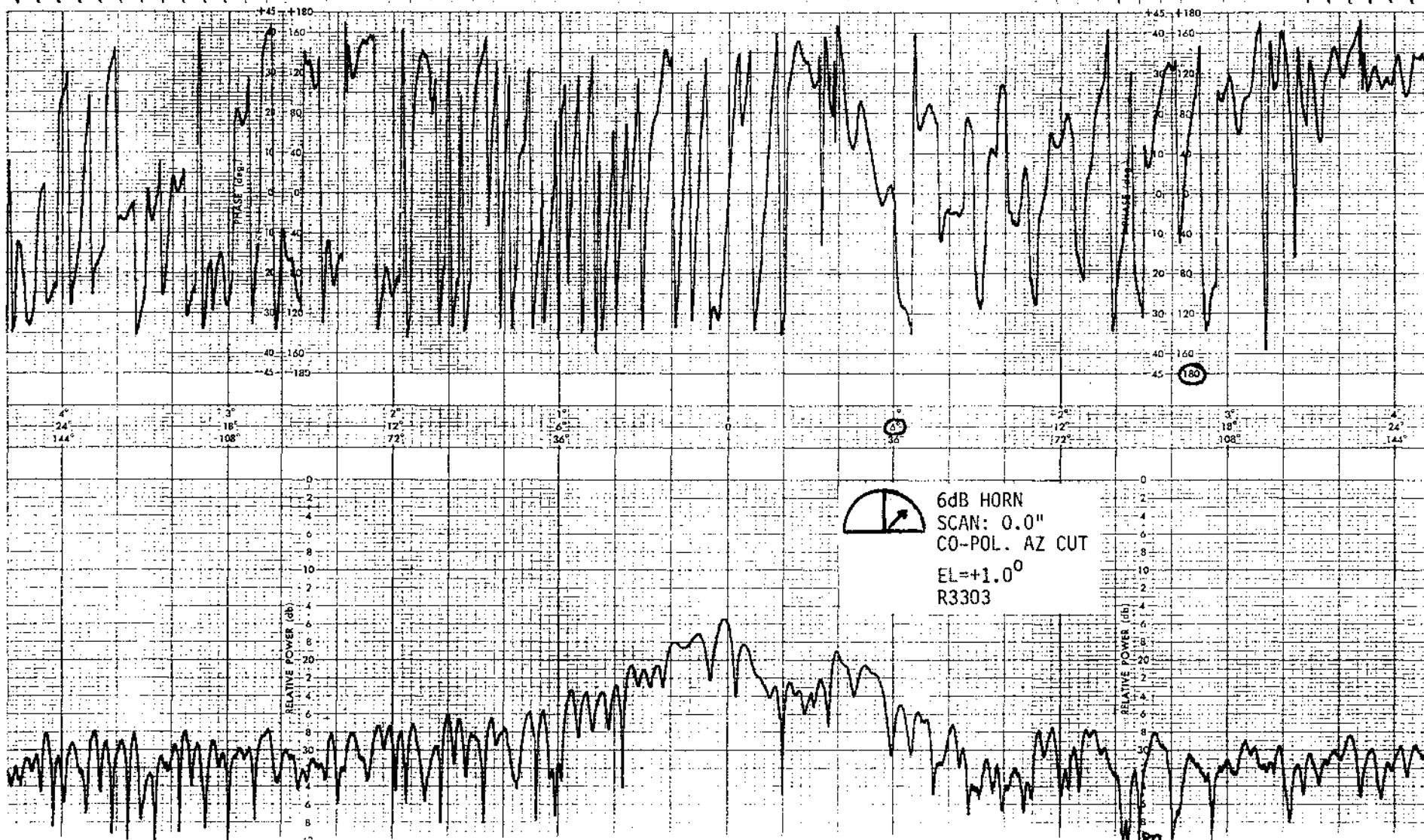
<u>CONFIGURATION</u>	<u>HORN</u>	<u>SCAN</u>	<u>POL.</u>	<u>PK. GAIN</u>	<u>PATTERN</u>	<u>FILE NAME</u>	<u>PAGE NUMBER</u>
	6 dB	0.0	CO	-	+3° EL + 45° AZ	R3301	151
	"	"	"	-	+2° EL "	R3302	152
	"	"	"	-	+1° EL "	R3303	153
	"	"	"	50.75	0° EL "	R3304	154
	"	"	"	-	-1° EL "	R3305	155
	"	"	"	-	-2° EL "	R3306	156
	"	"	"	-	-3° EL "	R3307	157
	6 dB	0.0	X	-	+3° EL + 45° AZ	R3401	158
	"	"	"	-	+2° EL "	R3402	159
	"	"	"	-	+1° EL "	R3403	160
	"	"	"	-	0° EL "	R3404	161
	"	"	"	-	-1° EL "	R3405	162
	"	"	"	-	-2° EL "	R3406	163
	"	"	"	-	-3° EL "	R3407	164
	6 dB	4.5"	CO	50.45	+45° AZ	L0045	165
	"	"	CO	"	+ 5° AZ	L0043	166
	"	"	CO	"	+ 5° EL	L0044	167
	"	"	X	"	+45° AZ	L0048	168
	"	"	X	"	+ 5° AZ	L0046	169
	"	"	X	"	+ 5° EL	L0047	170
	6 dB	0.0	CO	-	+3° EL + 45° AZ	R3101	171
	"	"	"	-	+2° EL "	R3102	172
	"	"	"	-	+1° EL "	R3103	173
	"	"	"	50.70	0° EL "	R3104	174
	"	"	"	-	-1° EL "	R3105	175
	"	"	"	-	-2° EL "	R3106	176
	"	"	"	-	-3° EL "	R3107	177
	6 dB	0.0	X	-	+3° EL + 45° AZ	R3201	178
	"	"	"	-	+2° EL "	R3202	179
	"	"	"	-	+1° EL "	R3203	180
	"	"	"	-	0° EL "	R3204	181
	"	"	"	-	-1° EL "	R3205	182
	"	"	"	-	-2° EL "	R3206	183
	"	"	"	-	-3° EL "	R3207	184

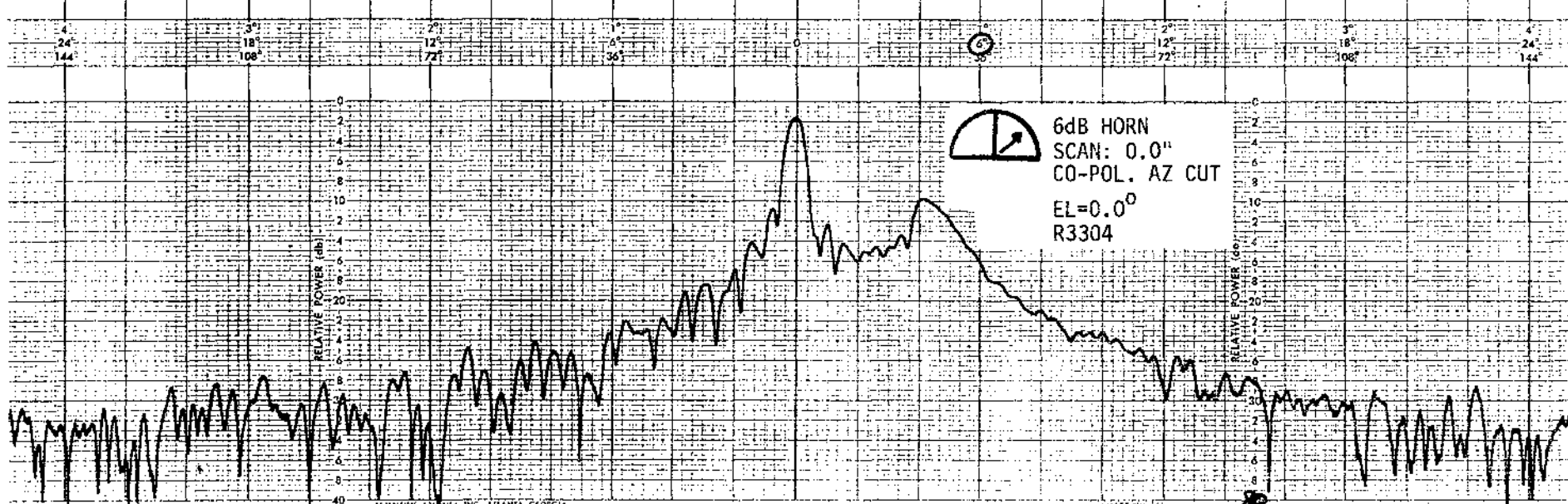
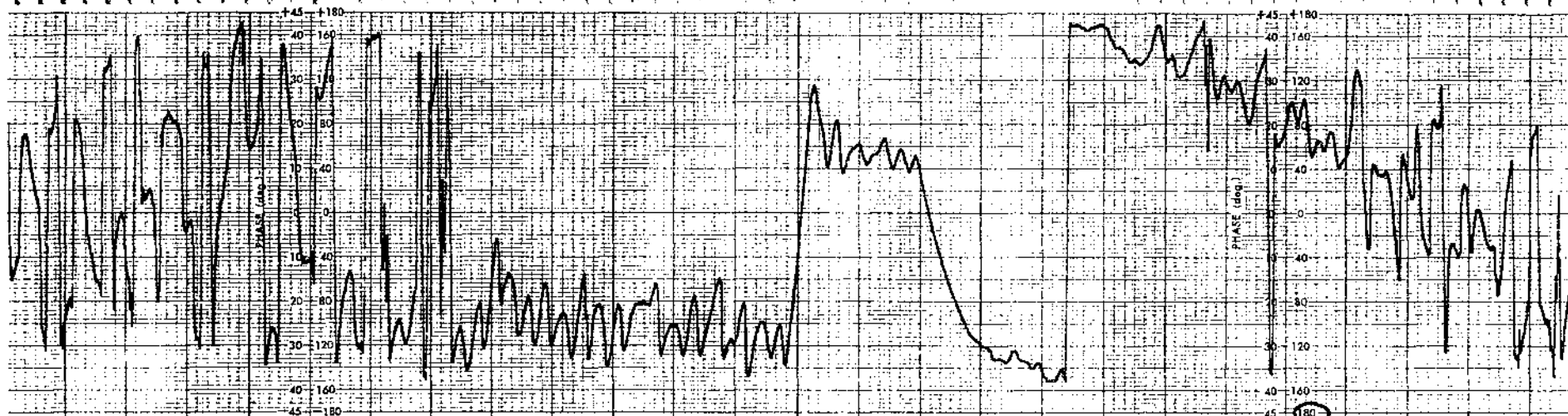


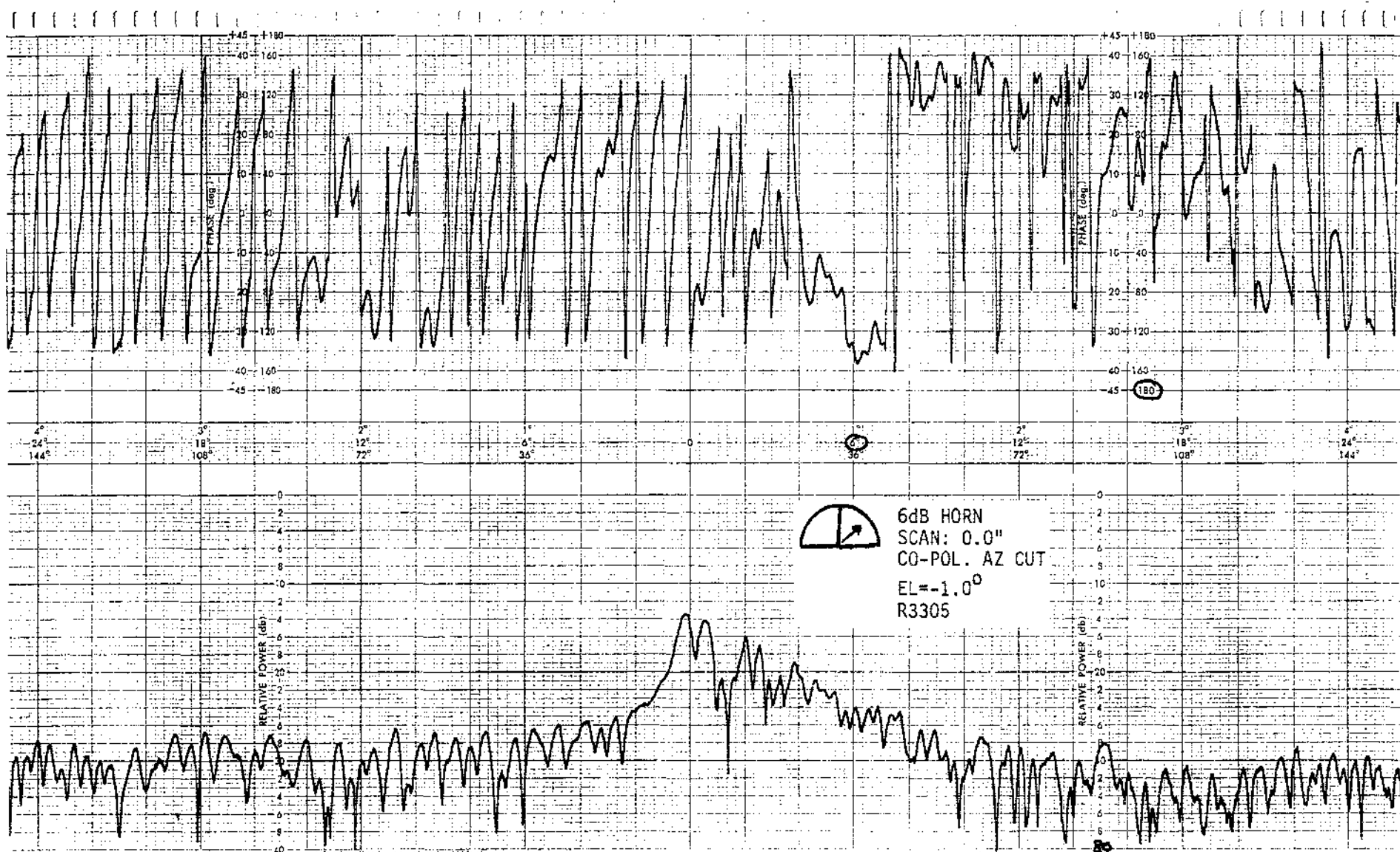
6dB HORN  
 SCAN: 0.0"  
 CO-POL. AZ CUT  
 EL=+3.0°  
 R3301

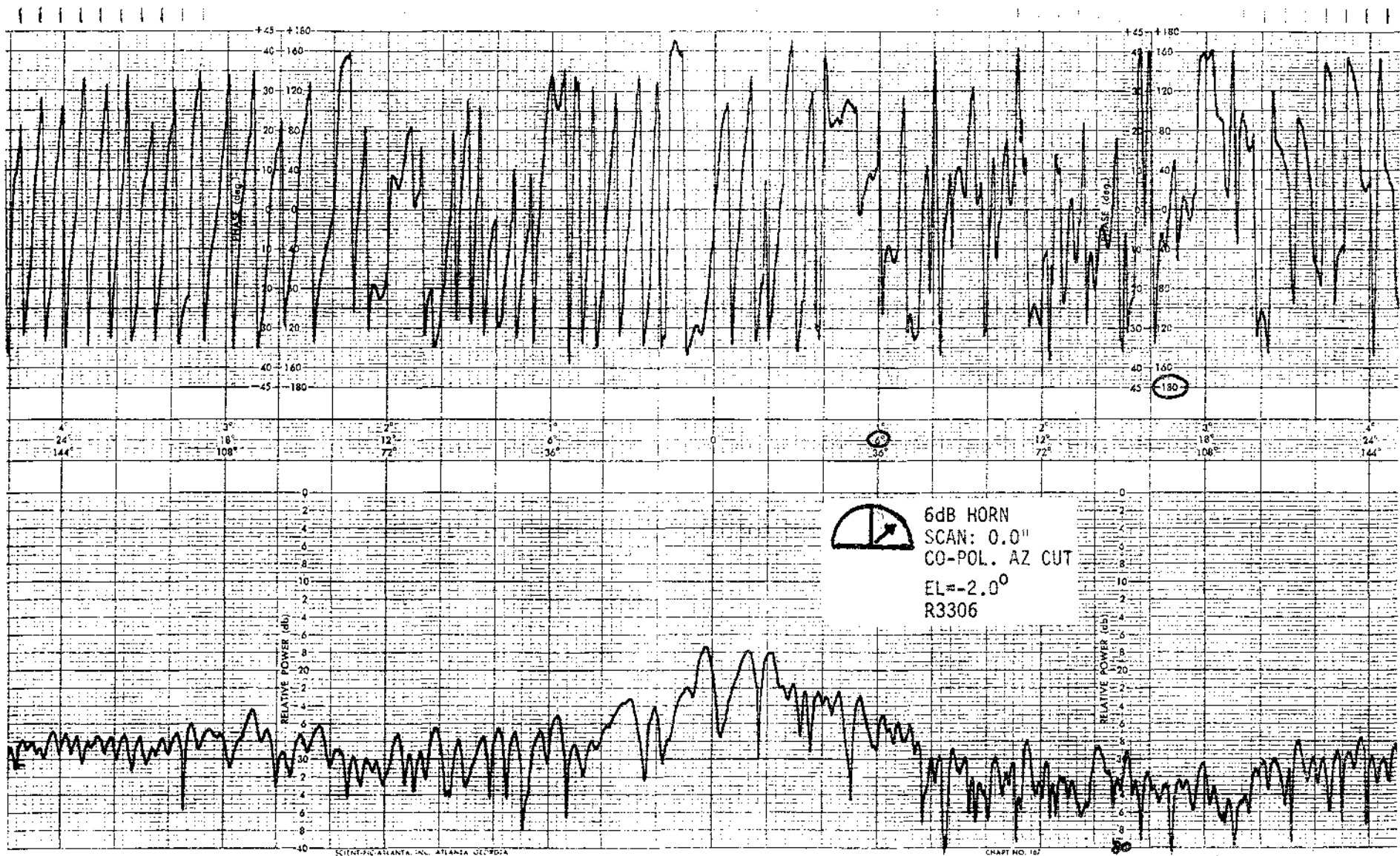




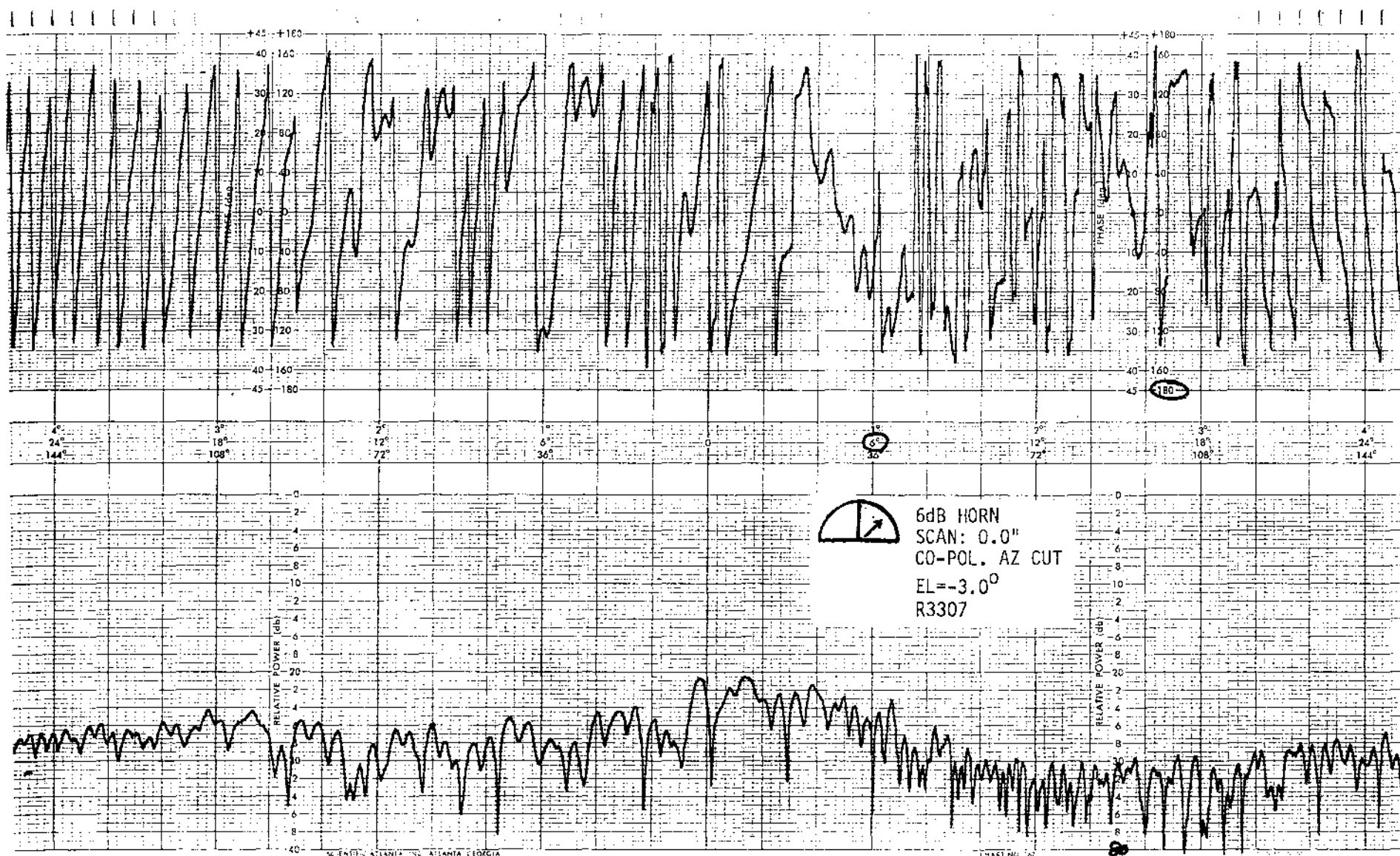




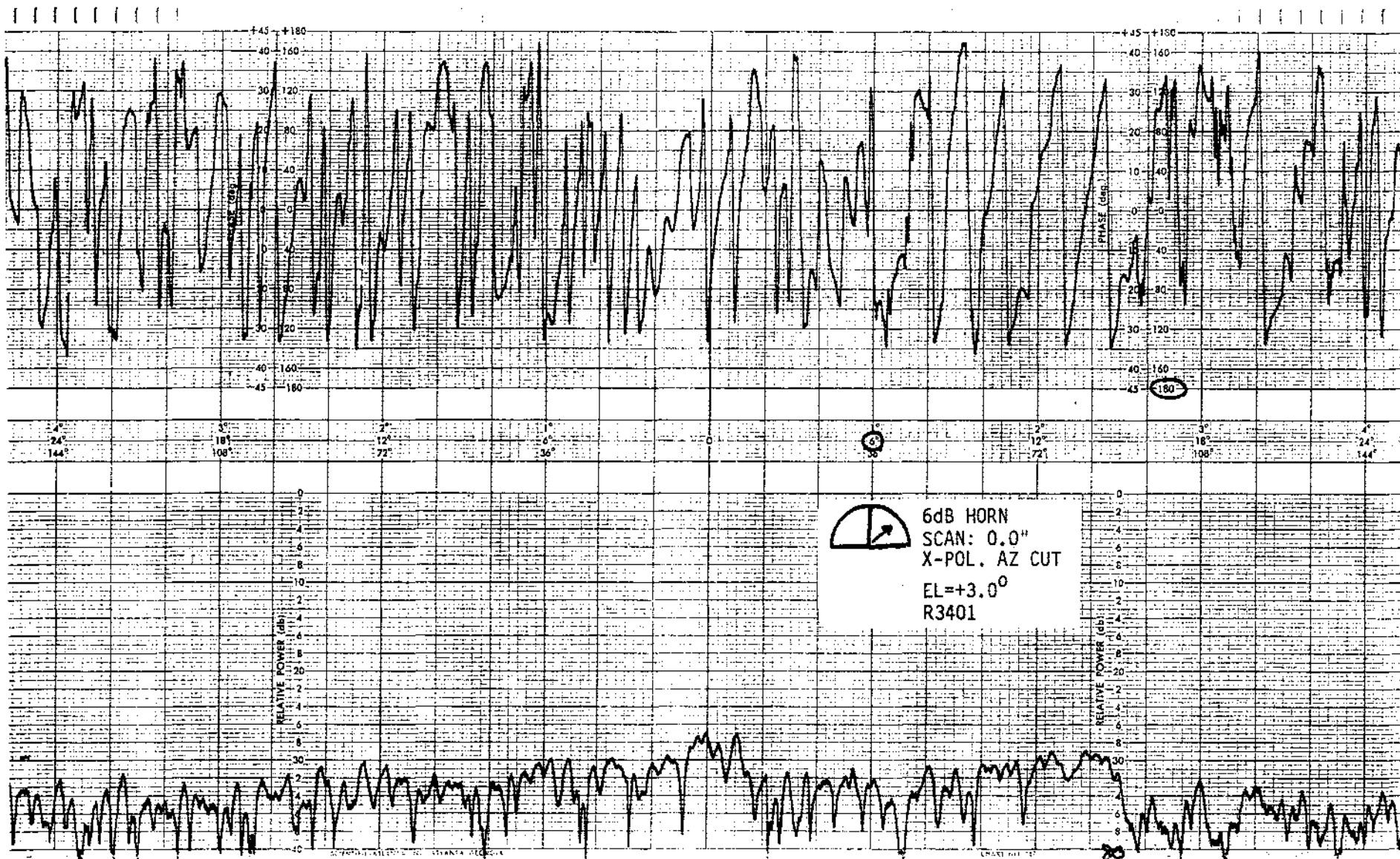


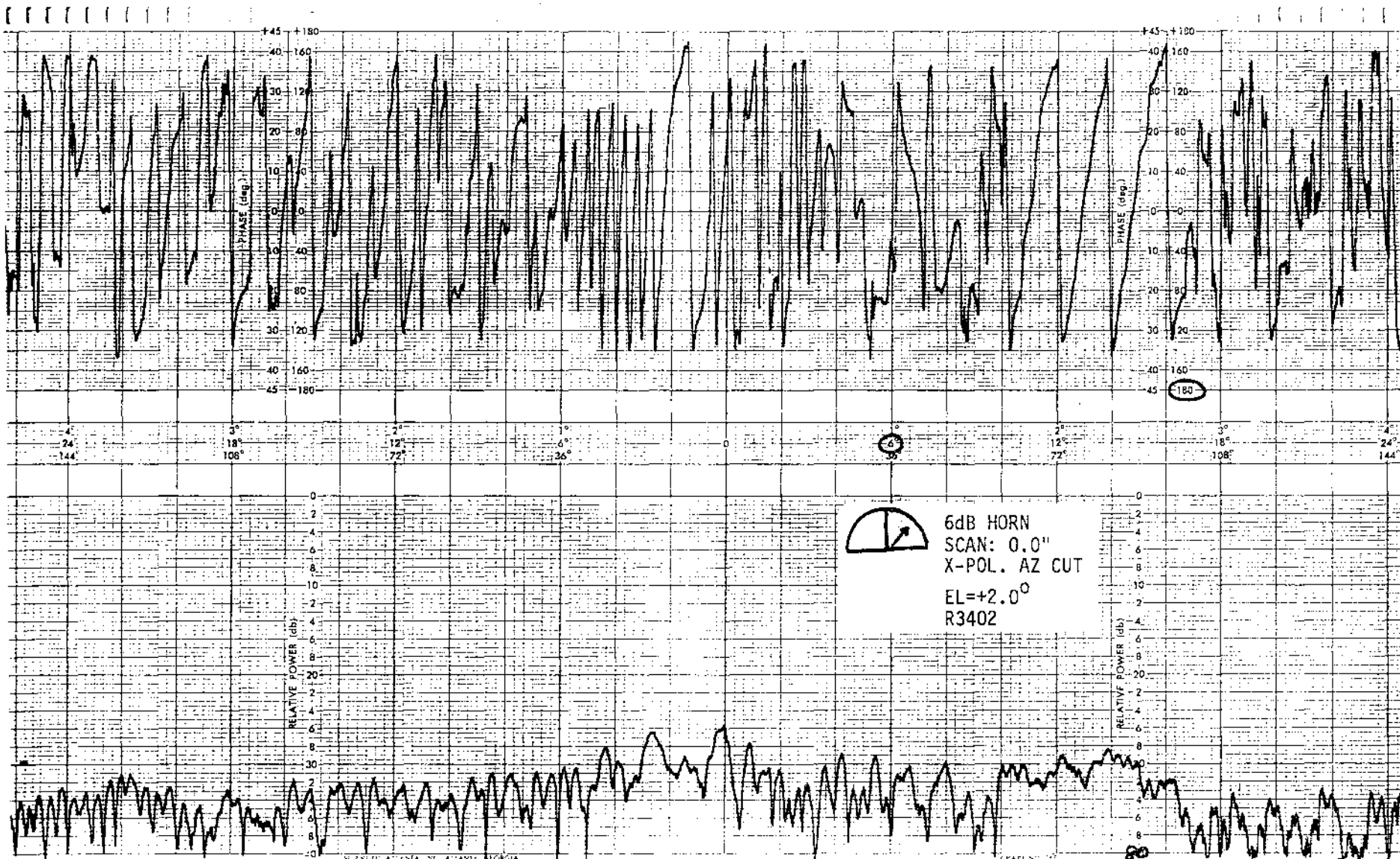








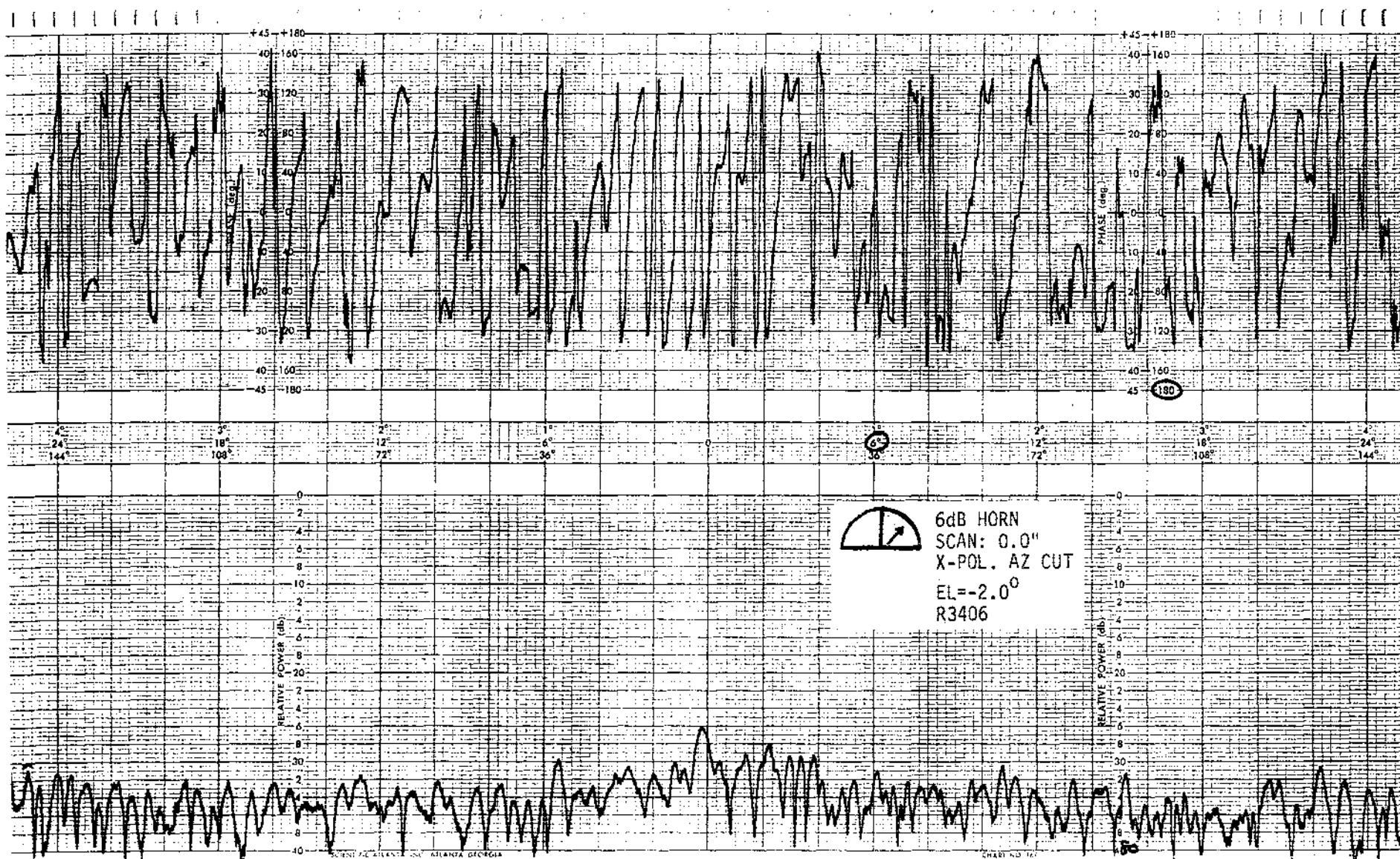






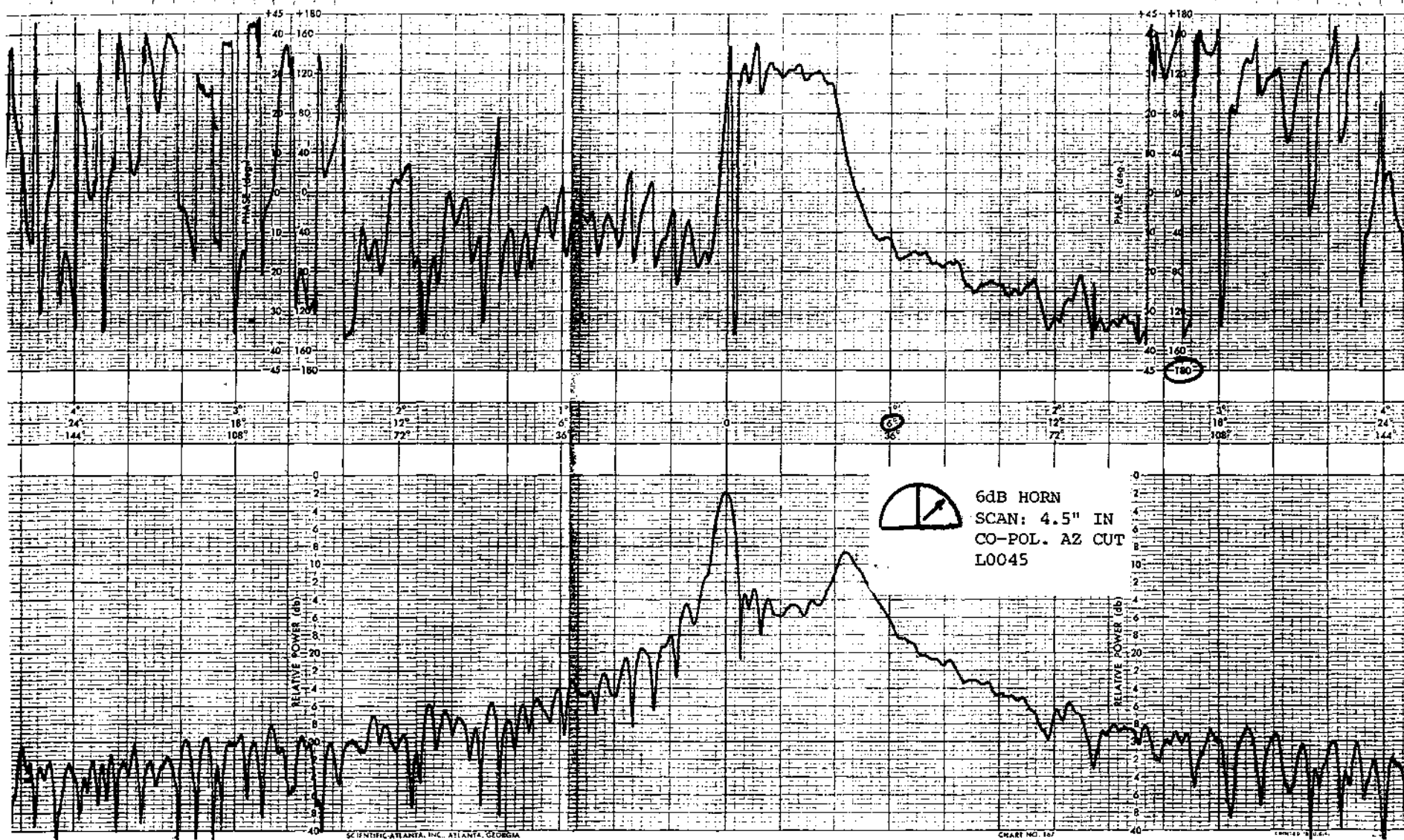






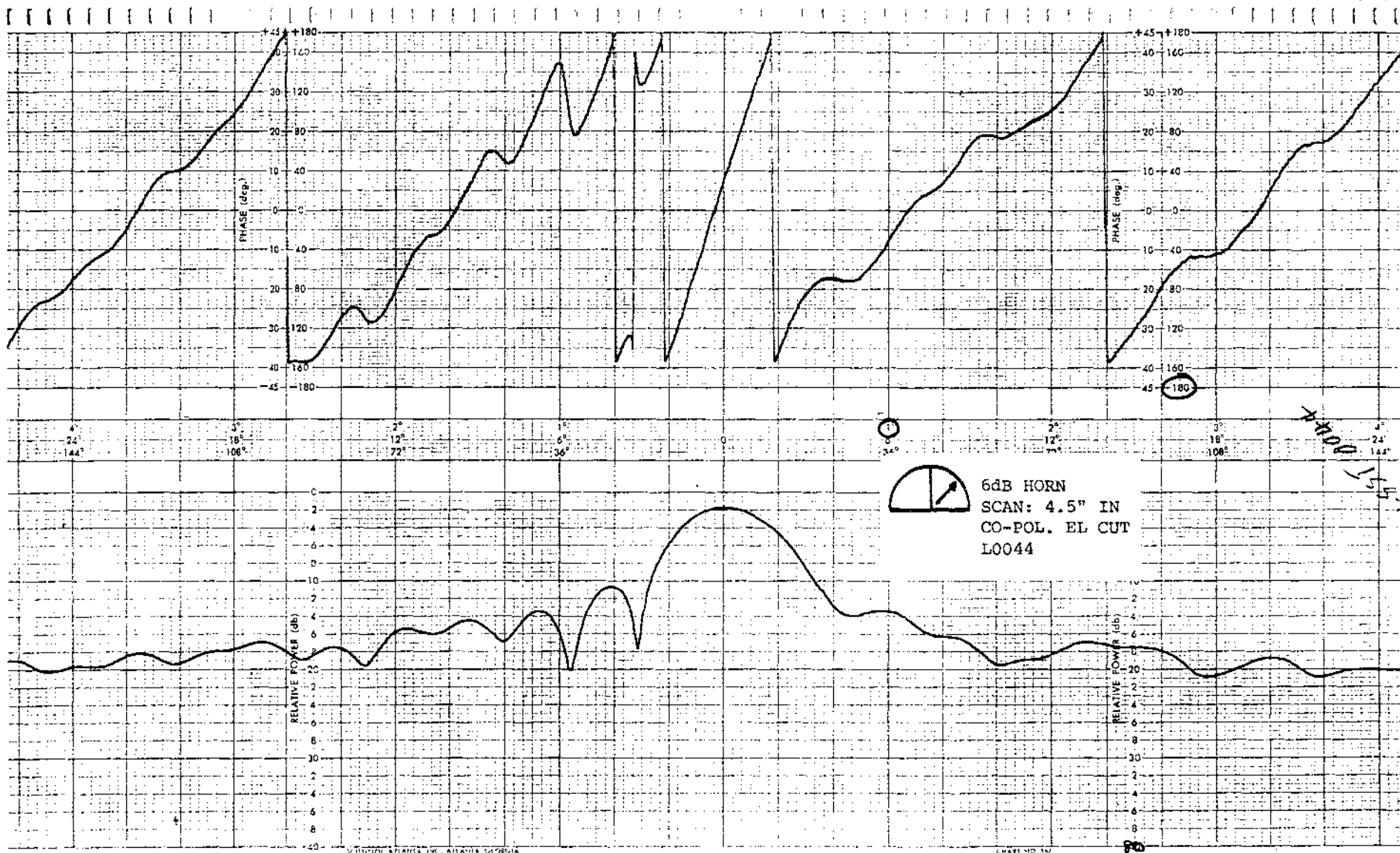


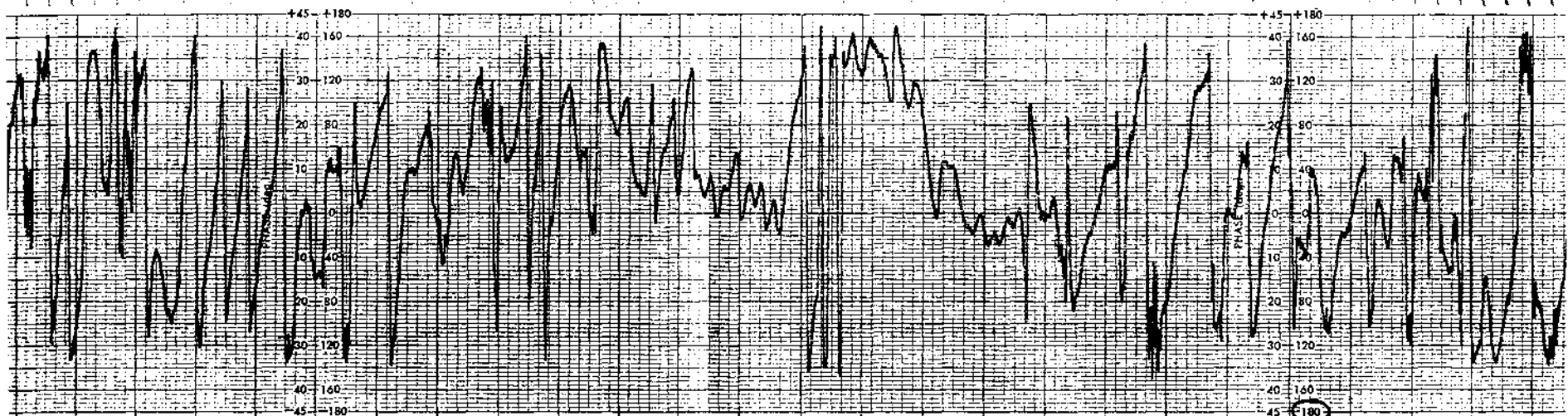




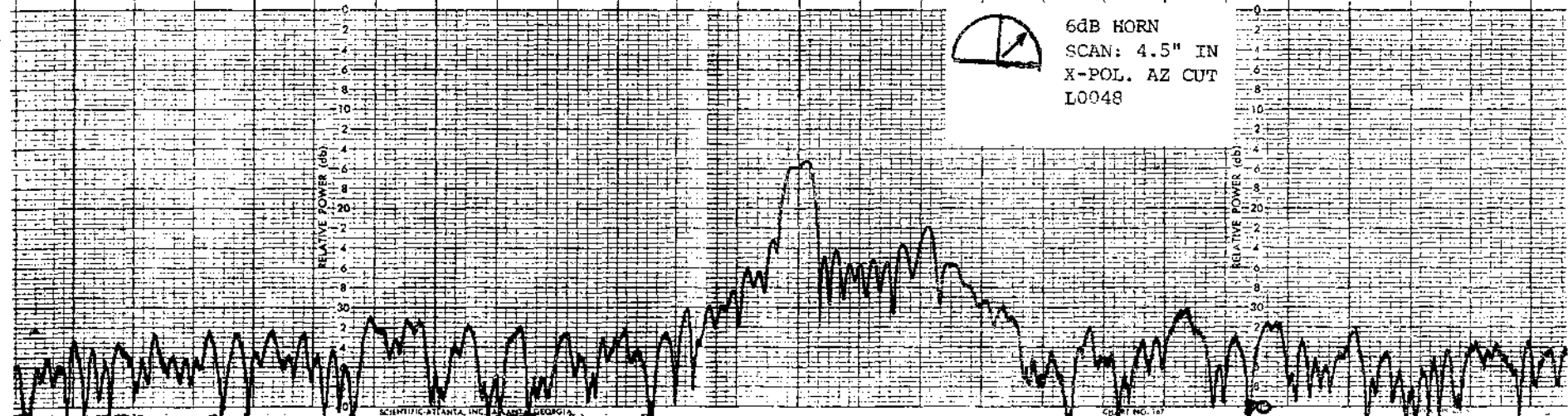








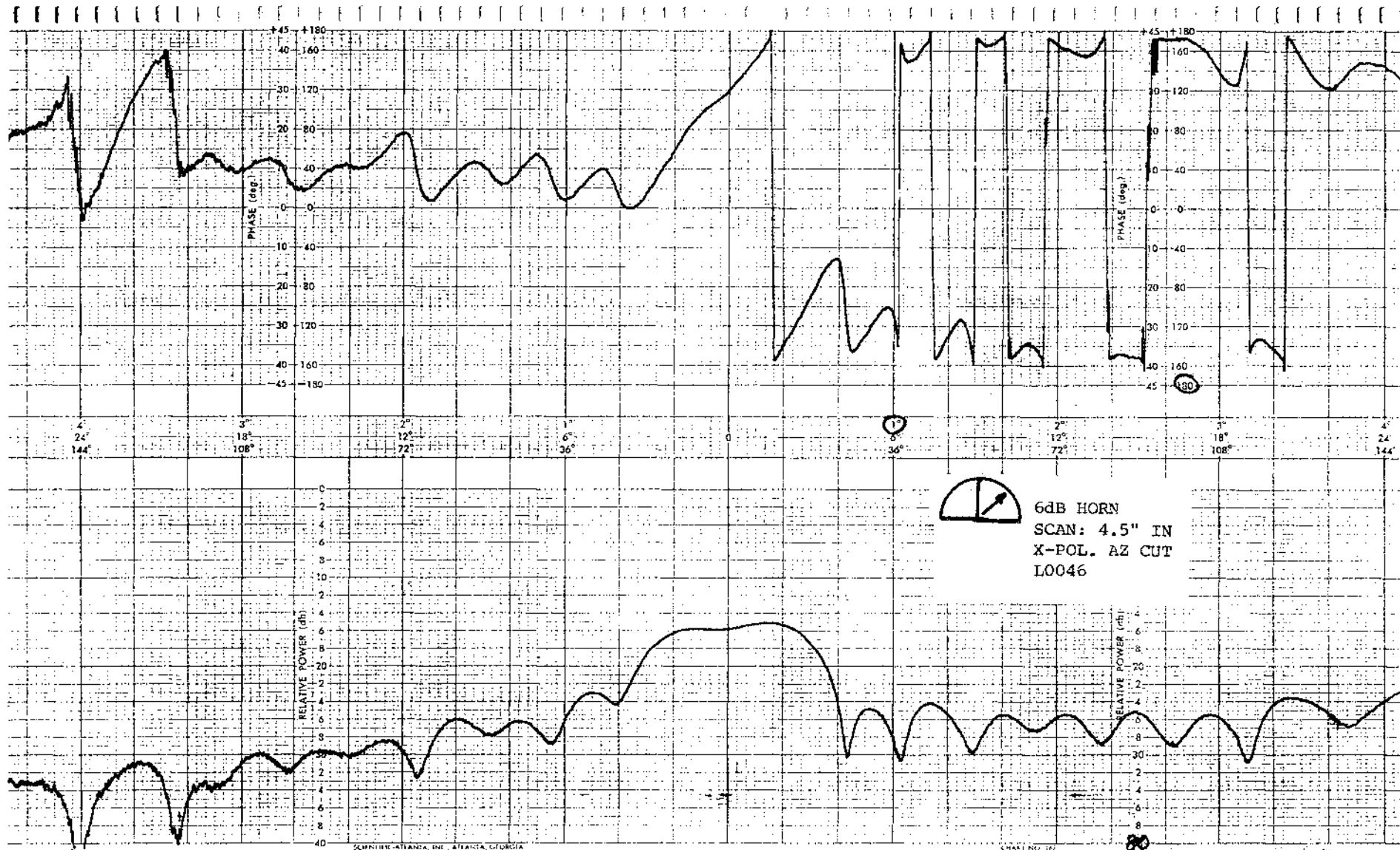
4° 24° 18° 12° 6° 0° 6° 12° 18° 24° 30° 36°

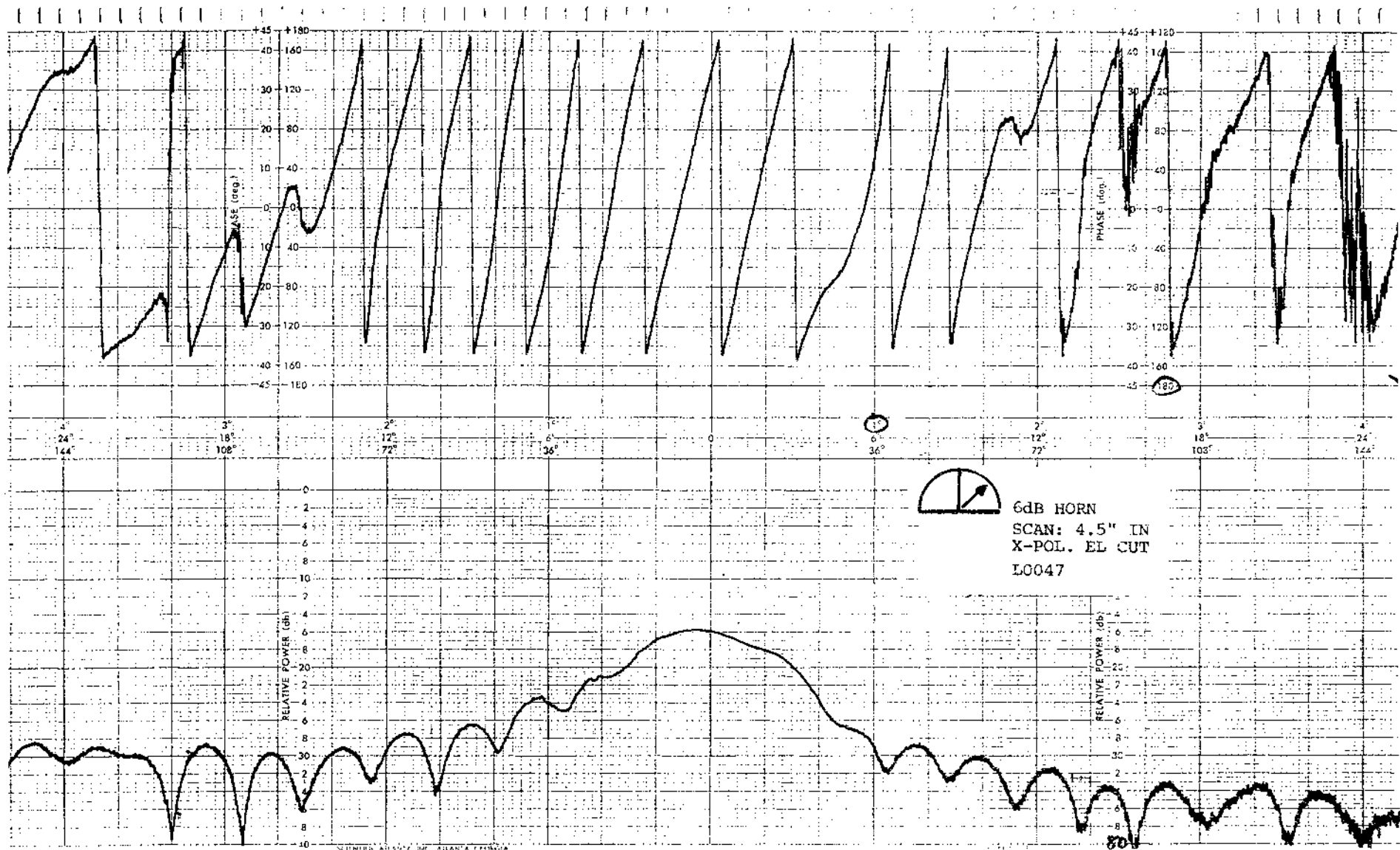


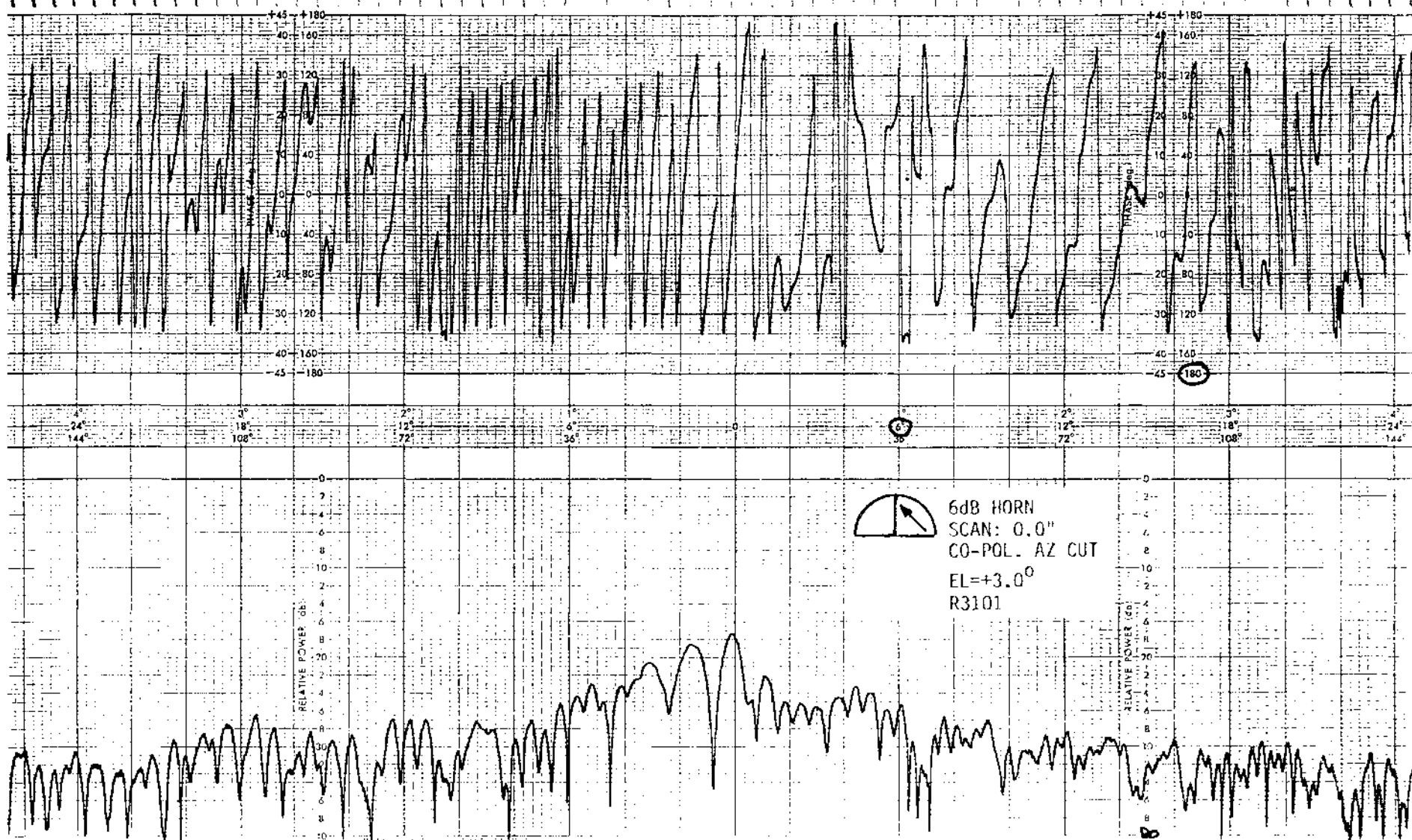
6dB HORN  
SCAN: 4.5" IN  
X-POL. AZ CUT  
L0048

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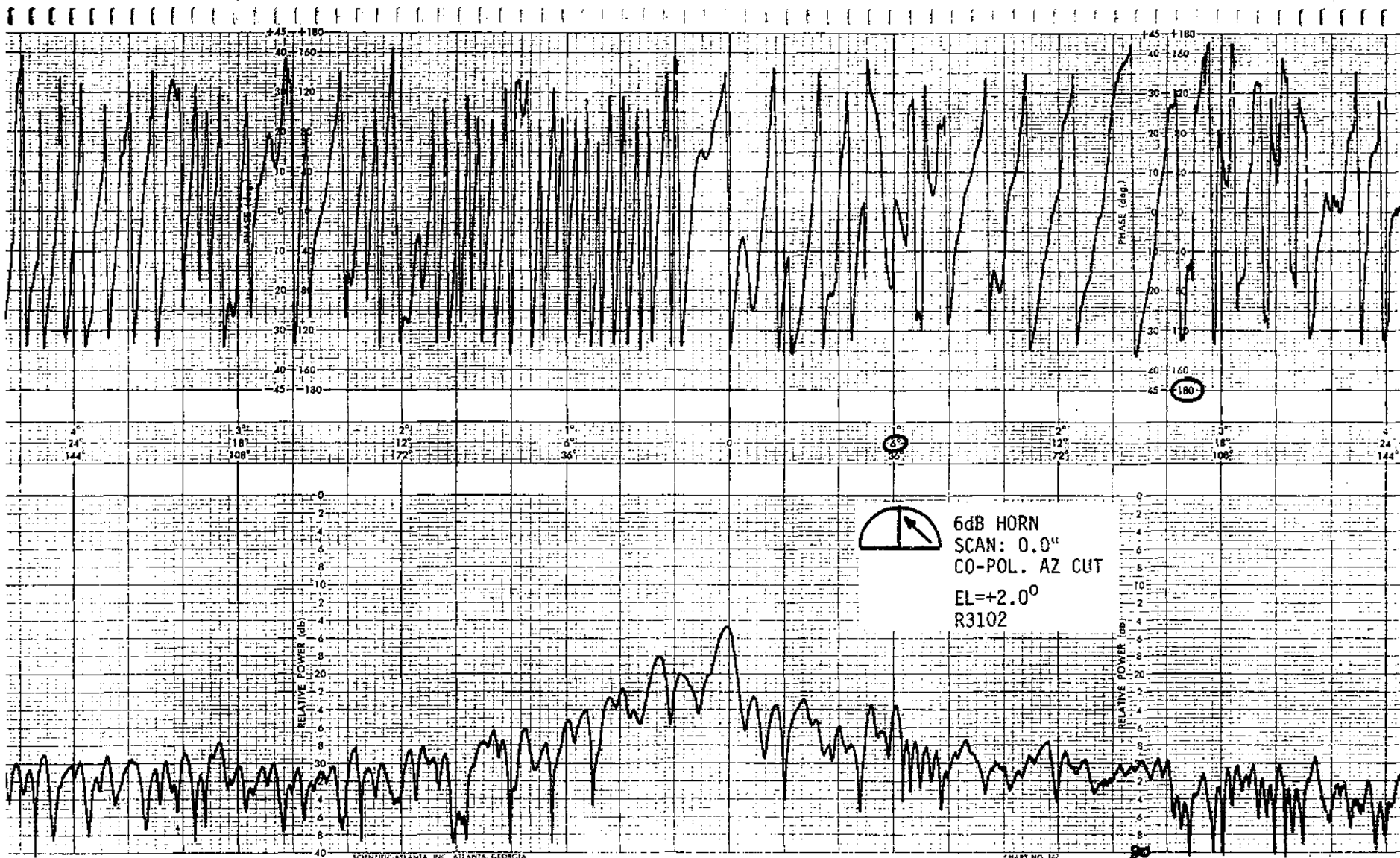
CONT. NO. 107

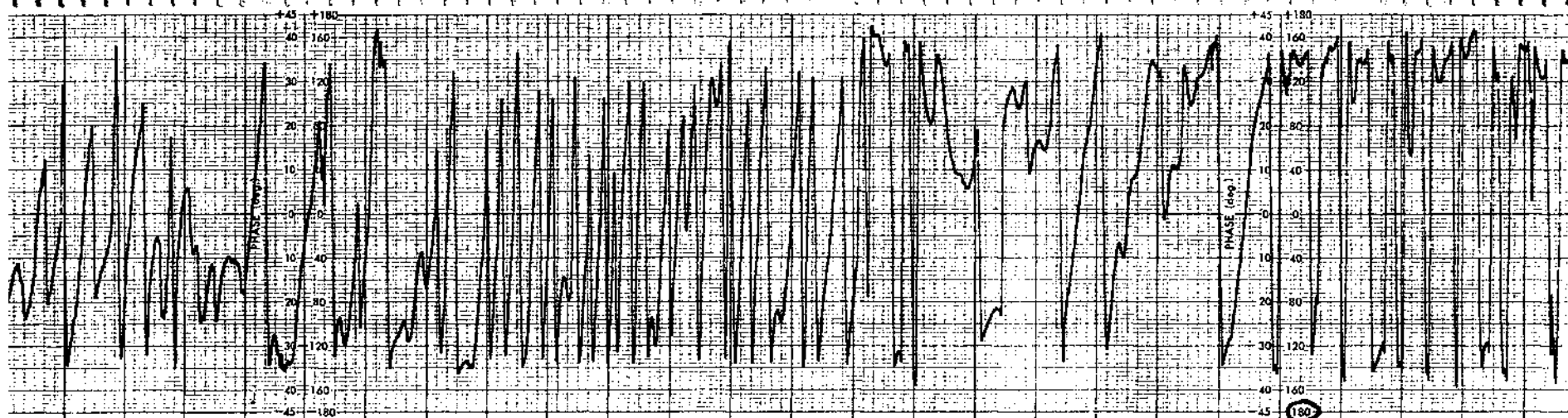




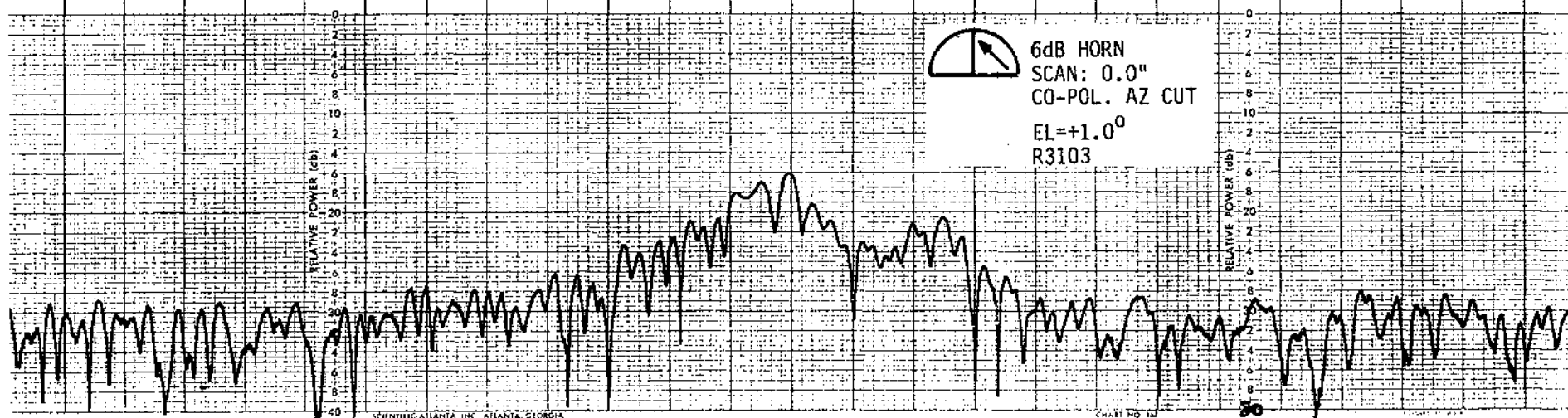








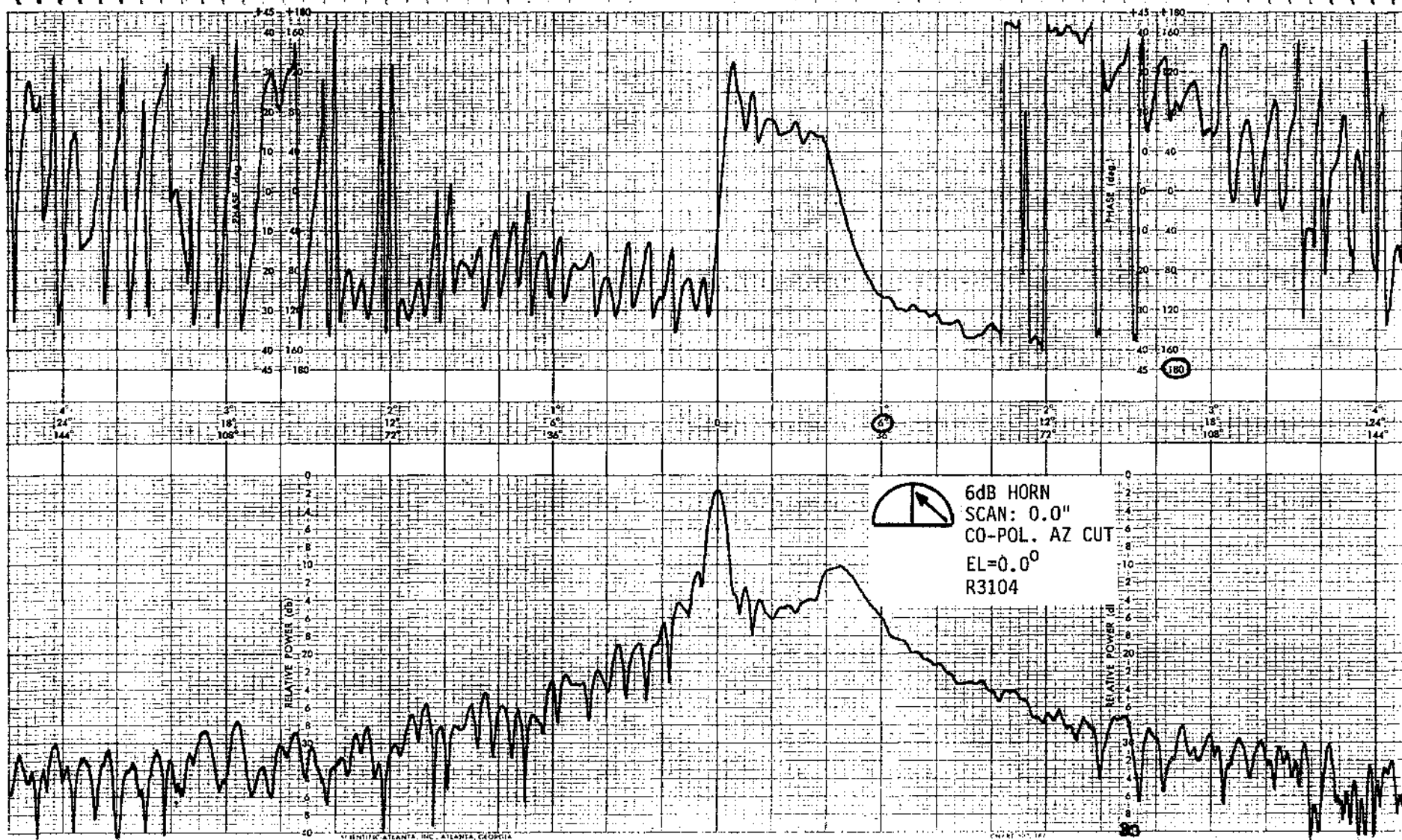
6dB HORN  
SCAN: 0.0"  
CO-POL. AZ CUT  
EL=+1.0°  
R3103

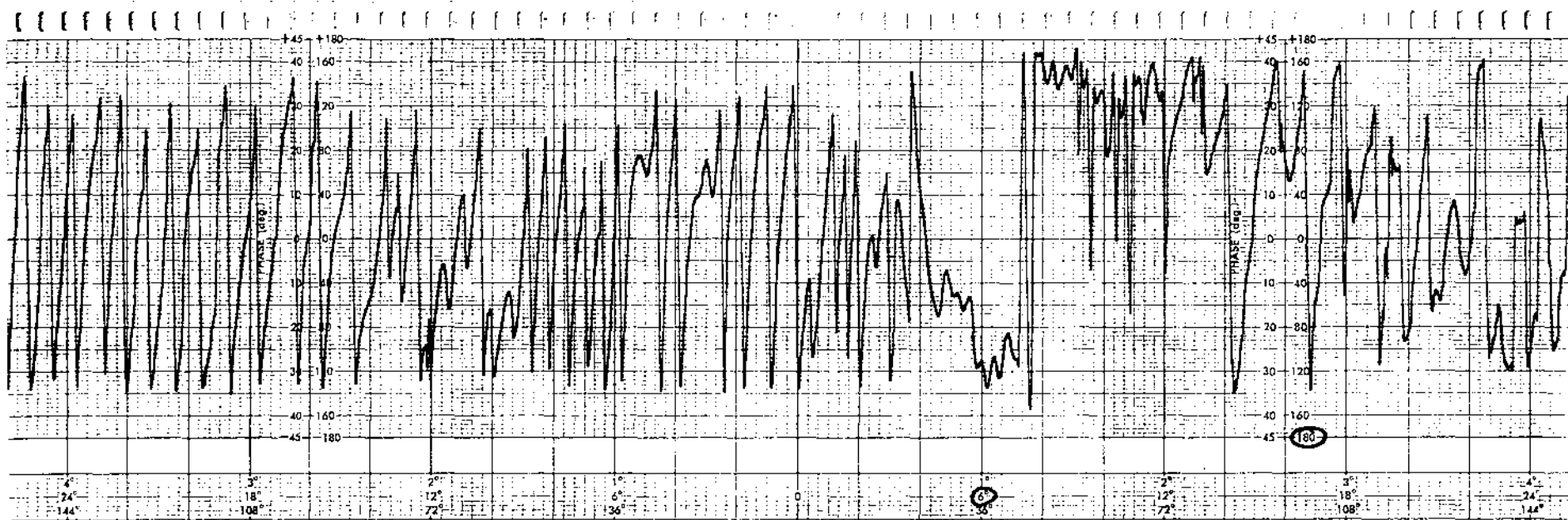


SCIENTIFIC ATLANTA, INC. ATLANTA, GEORGIA

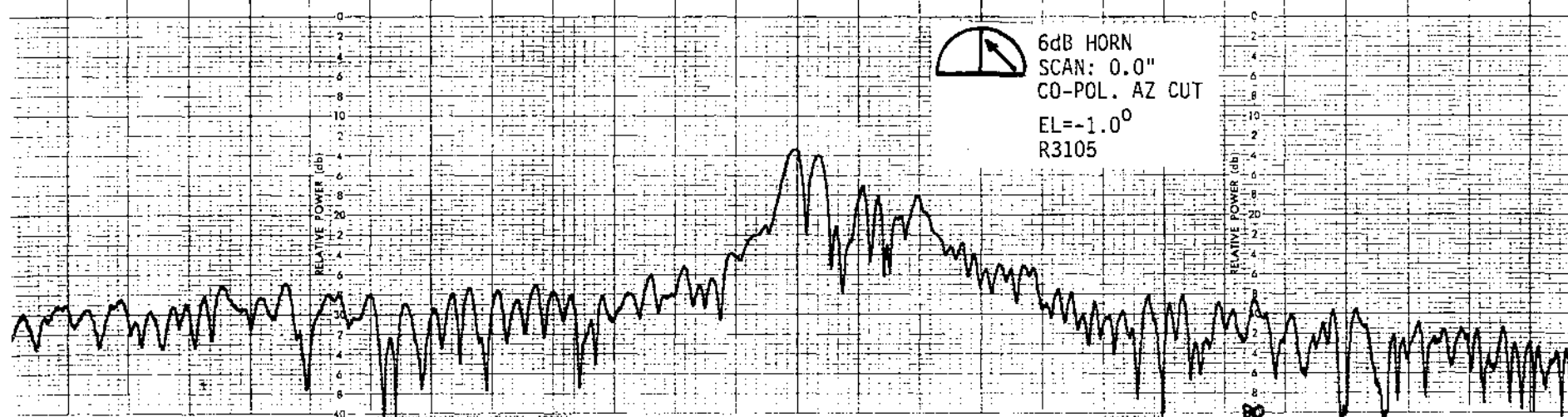
CHART NO. 12

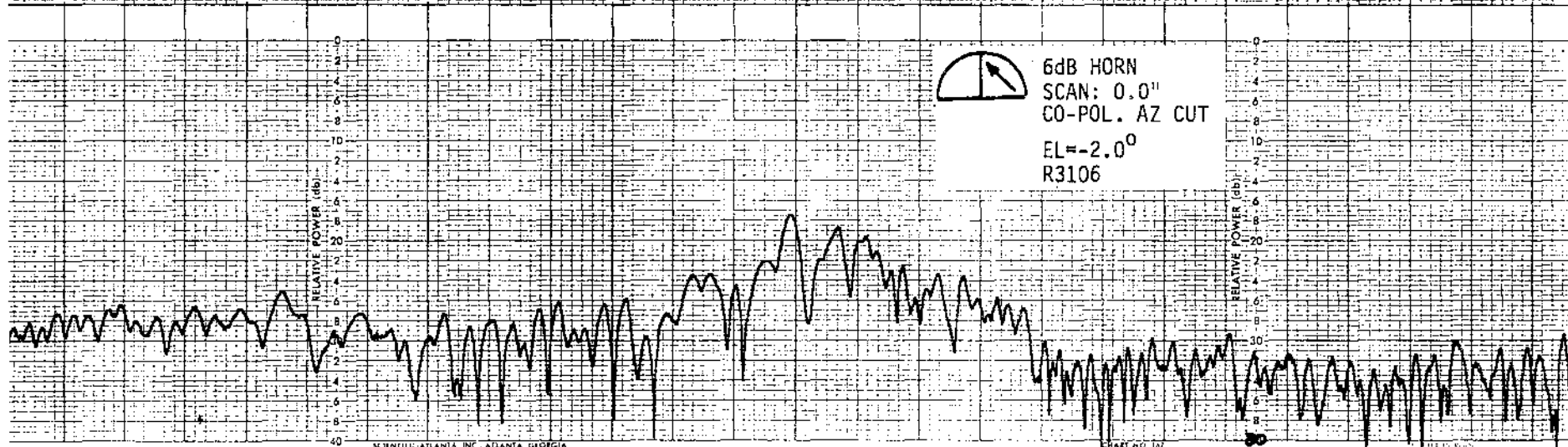
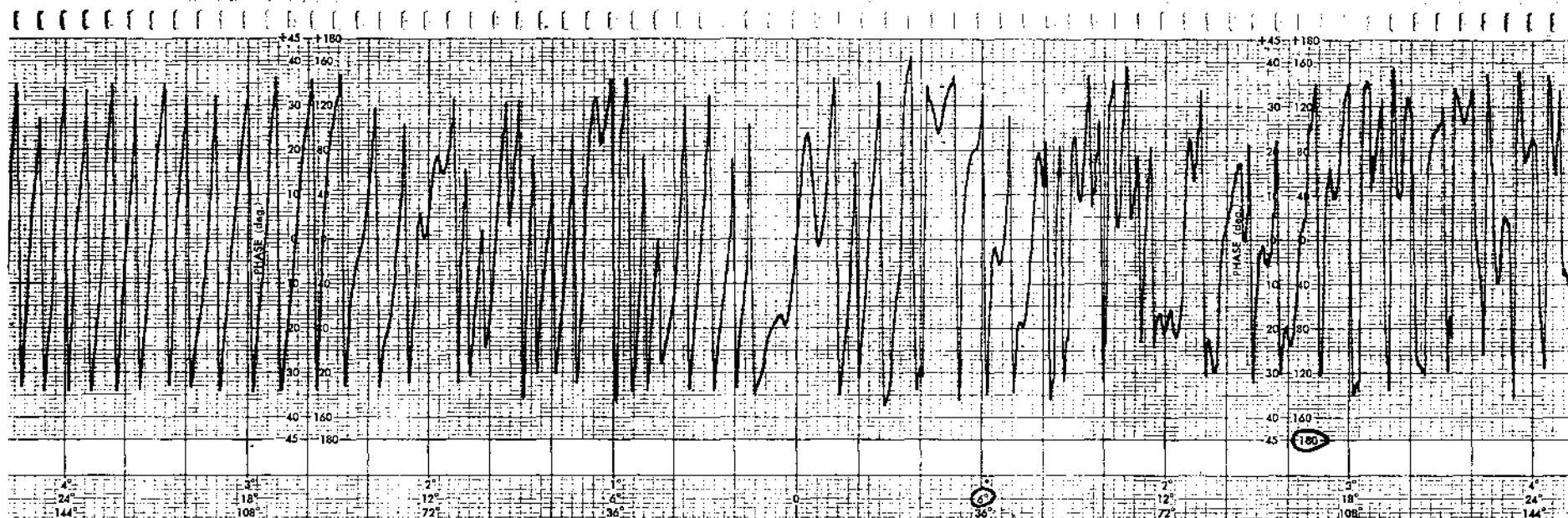


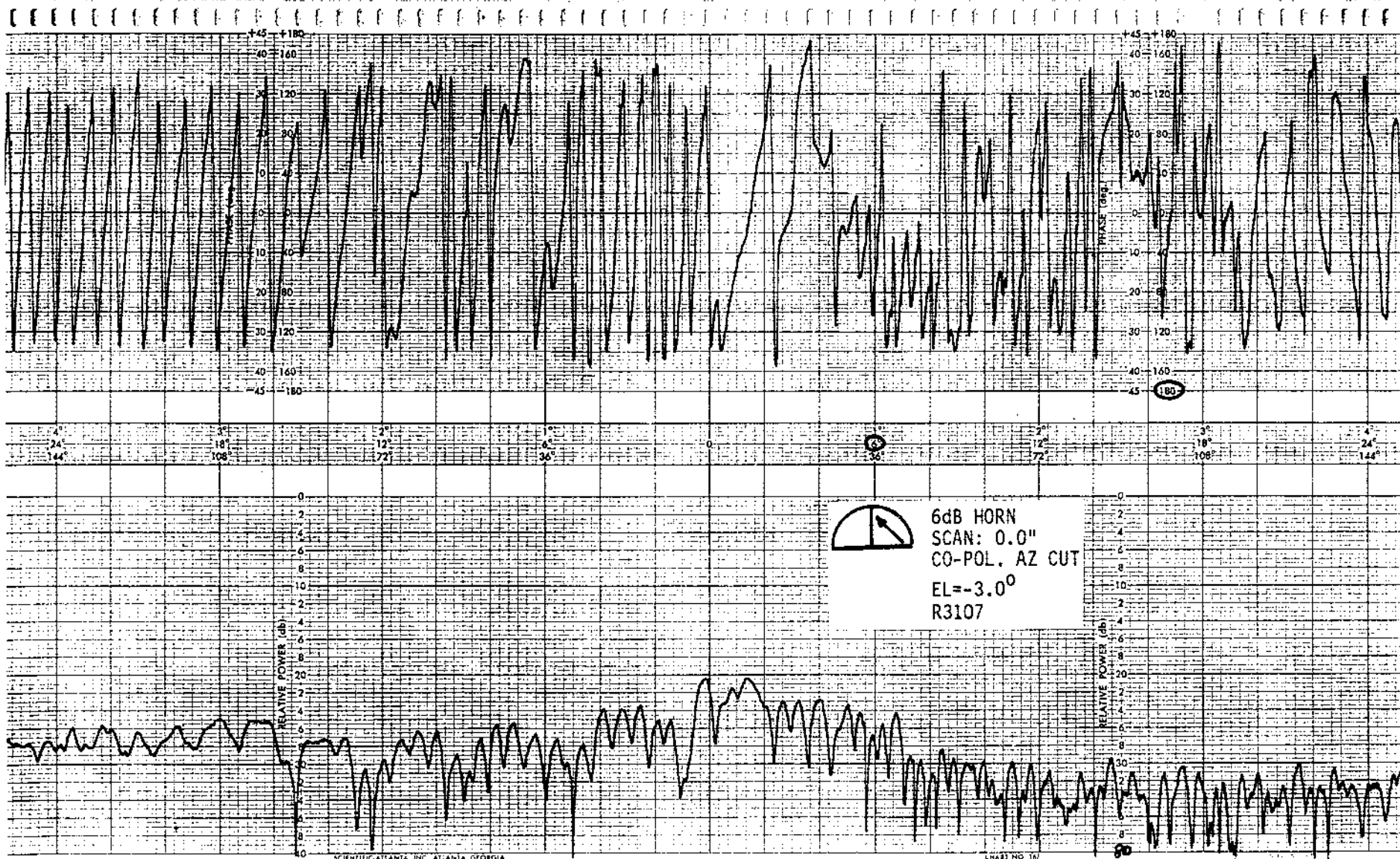


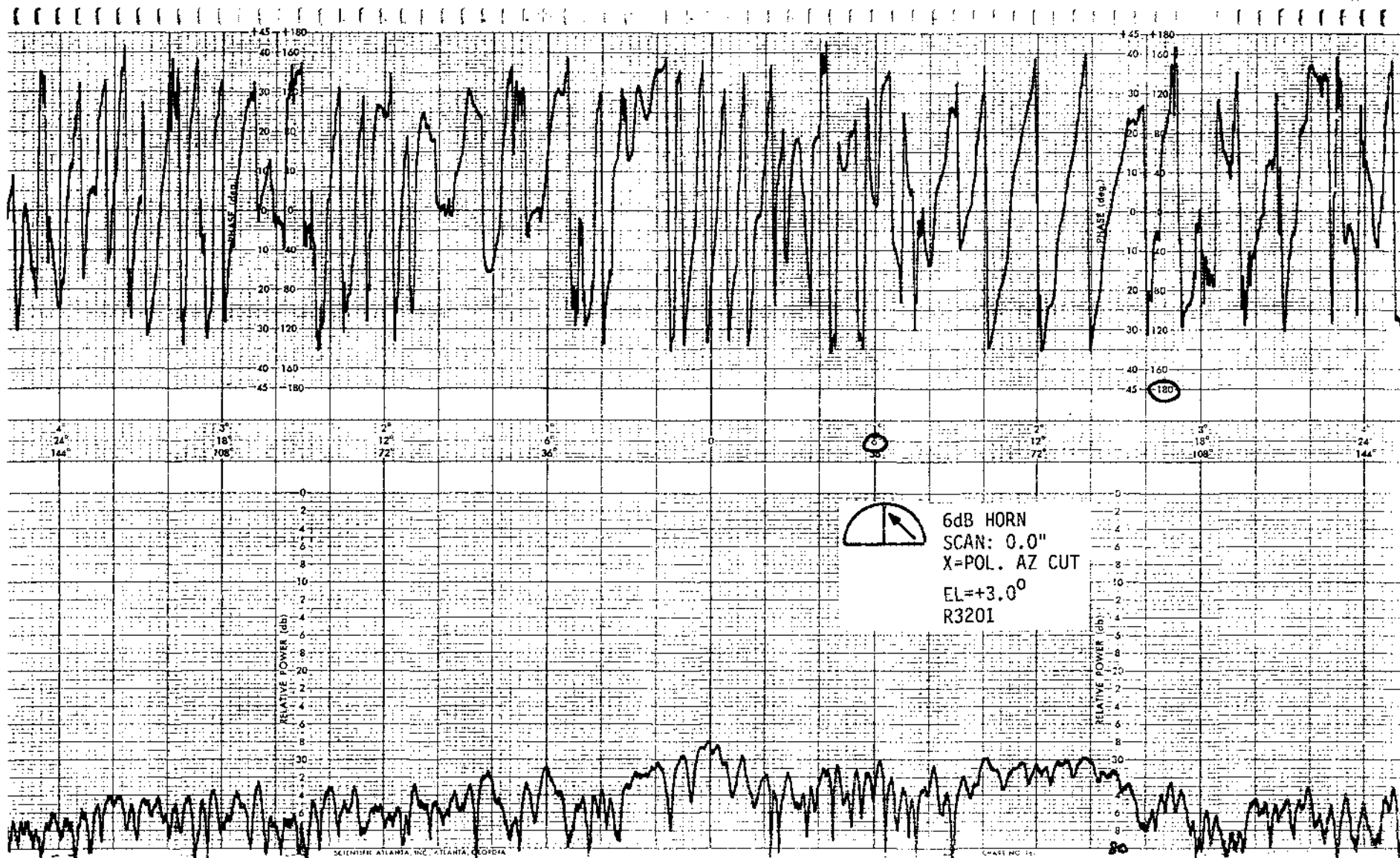


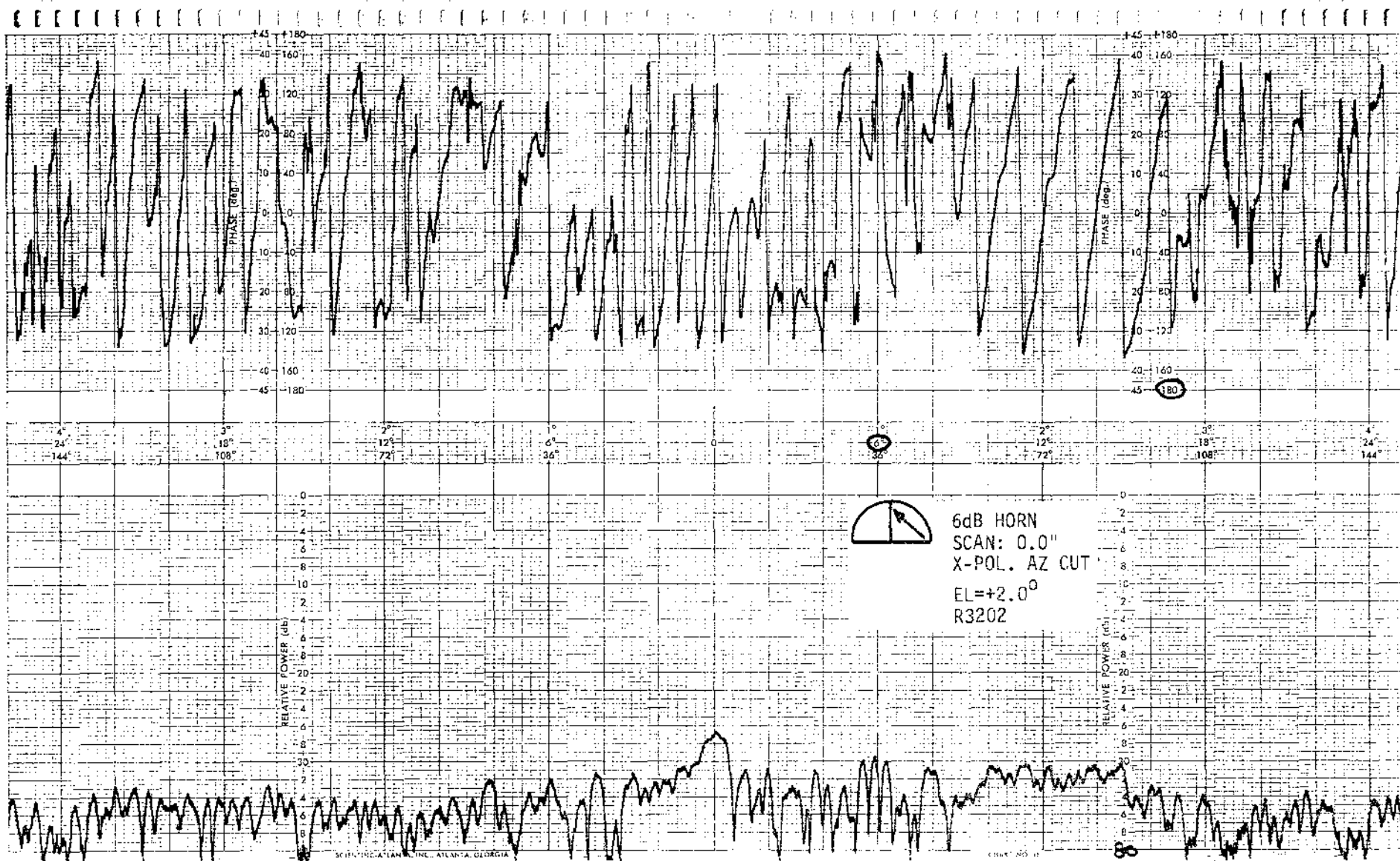
6dB HORN  
SCAN: 0.0"  
CO-POL. AZ CUT  
EL=-1.0°  
R3105



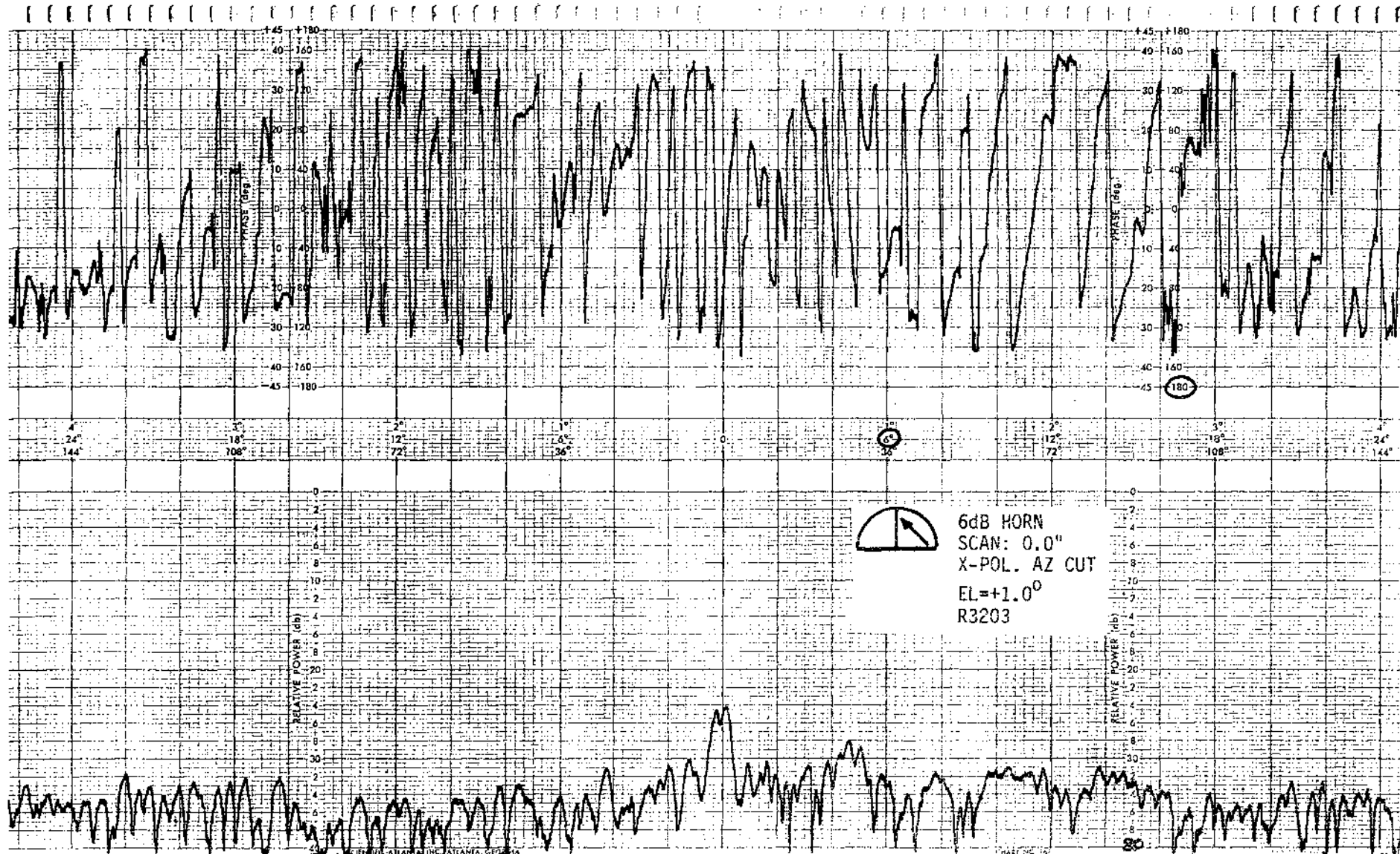


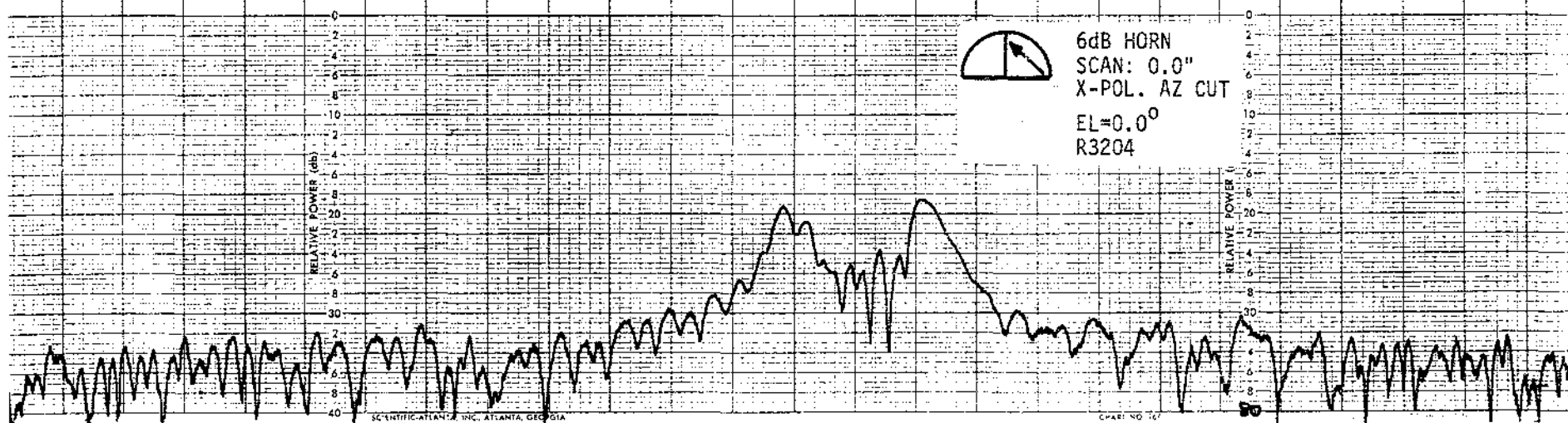
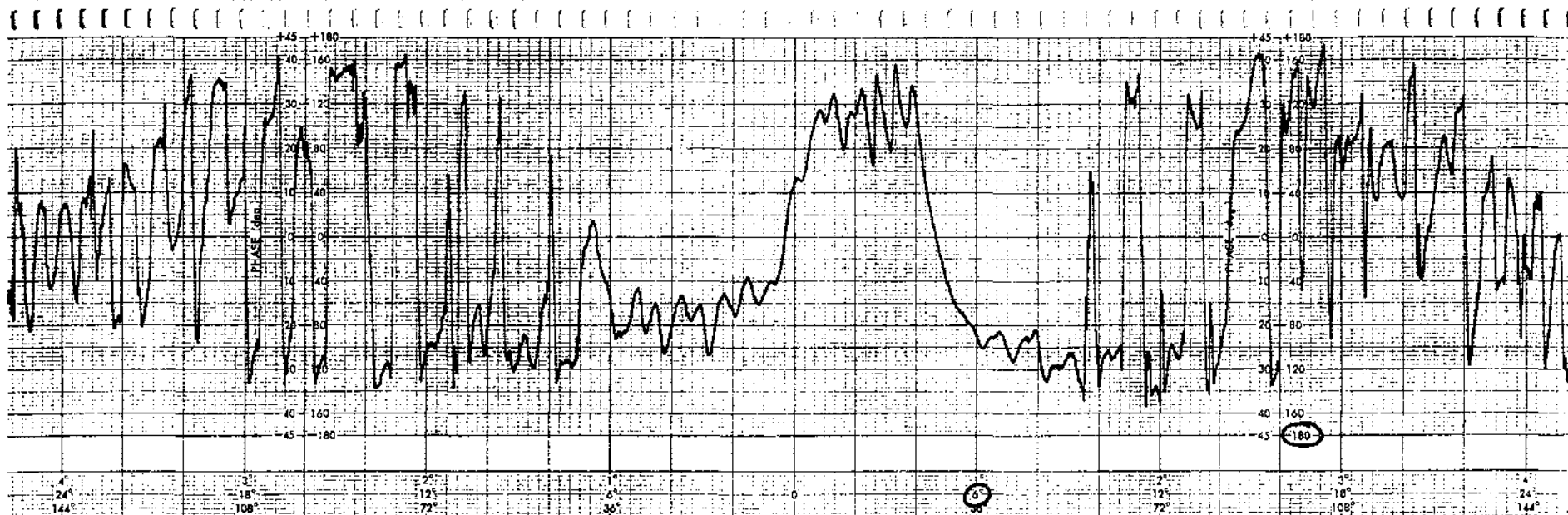




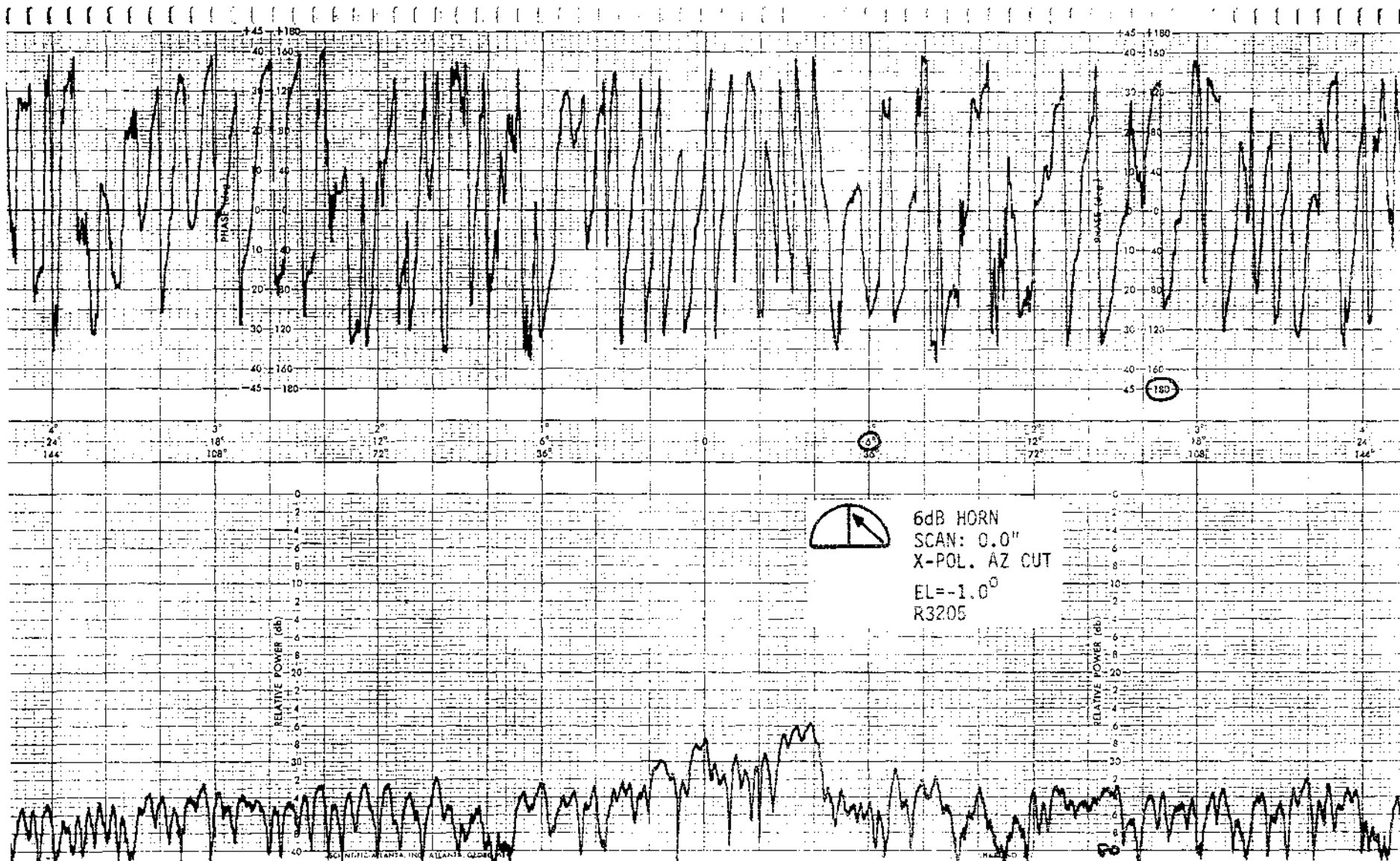


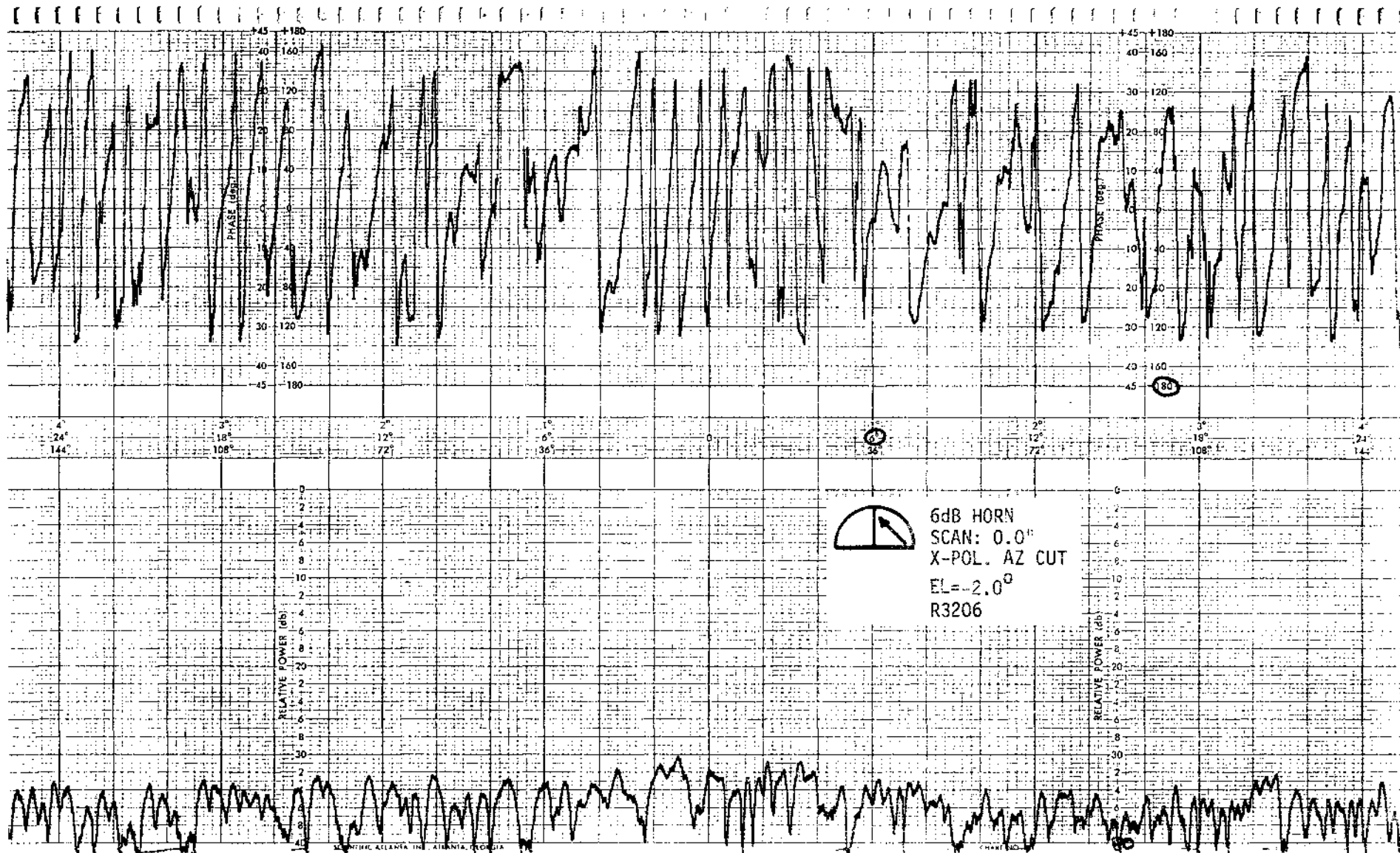


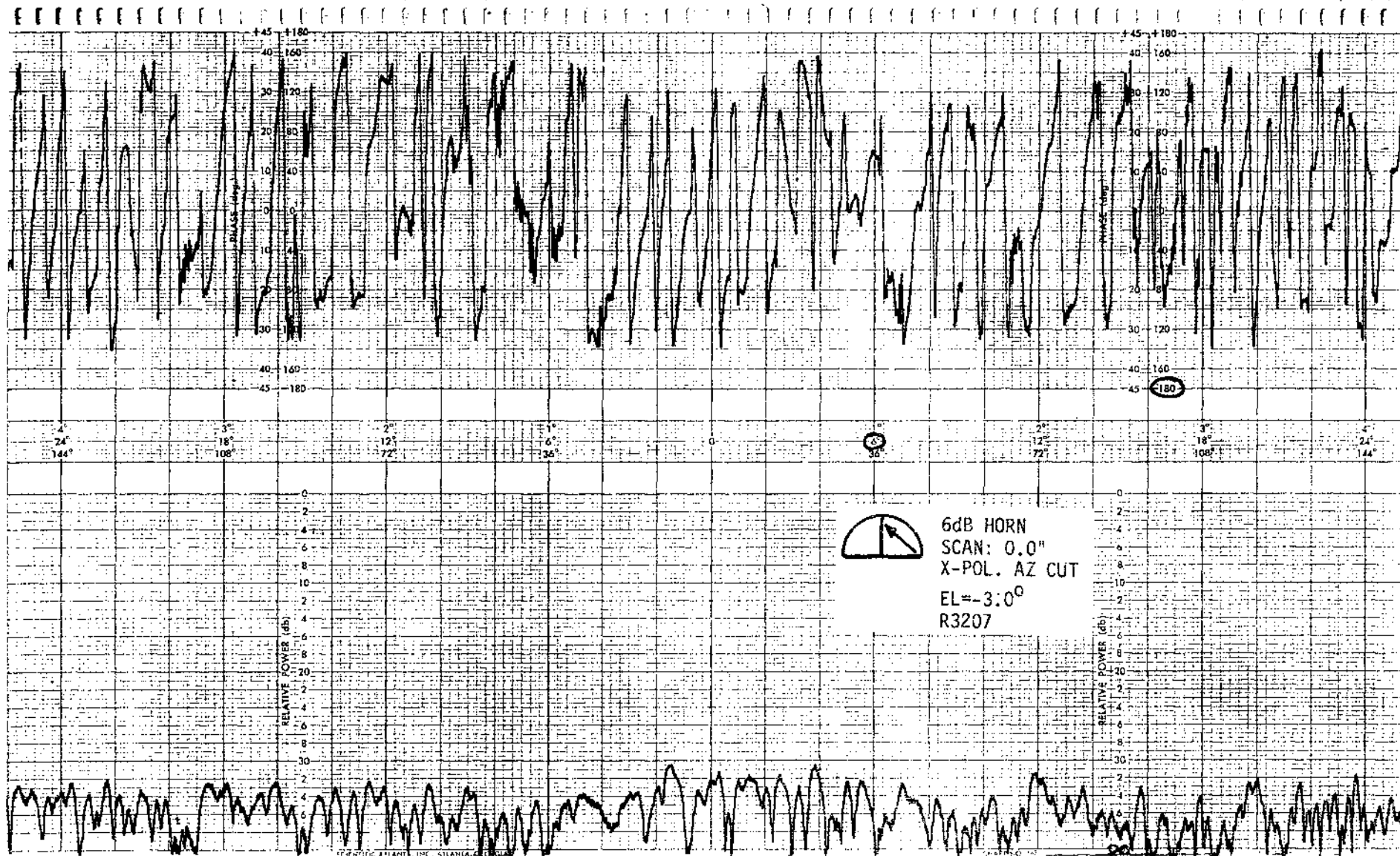








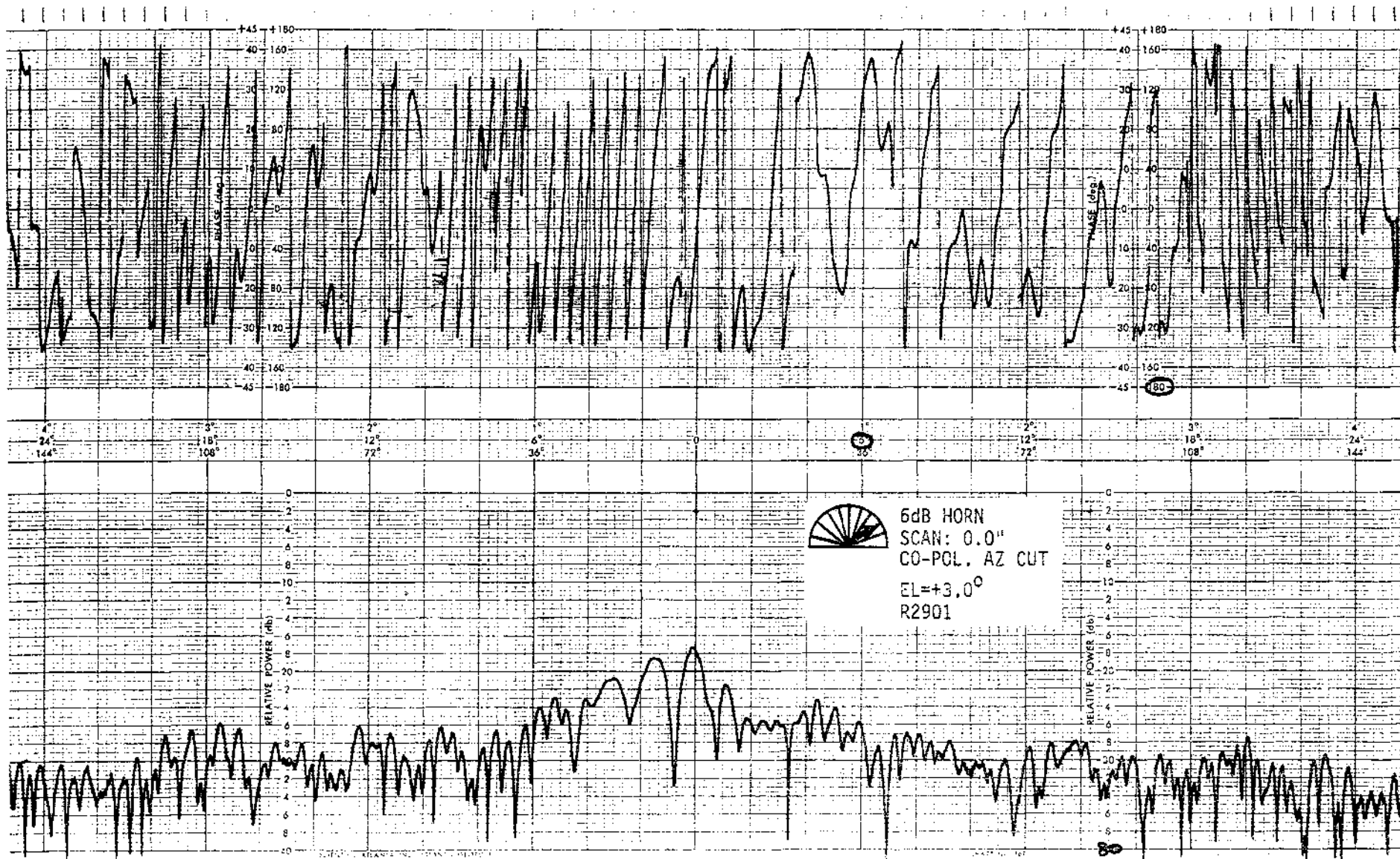


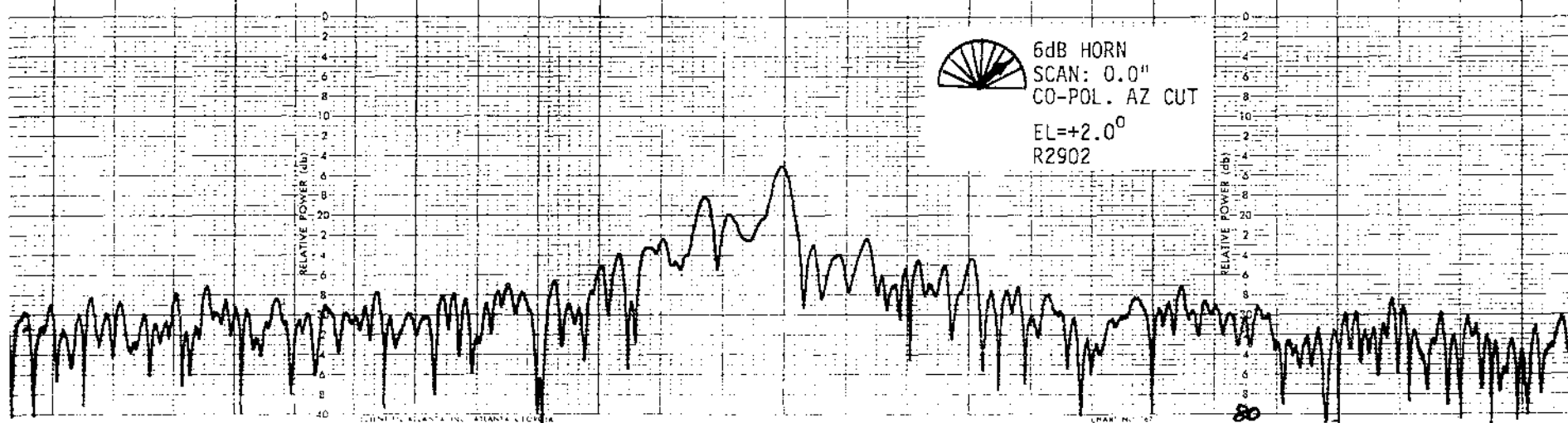
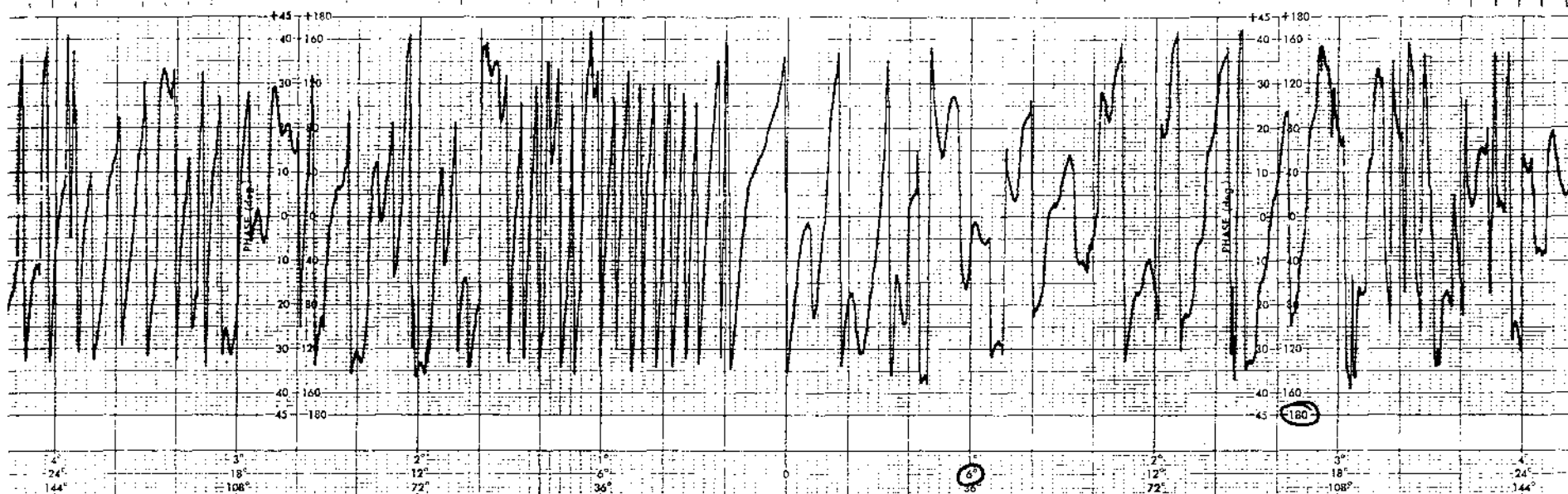


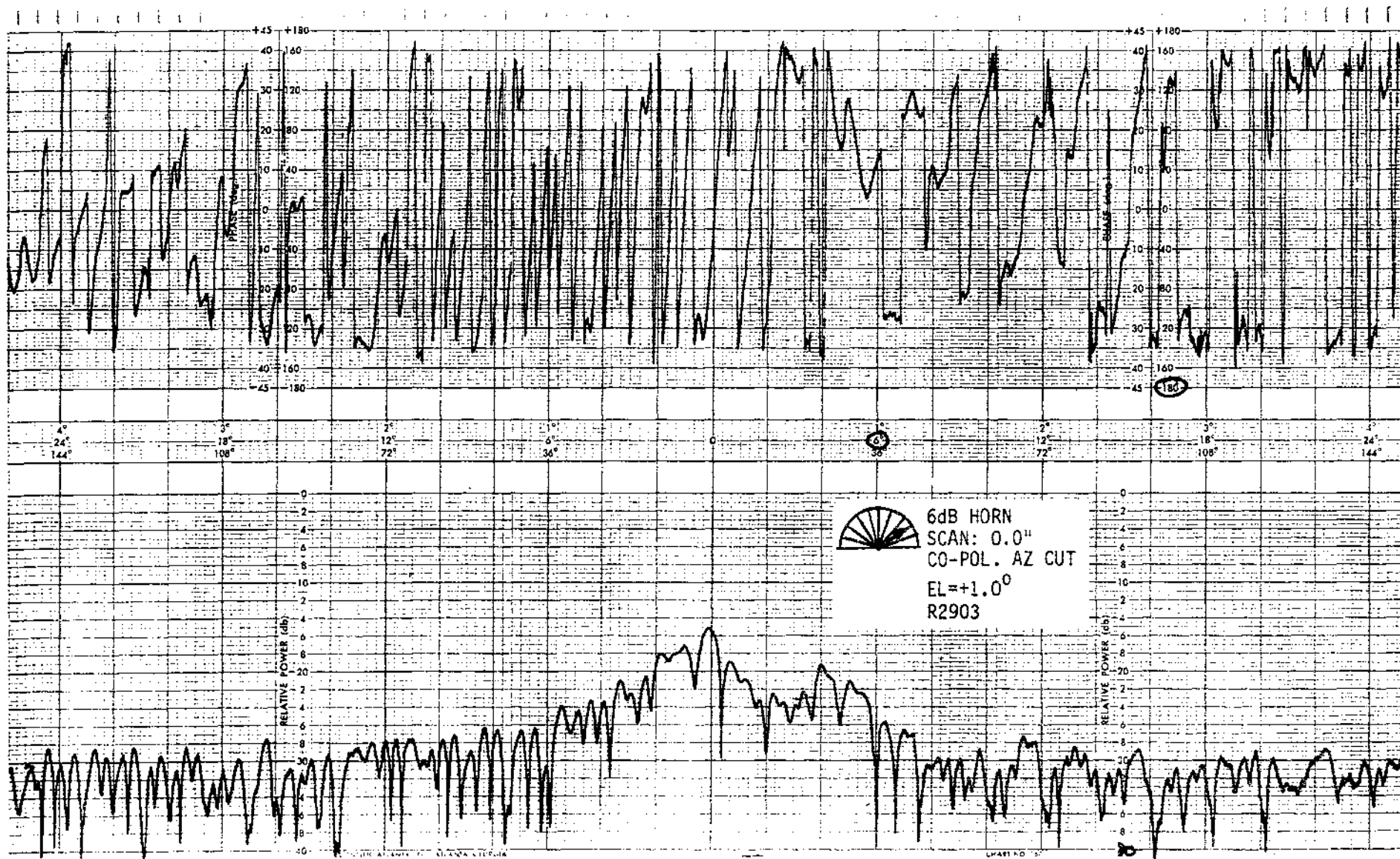


LSST - VISECONDARY PATTERN LOG

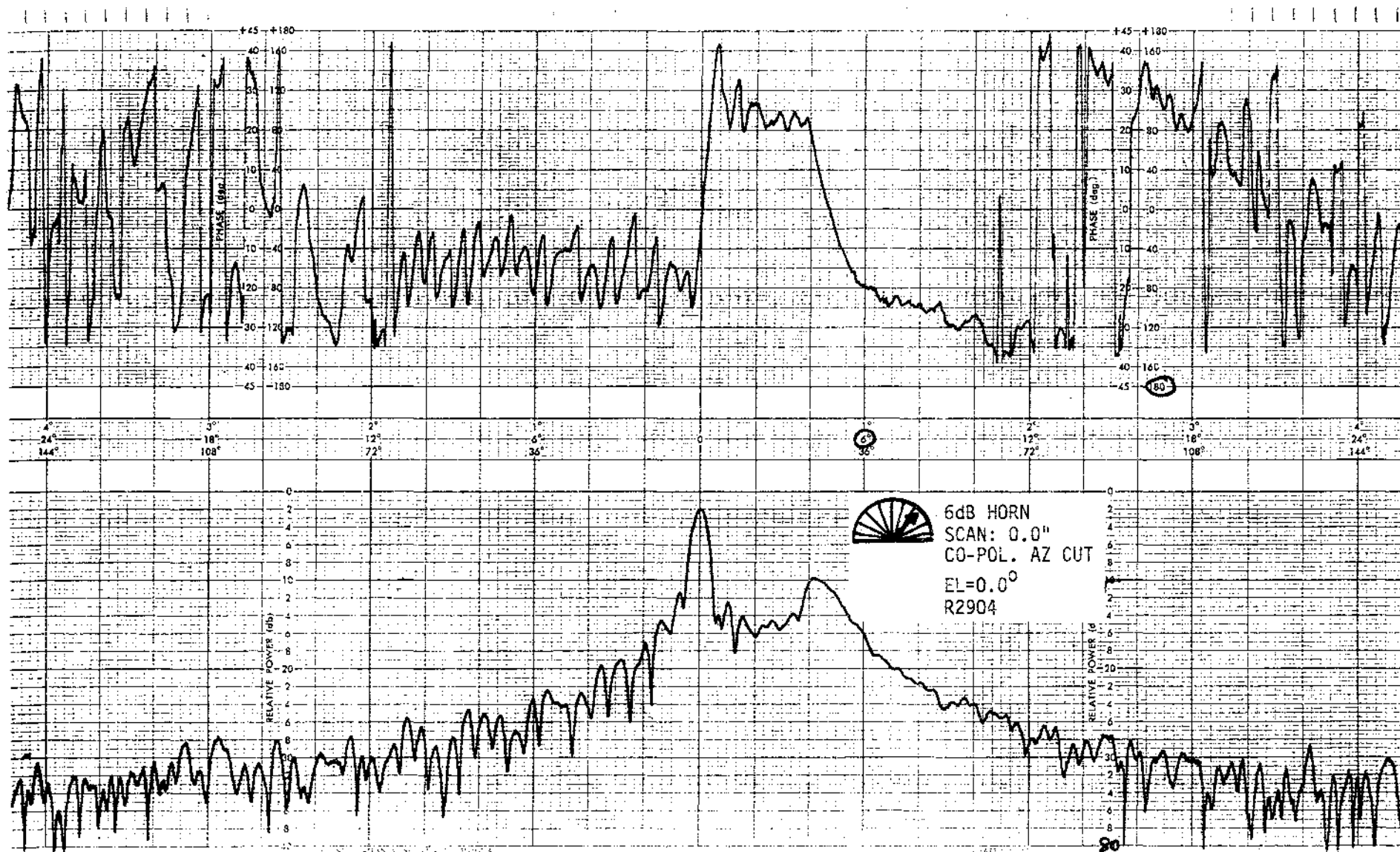
<u>CONFIGURATION</u>	<u>HORN</u>	<u>SCAN</u>	<u>POL.</u>	<u>PK. GAIN</u>	<u>PATTERN</u>	<u>FILE NAME</u>	<u>PAGE NUMBER</u>
	6 dB	0.0"	CO	-	+3°EL ± 45°AZ	R2901	186
	"	"	"	-	+2°EL "	R2902	187
	"	"	"	-	+1°EL "	R2903	188
	"	"	"	50.80	0°EL "	R2904	189
	"	"	"	-	-1°EL "	R2905	190
	"	"	"	-	-2°EL "	R2906	191
	"	"	"	-	-3°EL "	R2907	192
	6 dB	0.0"	X	-	+3°EL ± 45°AZ	R3001	193
	"	"	"	-	+2°EL "	R3002	194
	"	"	"	-	+1°EL "	R3003	195
	"	"	"	-	0°EL "	R3004	196
	"	"	"	-	-1°EL "	R3005	197
	"	"	"	-	-2°EL "	R3006	198
	"	"	"	-	-3°EL "	R3007	199
	6 dB	0.0"	CO	-	+3°EL ± 45°AZ	R2701	200
	"	"	"	-	+2°EL "	R2702	201
	"	"	"	-	+1°EL "	R2703	202
	"	"	"	50.65	0°EL "	R2704	203
	"	"	"	-	-1°EL "	R2705	204
	"	"	"	-	-2°EL "	R2706	205
	"	"	"	-	-3°EL "	R2707	206
	6 dB	0.0"	X	-	+3°EL ± 45°AZ	R2801	207
	"	"	"	-	+2°EL "	R2802	208
	"	"	"	-	+1°EL "	R2803	209
	"	"	"	-	0°EL "	R2804	210
	"	"	"	-	-1°EL "	R2805	211
	"	"	"	-	-2°EL "	R2806	212
	"	"	"	-	-3°EL "	R2807	213



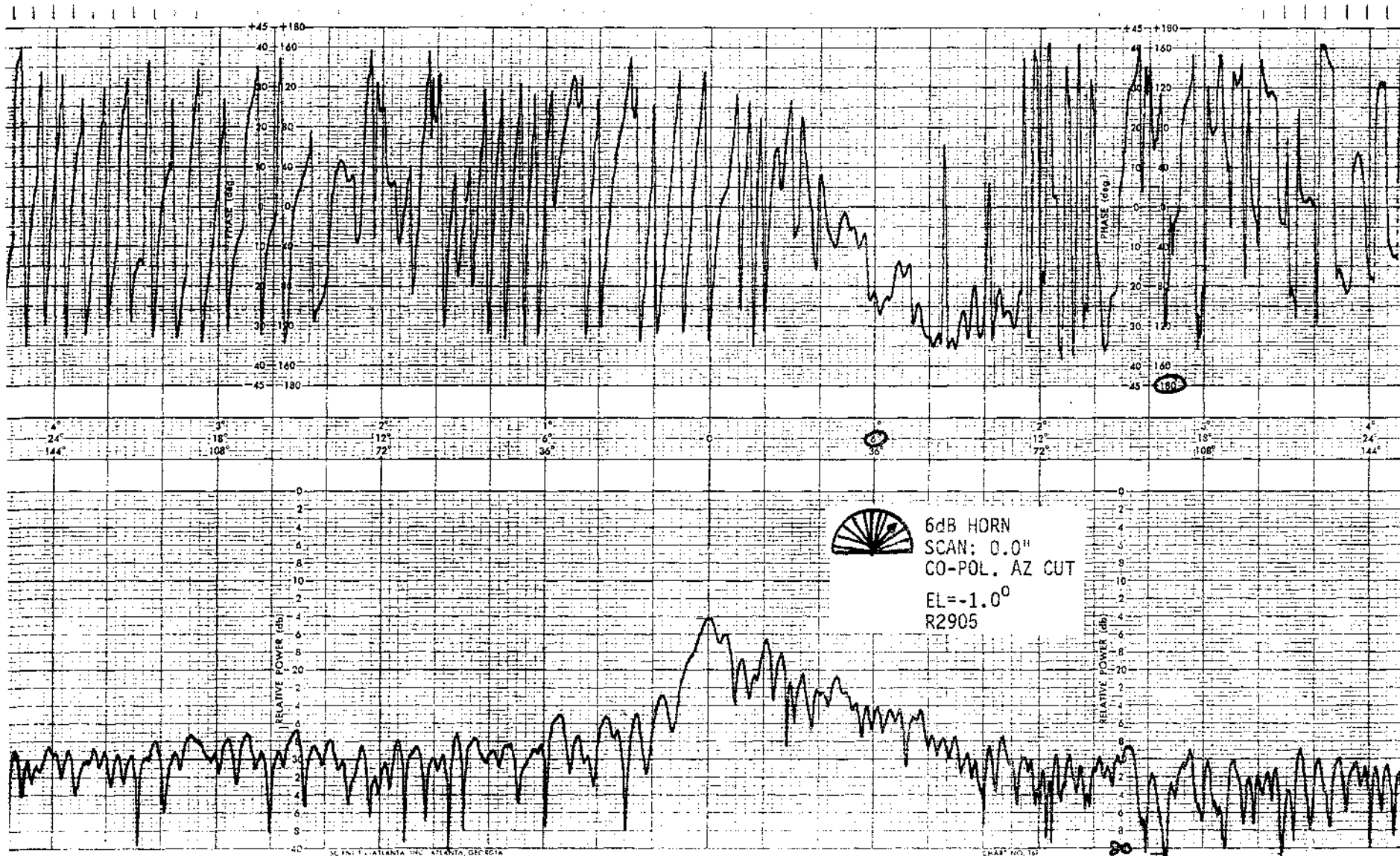


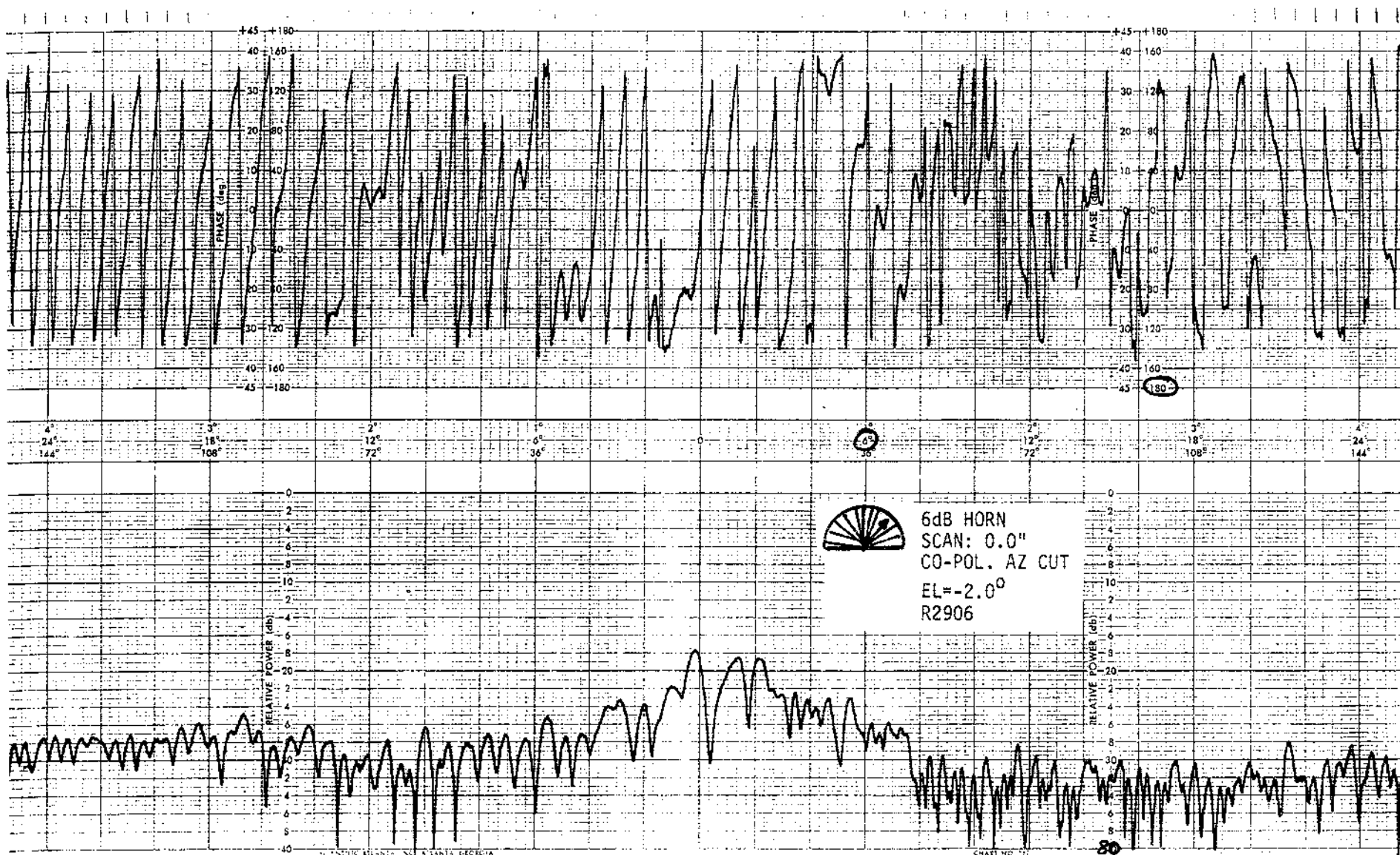


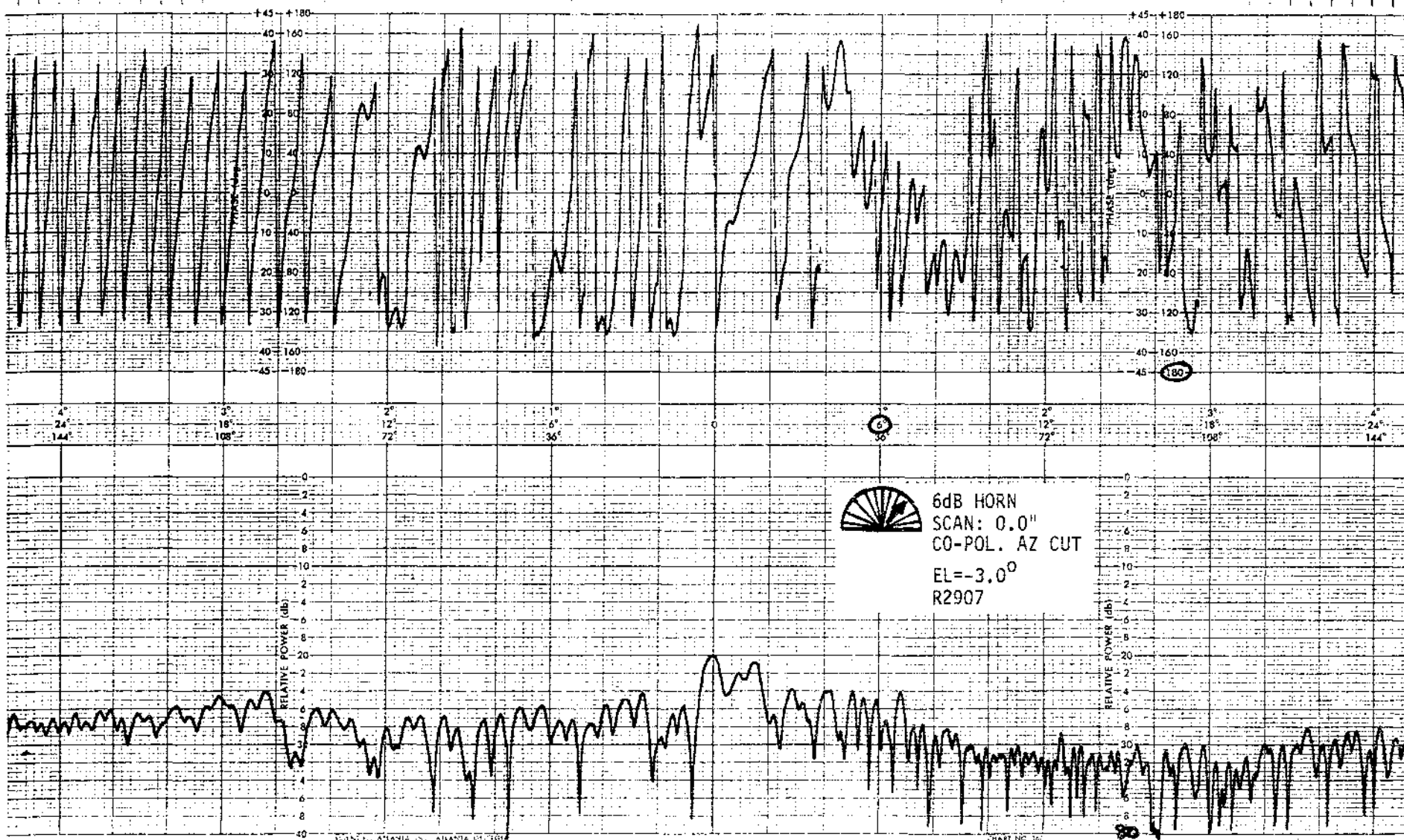


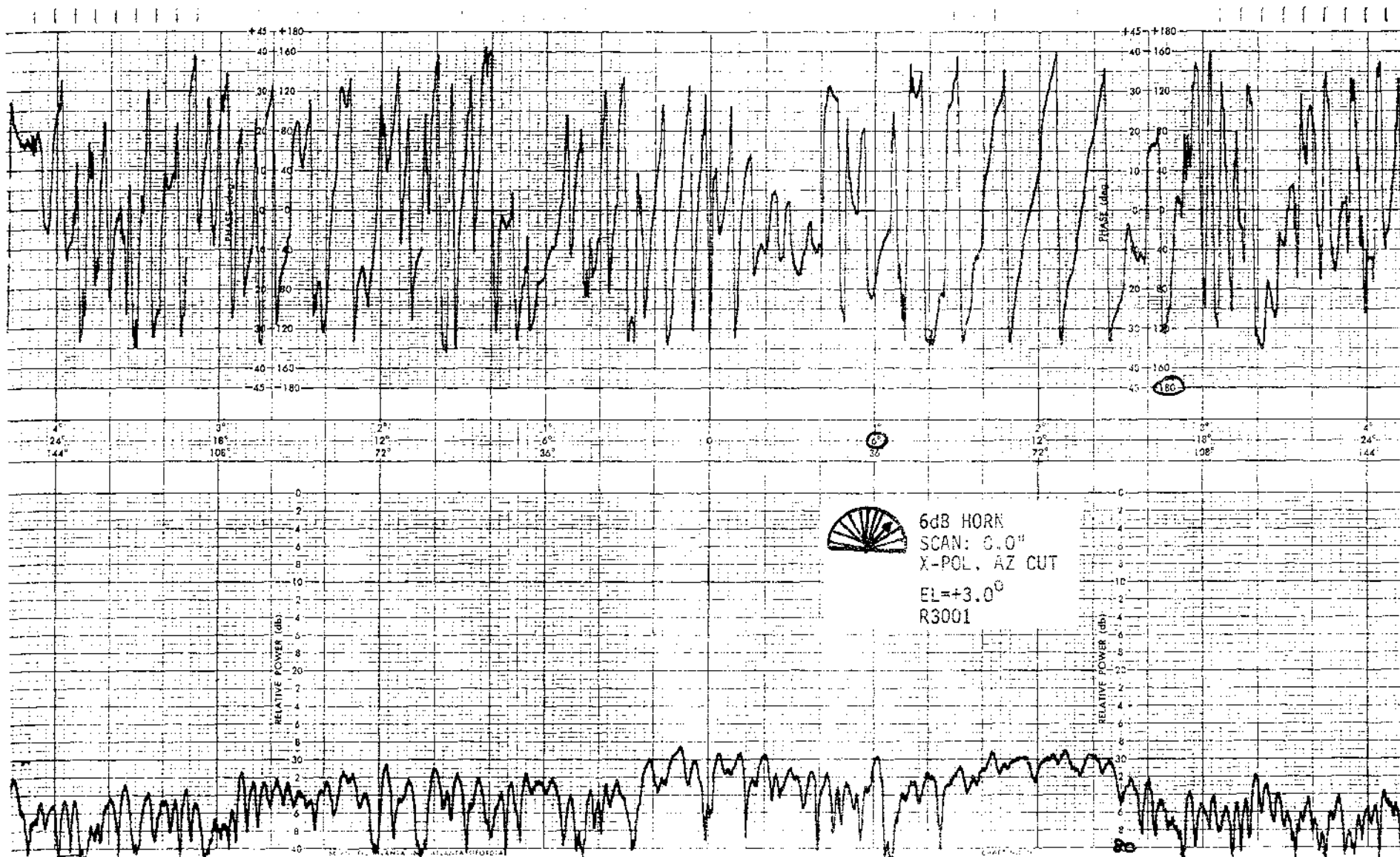


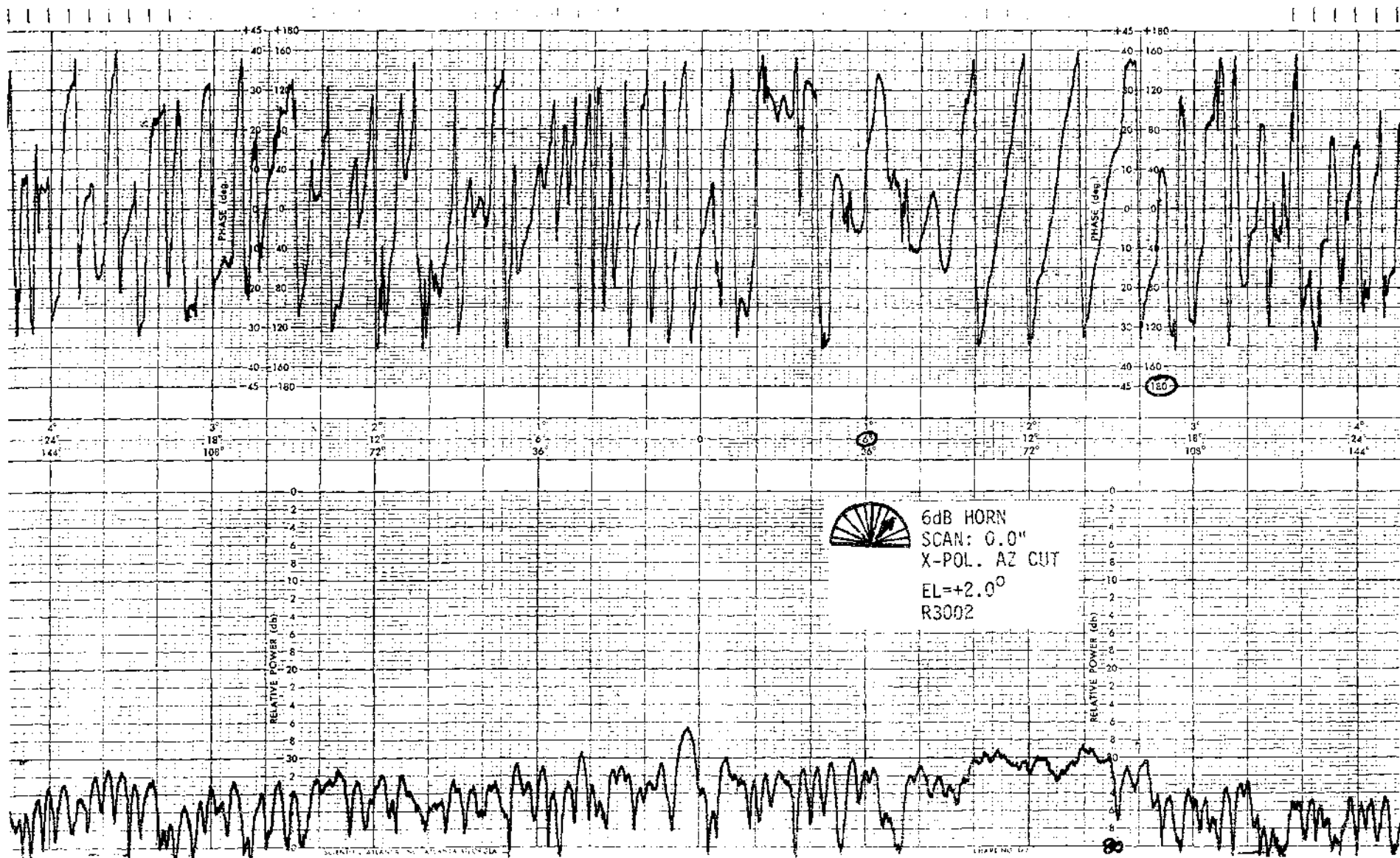


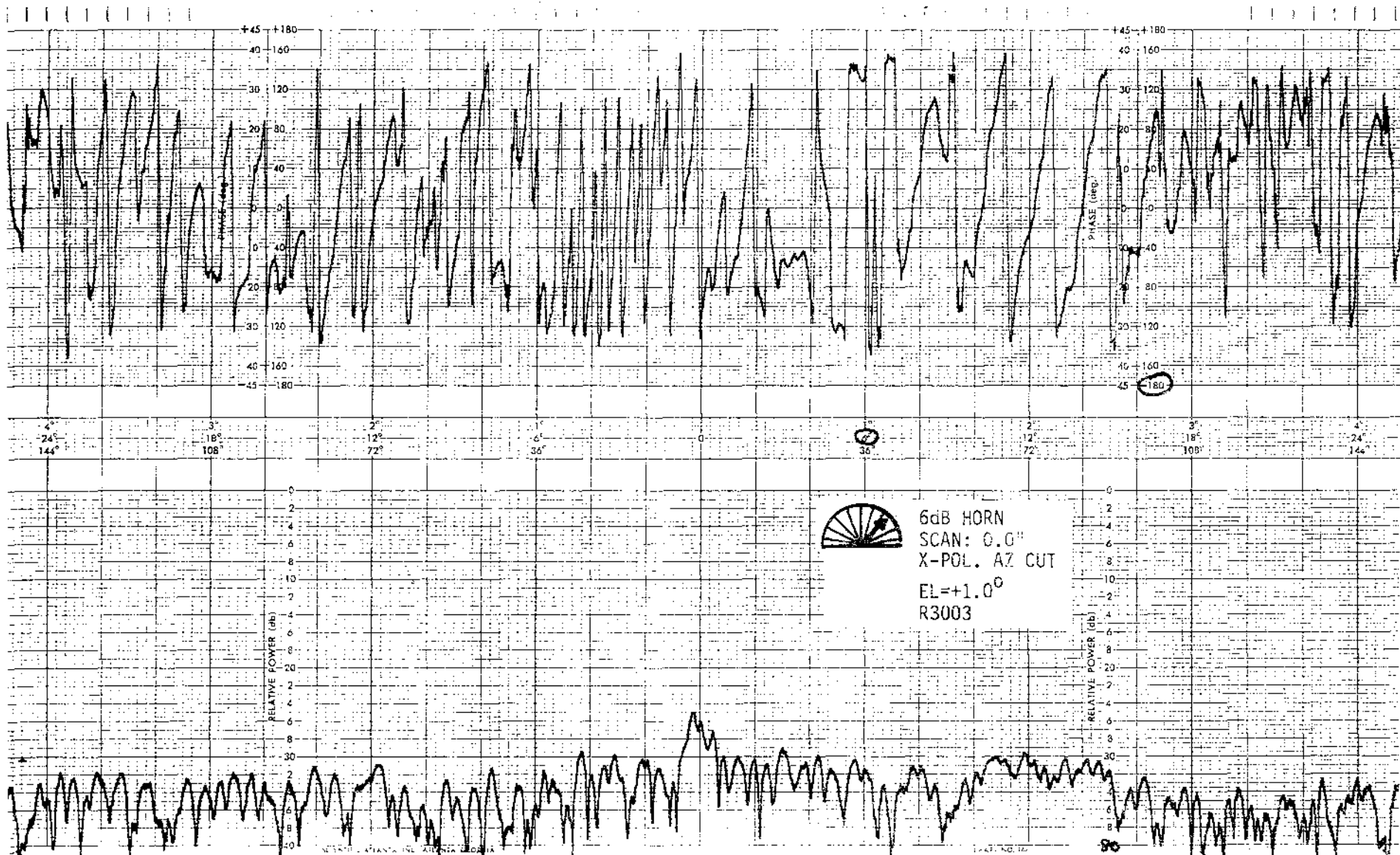




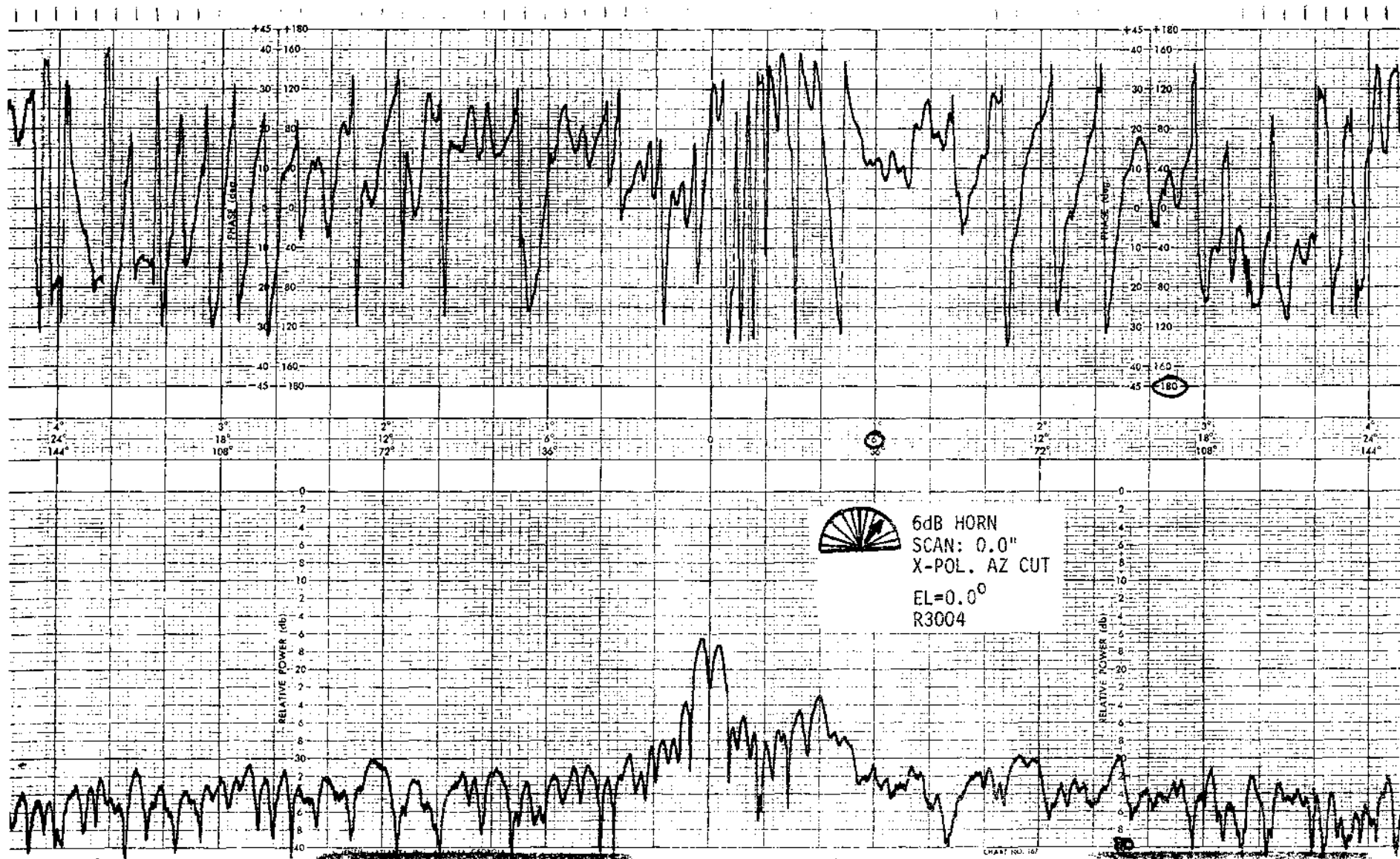


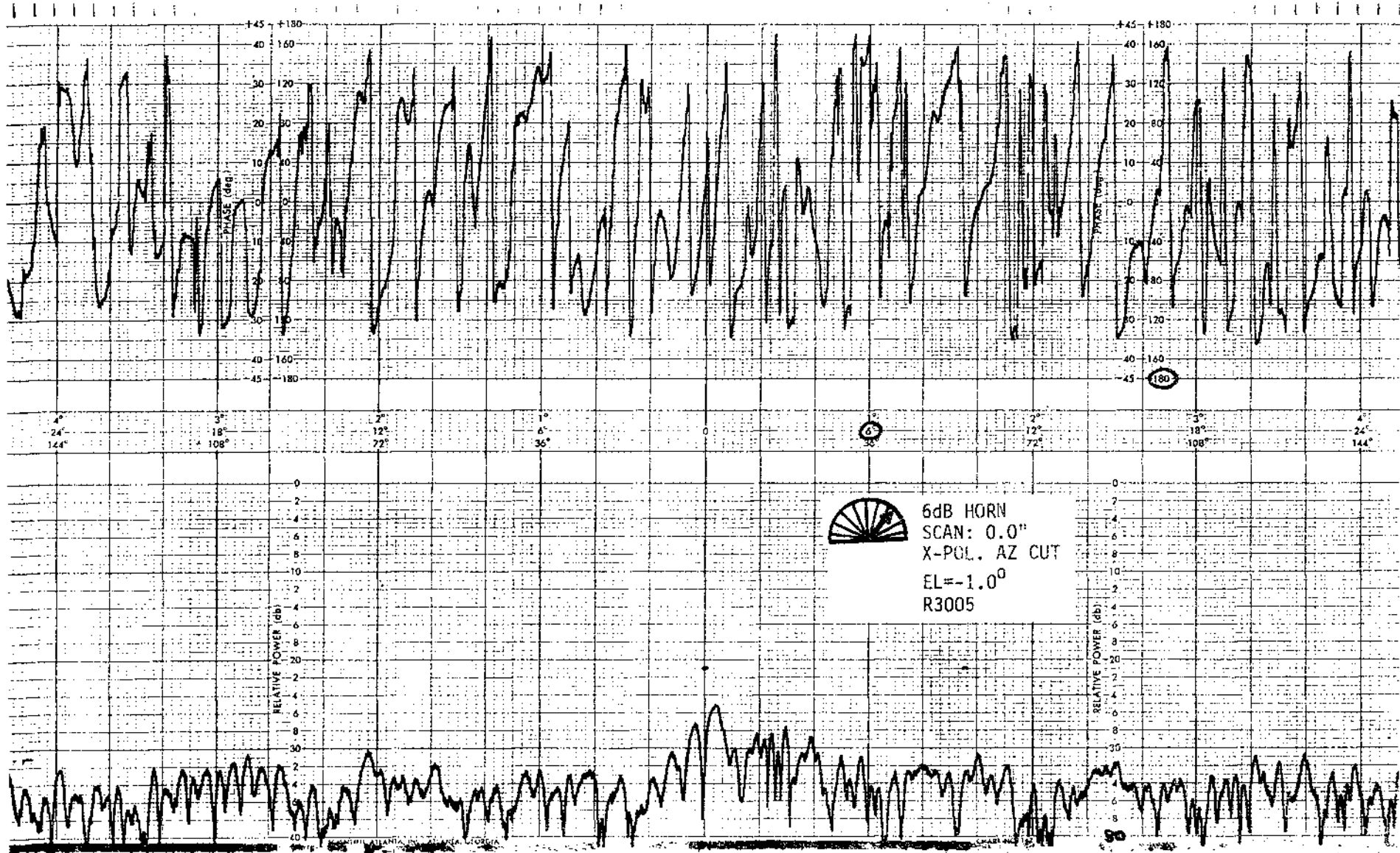








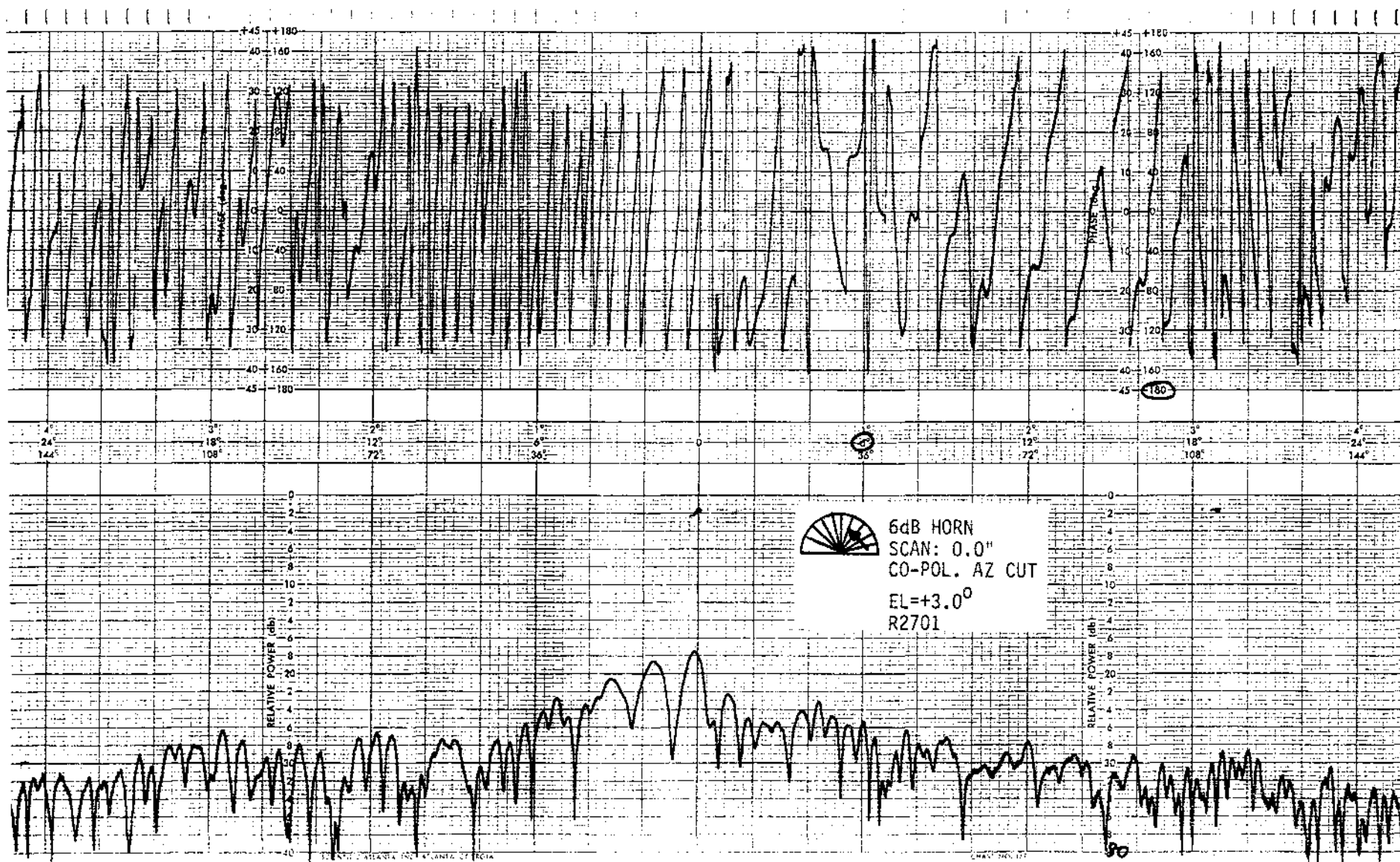


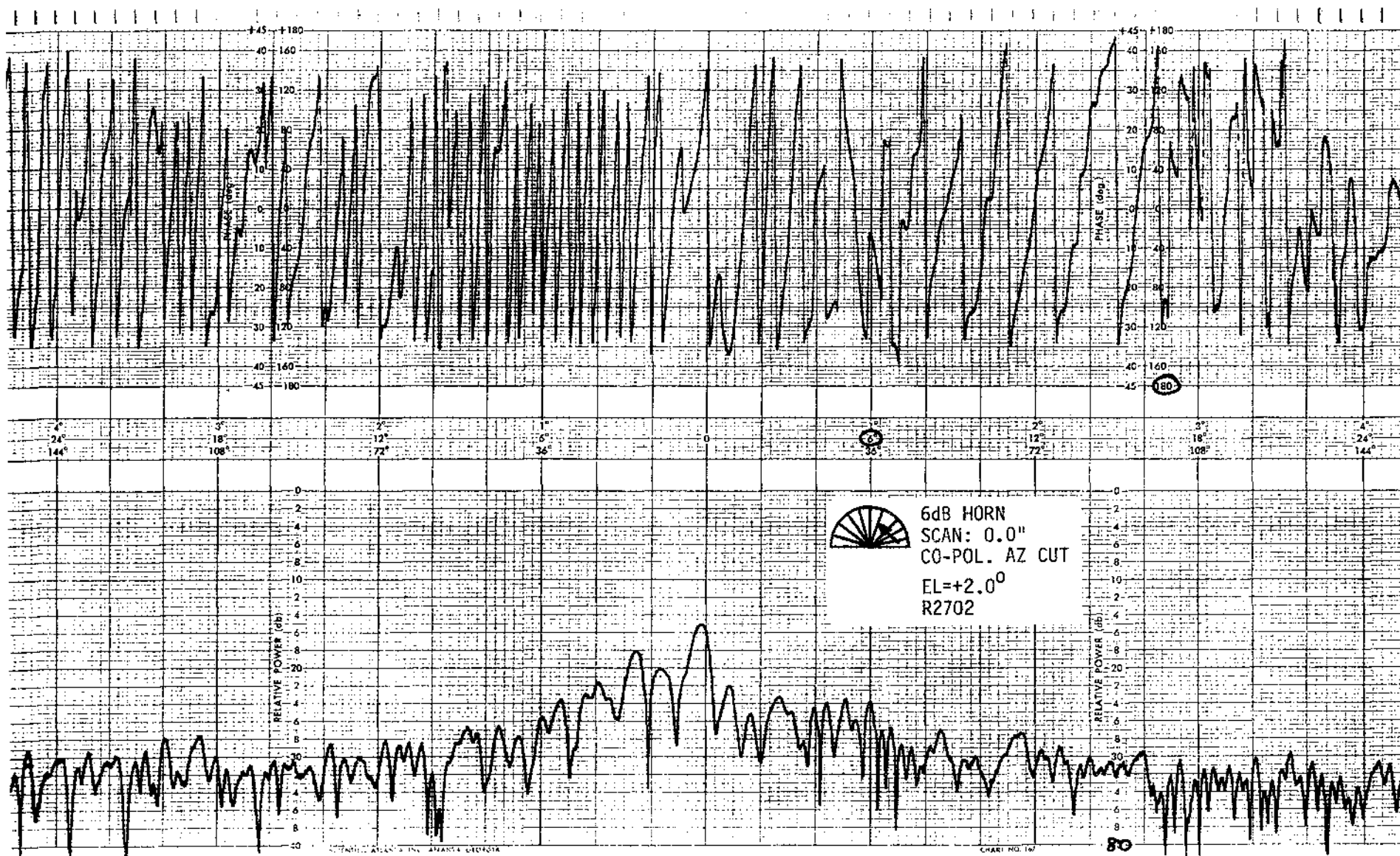


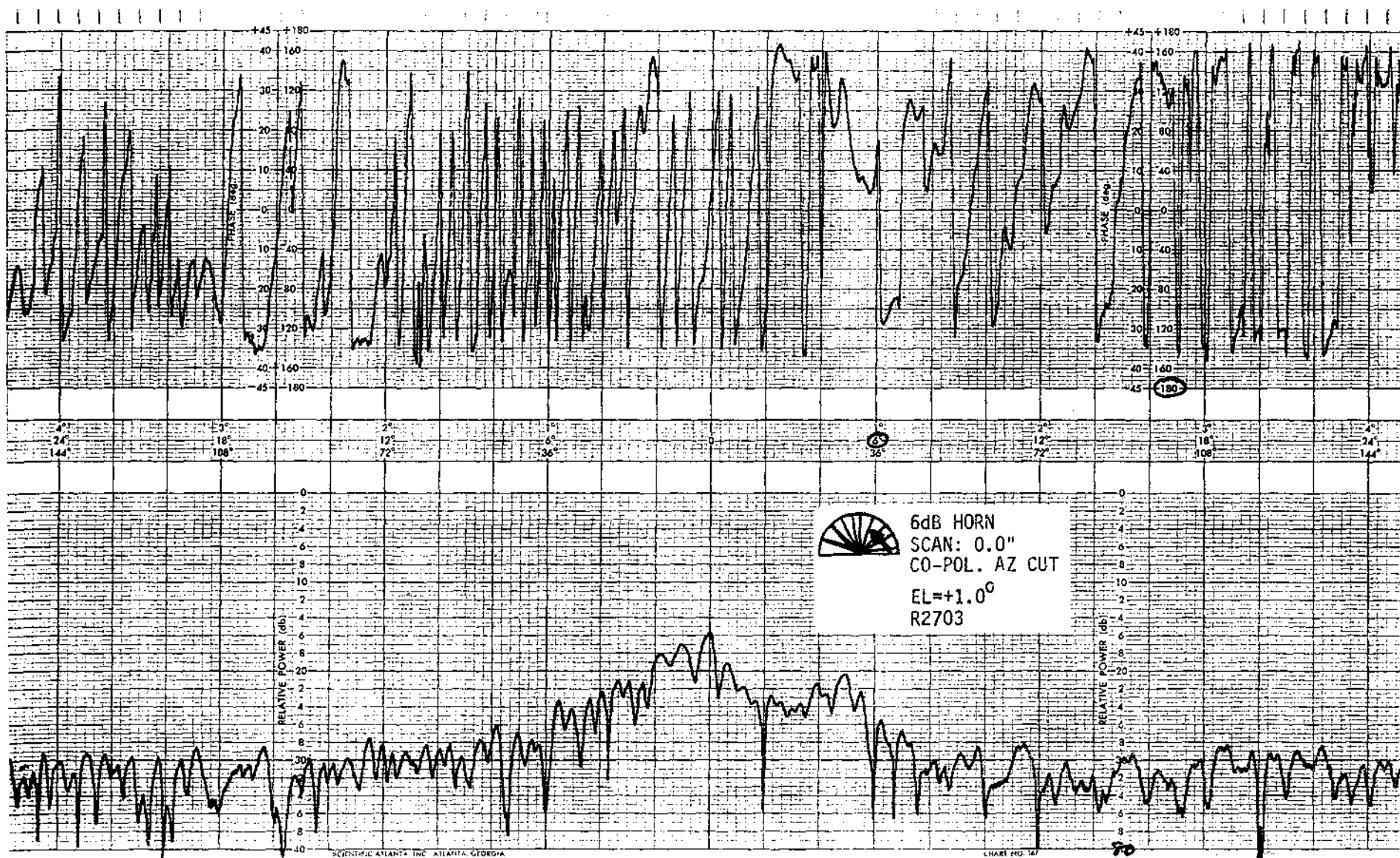




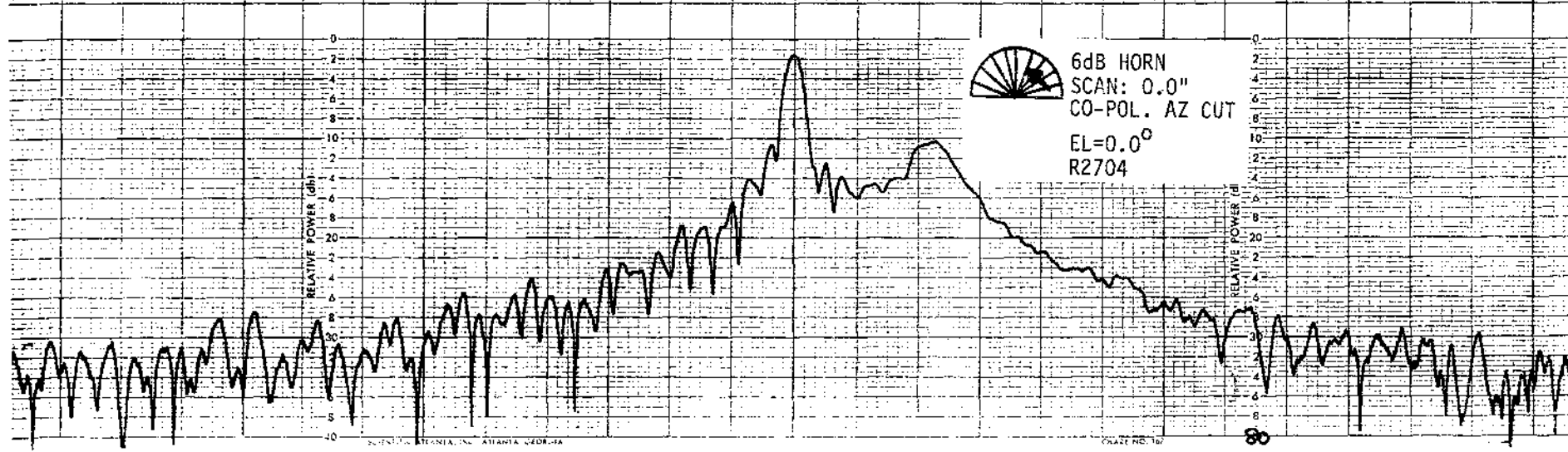
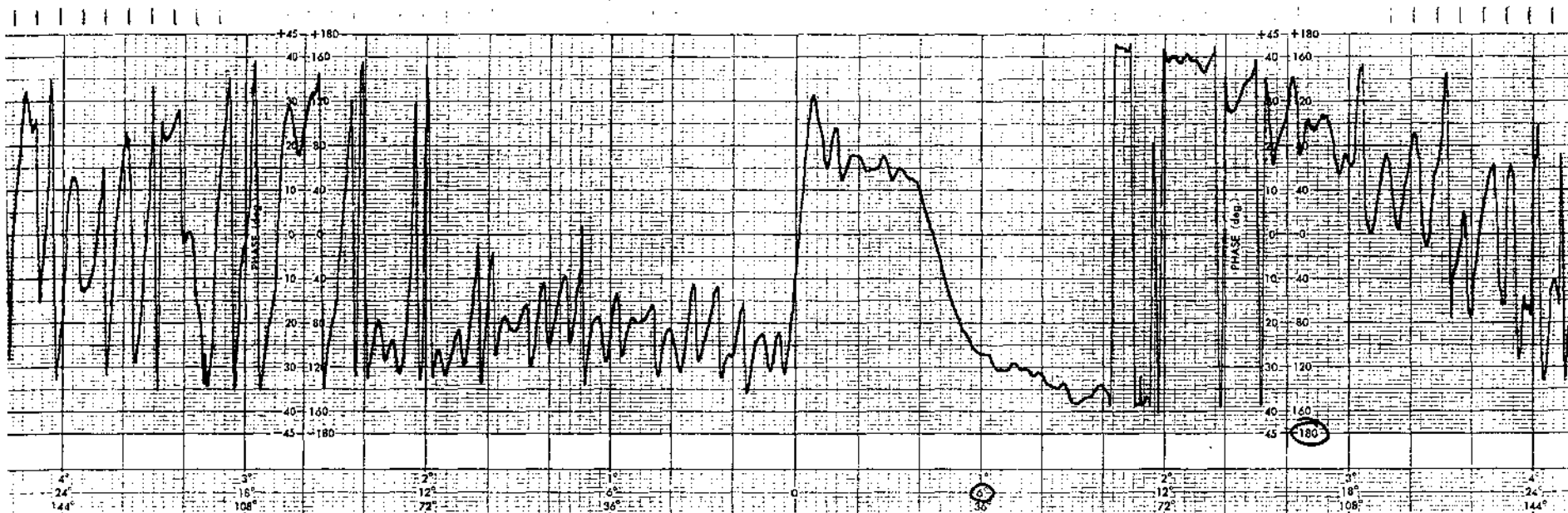


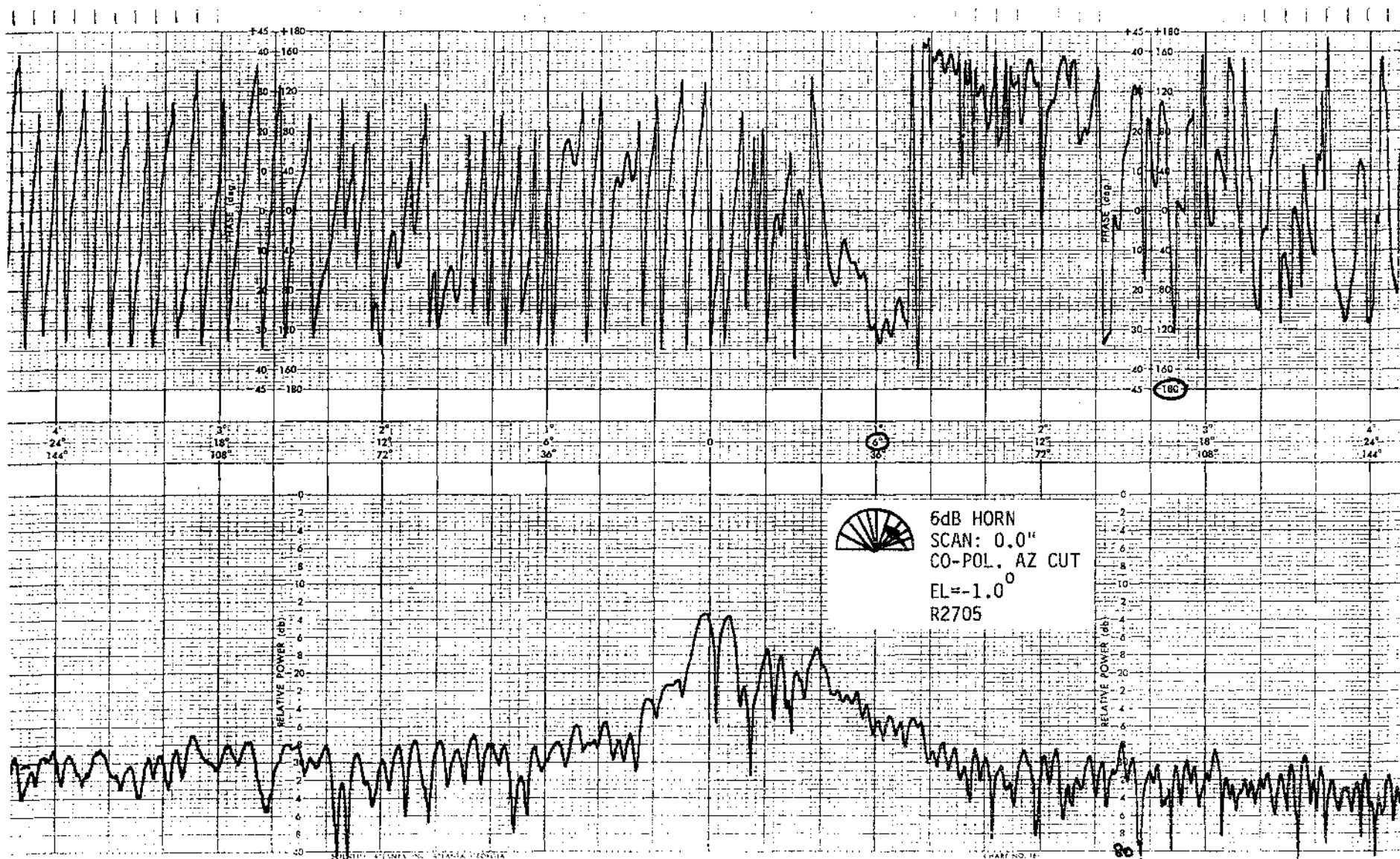


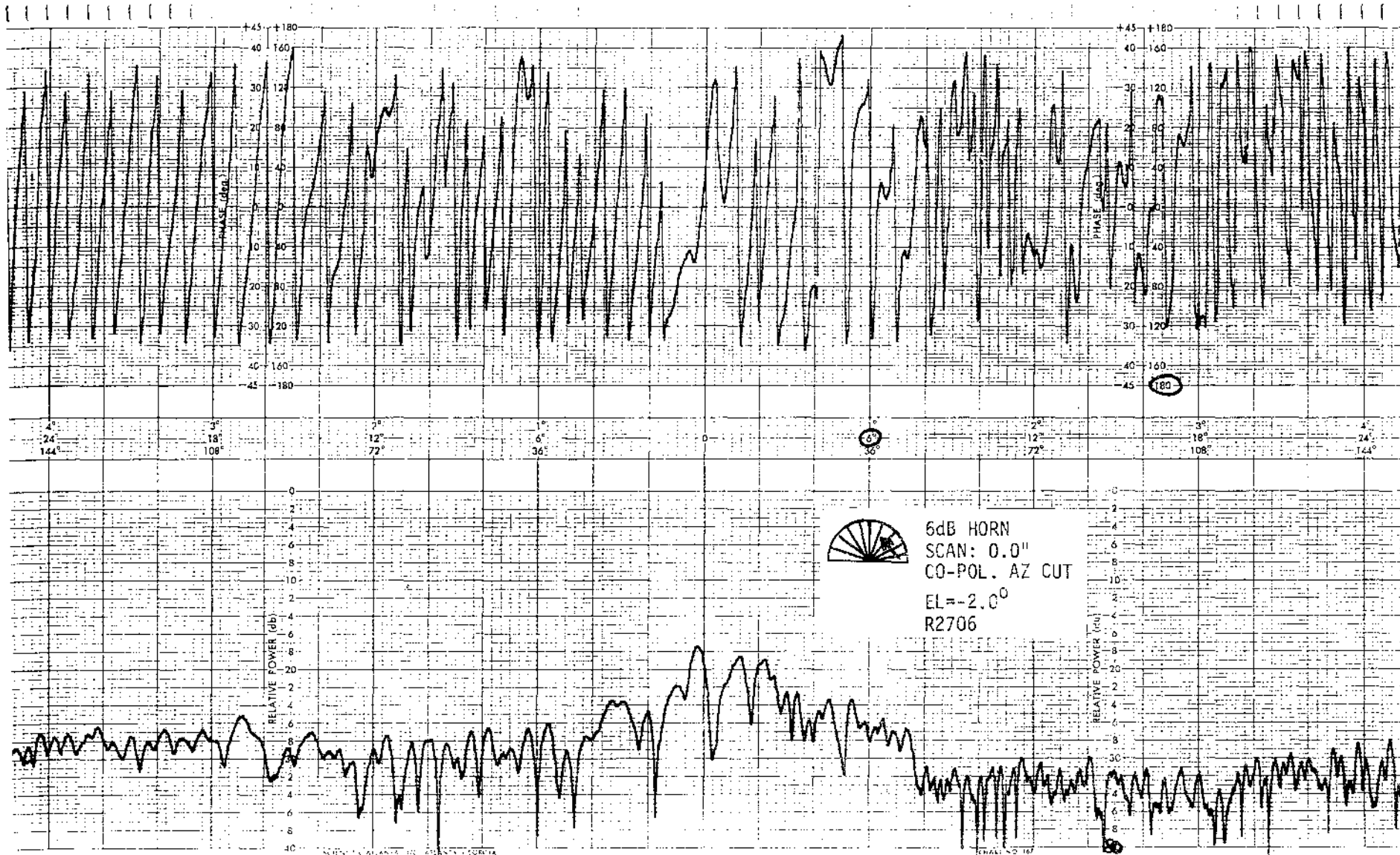




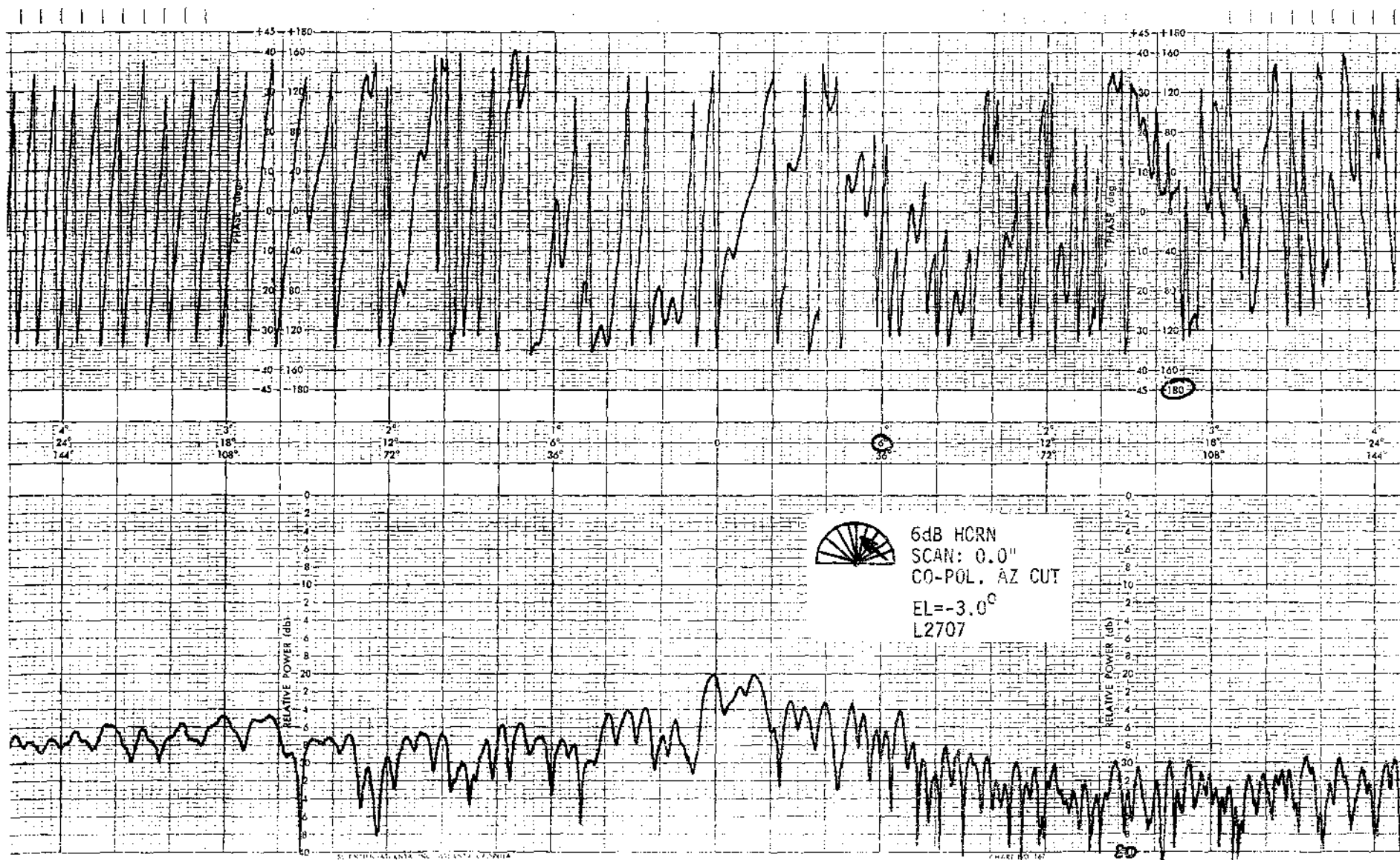


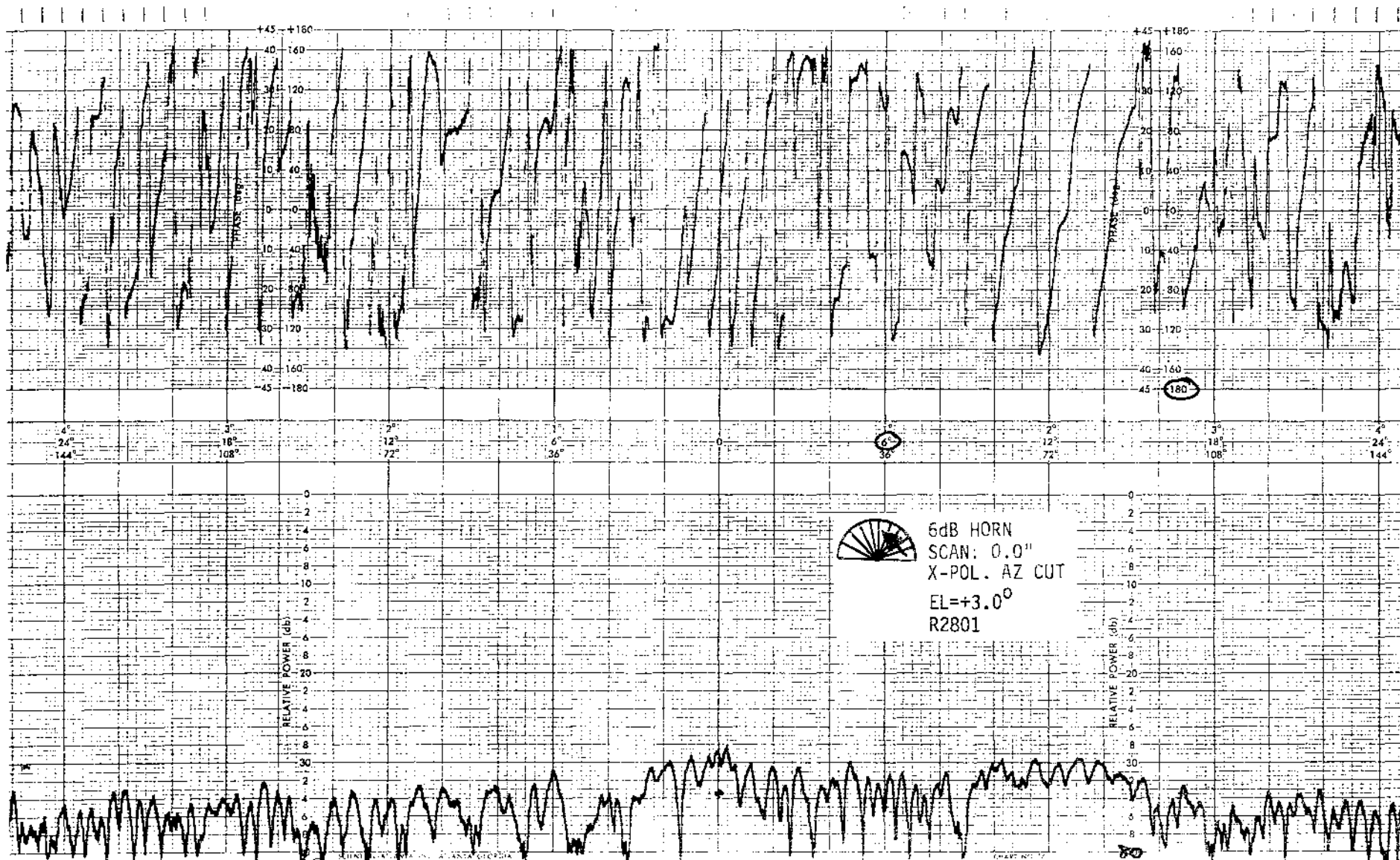


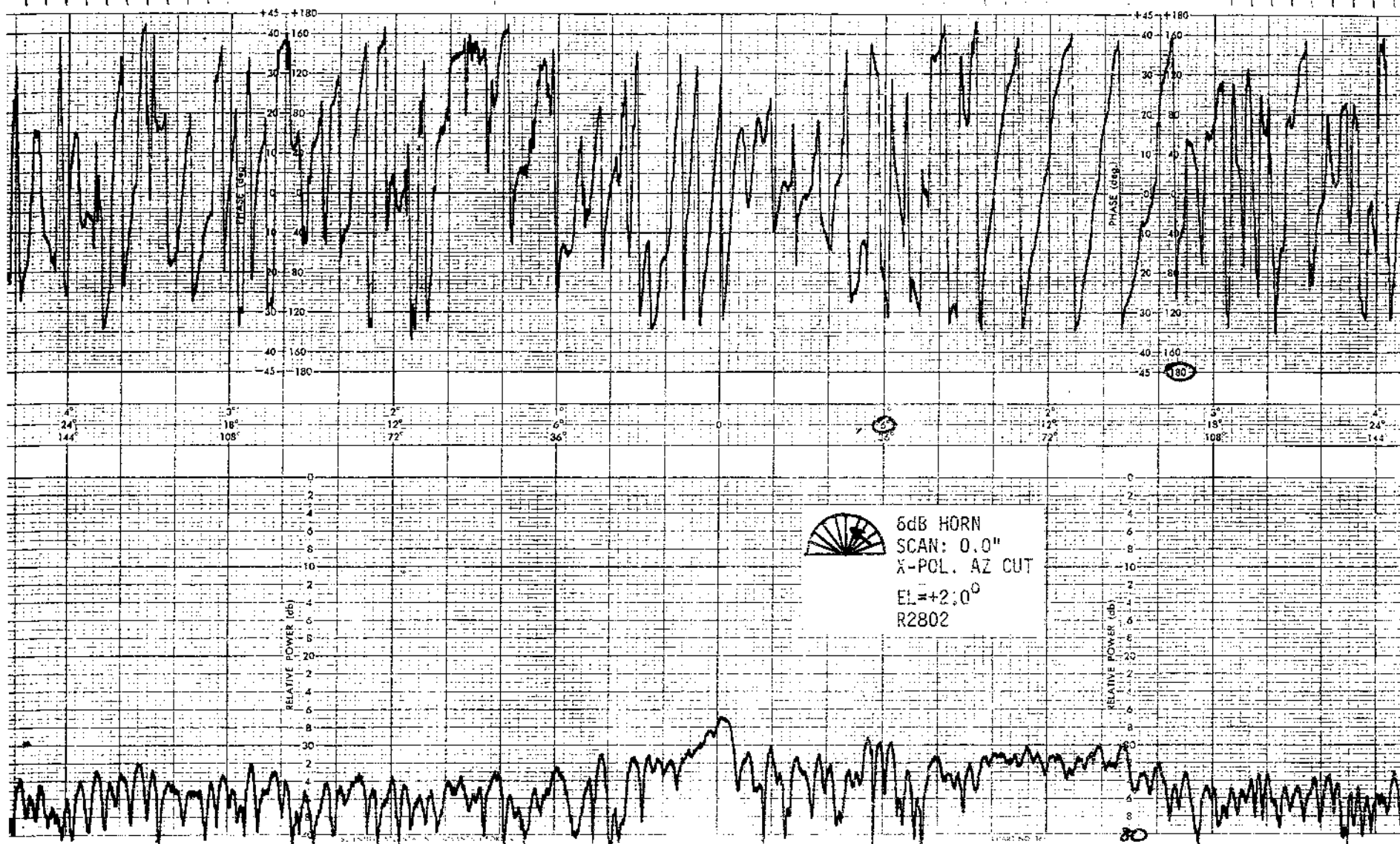




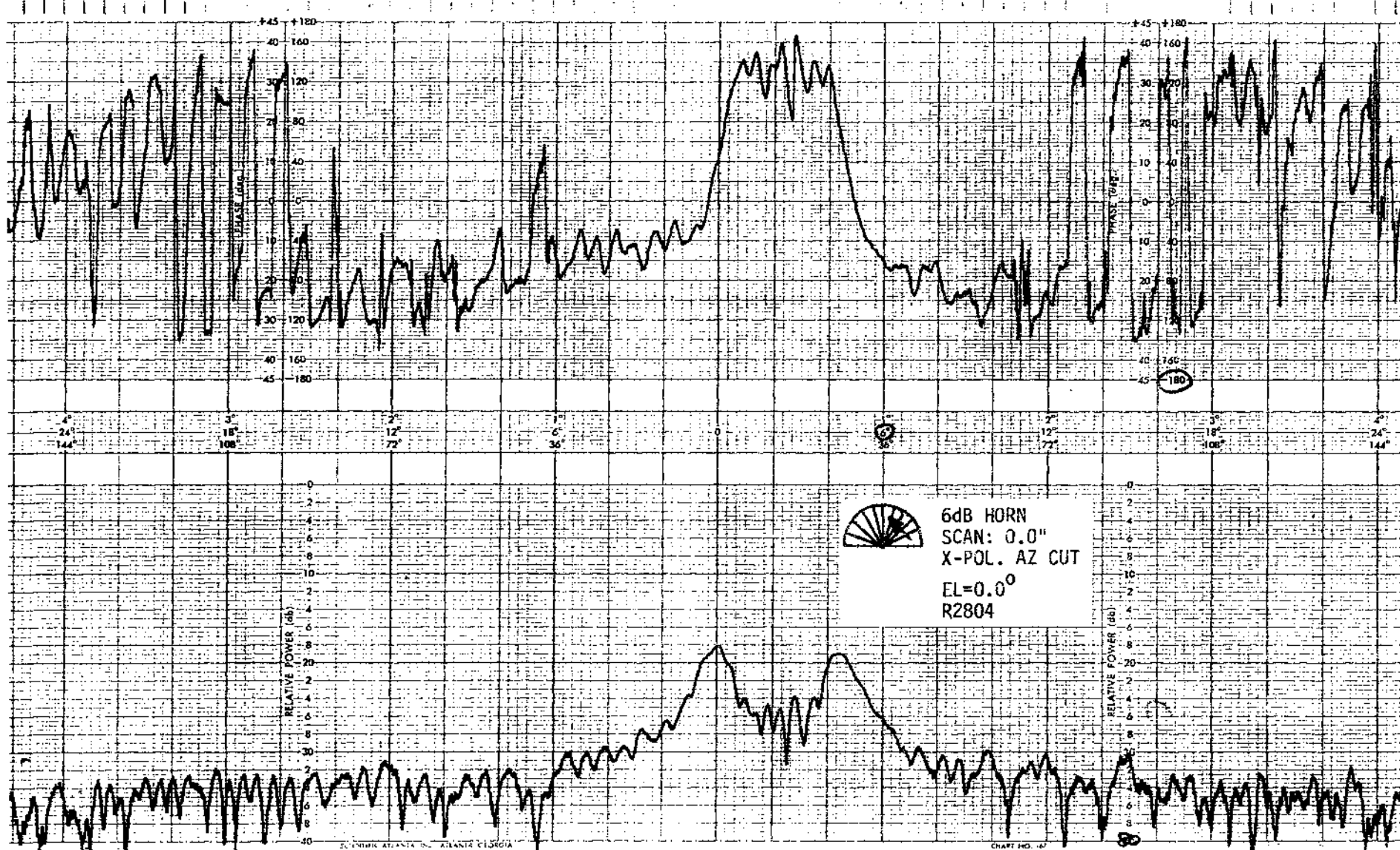


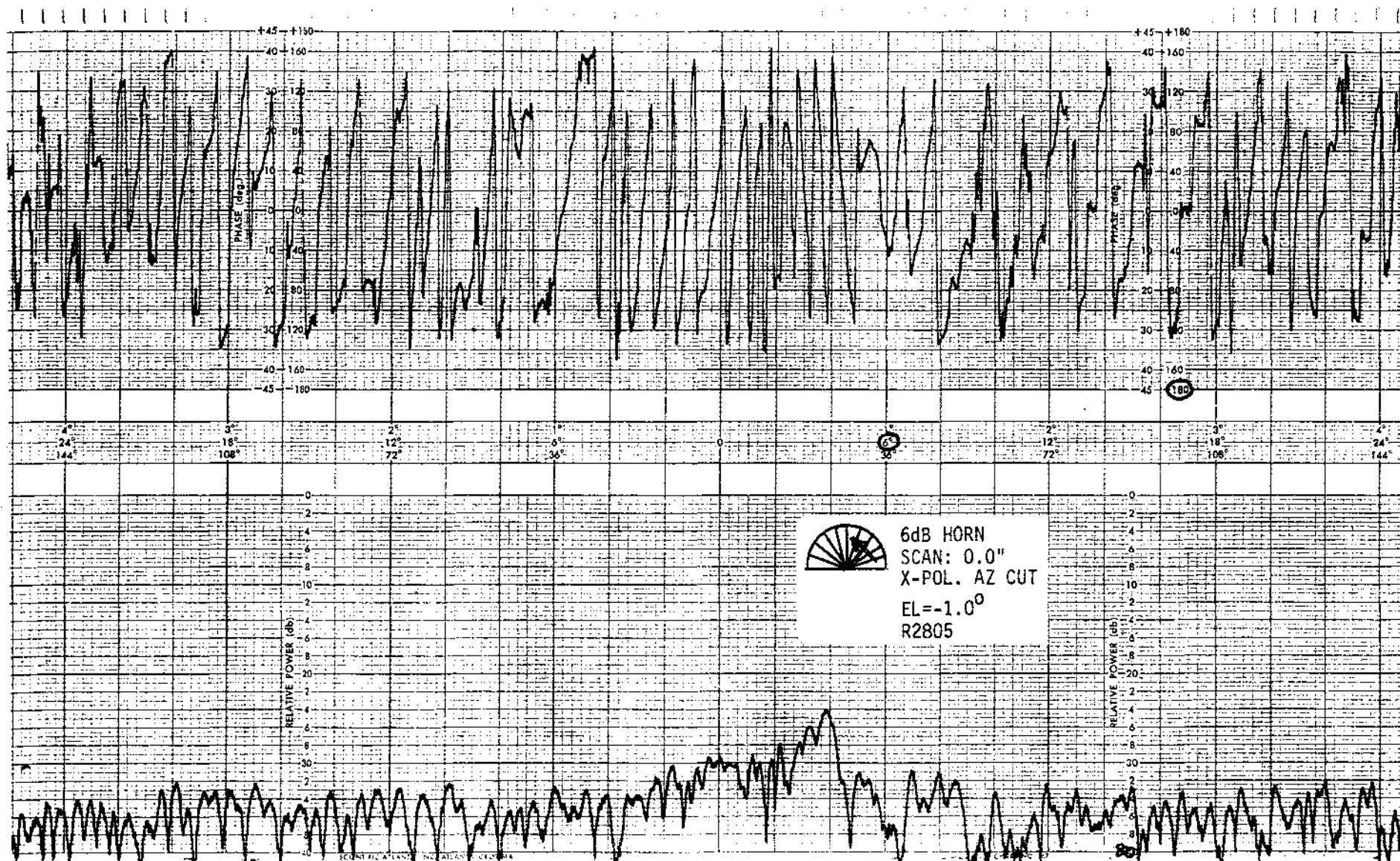




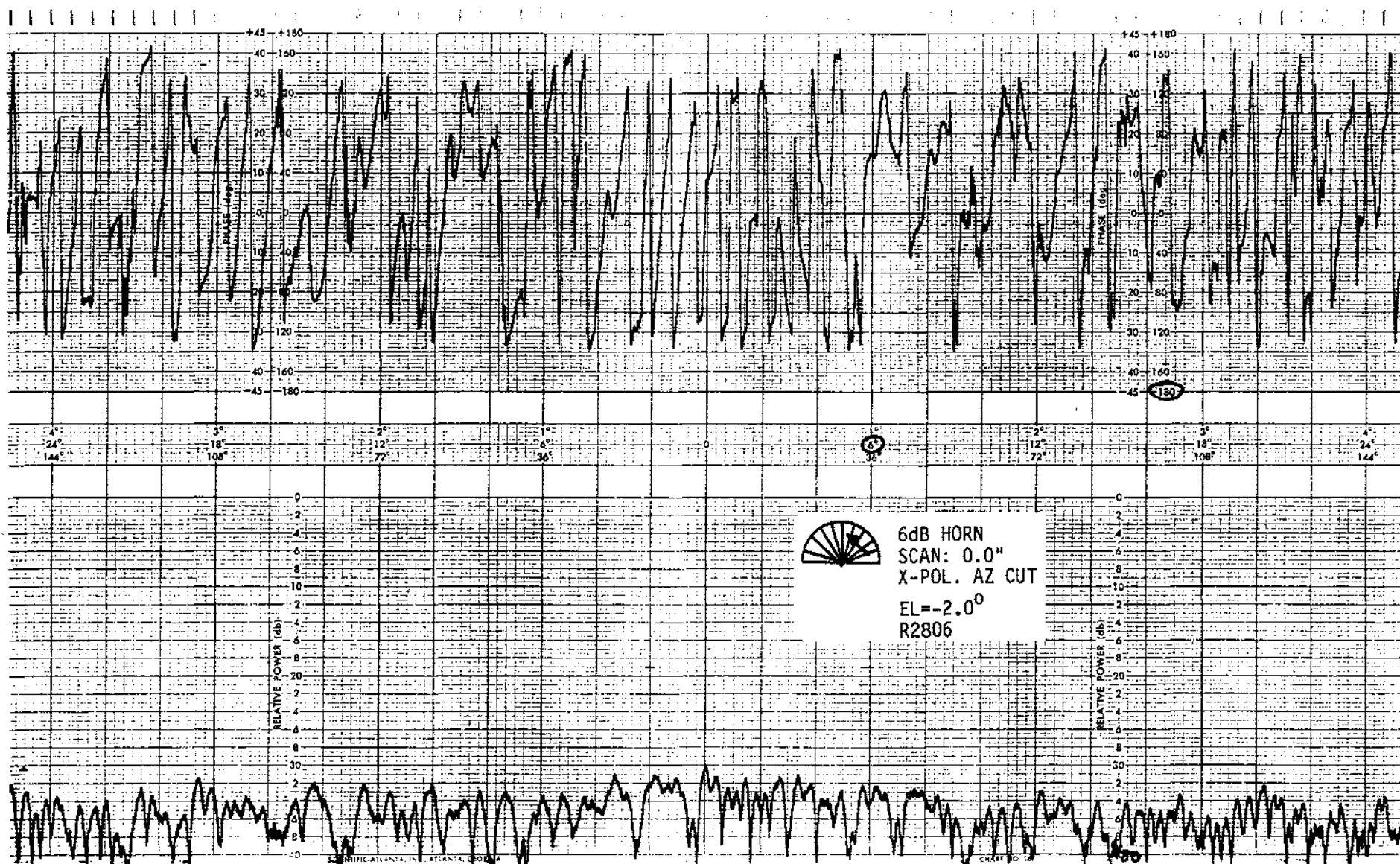









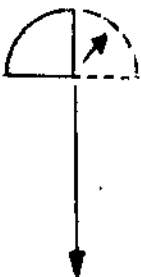



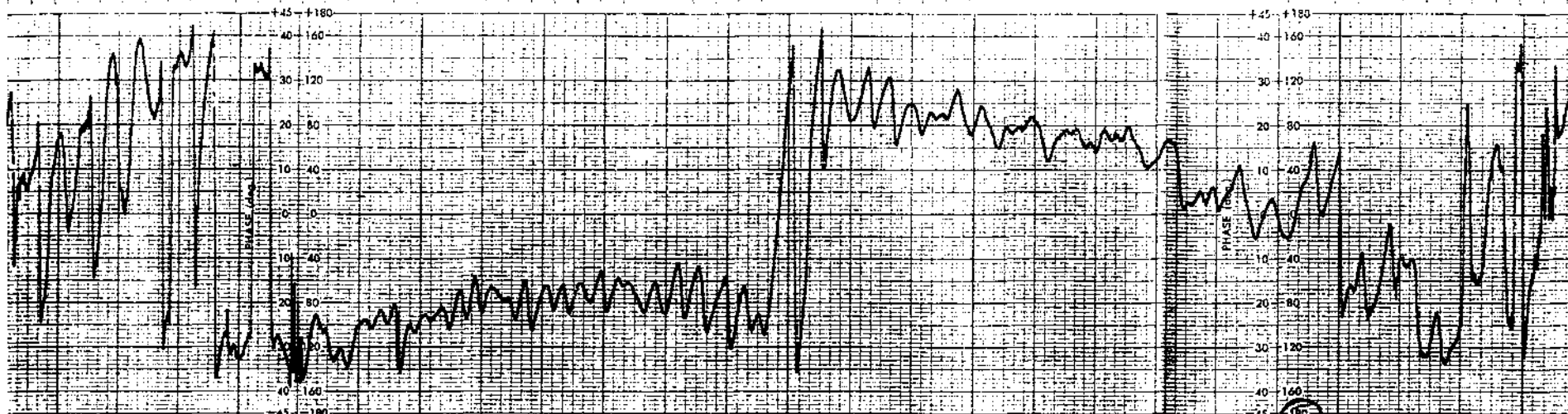




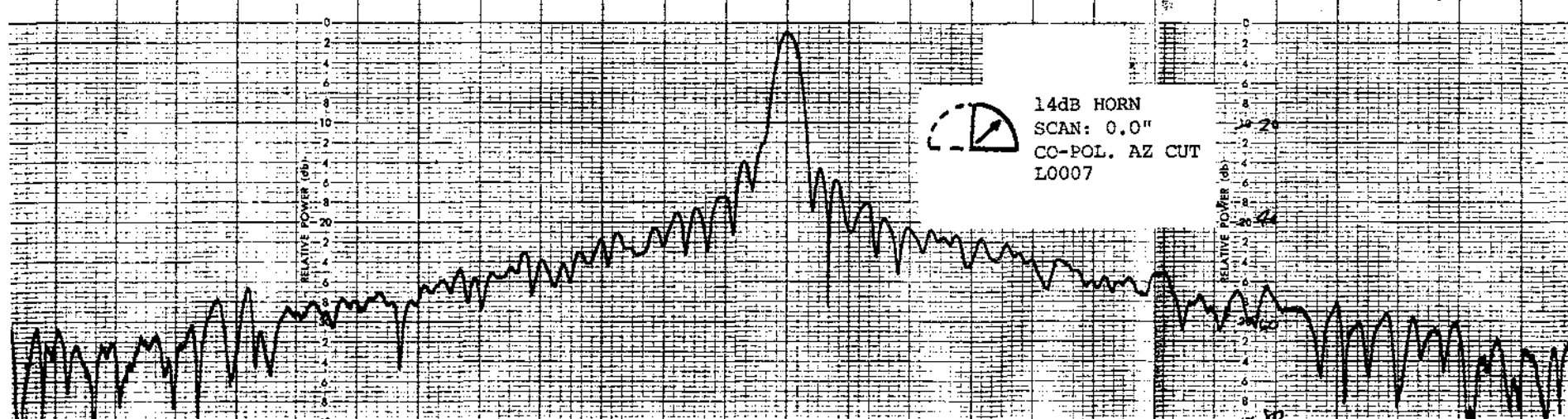


LSST - VIISECONDARY PATTERN LOG

<u>CONFIGURATION</u>	<u>HORN</u>	<u>SCAN</u>	<u>POL.</u>	<u>PK. GAIN</u>	<u>PATTERN</u>	<u>FILE NAME</u>	<u>PAGE NUMBER</u>
	14 dB	0.0"	CO	50.52	$\pm 45^\circ$ AZ	L0007	215
	"	"	CO	"	$\pm 5^\circ$ AZ	L0008	216
	"	"	CO	"	$\pm 5^\circ$ EL	L0009	217
	"	"	X	-	$\pm 45^\circ$ AZ	L0010	218
	"	"	X	-	$\pm 5^\circ$ AZ	L0011	219
	"	"	X	-	$\pm 5^\circ$ EL	L0012	220
	14 dB	4.5"	CO	50.35	$\pm 45^\circ$ AZ	L0017	221
	"	"	CO	"	$\pm 5^\circ$ AZ	L0015	222
	"	"	CO	"	$\pm 5^\circ$ EL	L0016	223
	"	"	X	-	$\pm 45^\circ$ AZ	L0020	224
	"	"	X	-	$\pm 5^\circ$ AZ	L0018	225
	"	"	X	-	$\pm 5^\circ$ EL	L0019	226
	14 dB	6.5"	CO	50.05	$\pm 45^\circ$ AZ	AAN45	227
	"	"	CO	"	$\pm 5^\circ$ AZ	AANC1	228
	"	"	CO	"	$\pm 5^\circ$ EL	EANC1	229
	"	"	X	-	$\pm 45^\circ$ AZ	AXPSC	230
	"	"	X	-	$\pm 5^\circ$ AZ	AZPSC	231
	"	"	X	-	$\pm 5^\circ$ EL	EXPSC	232
	14 dB	0.0"	CO	32.15	$\pm 45^\circ$ AZ	L0068	233
	"	"	CO	"	$\pm 5^\circ$ AZ	L0067	234
	"	"	CO	"	$\pm 5^\circ$ EL	L0069	235
	"	"	X	-	$\pm 45^\circ$ AZ	L0072	236
	"	"	X	-	$\pm 5^\circ$ AZ	L0071	237
	"	"	X	-	$\pm 5^\circ$ EL	L0070	238
	14 dB	0.0"	CO	35.05	$\pm 45^\circ$ AZ	L0063	239
	"	"	CO	"	$\pm 5^\circ$ AZ	L0061	240
	"	"	CO	"	$\pm 5^\circ$ EL	L0062	241
	"	"	X	-	$\pm 45^\circ$ AZ	L0066	242
	"	"	X	-	$\pm 5^\circ$ AZ	L0065	243
	"	"	X	-	$\pm 5^\circ$ EL	L0064	244



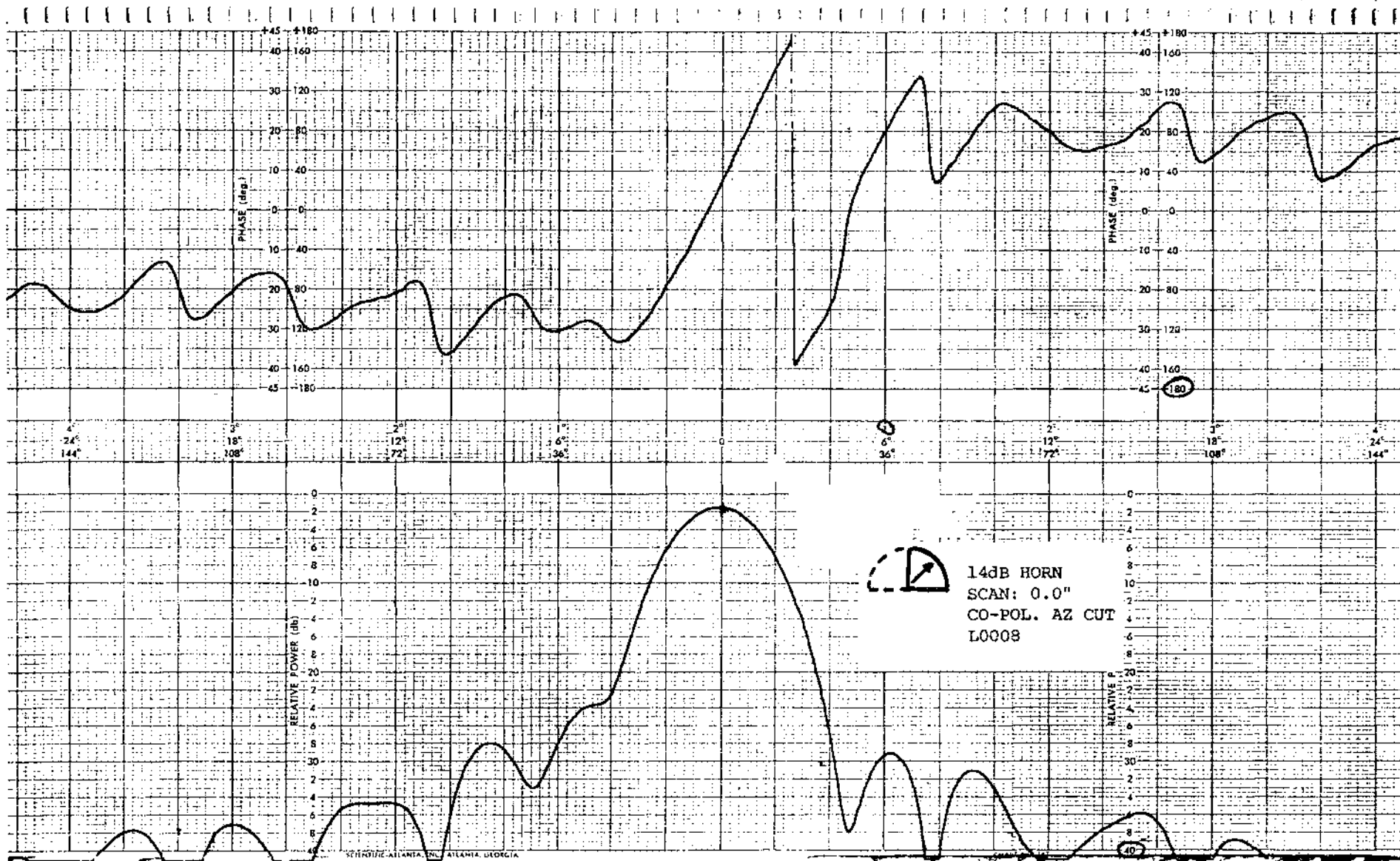
144 120 96 72 48 24 0 24 48 72 96 120 144  
 180 160 140 120 100 80 60 40 20 0 -20 -40 -60 -80 -100 -120 -140 -160 -180

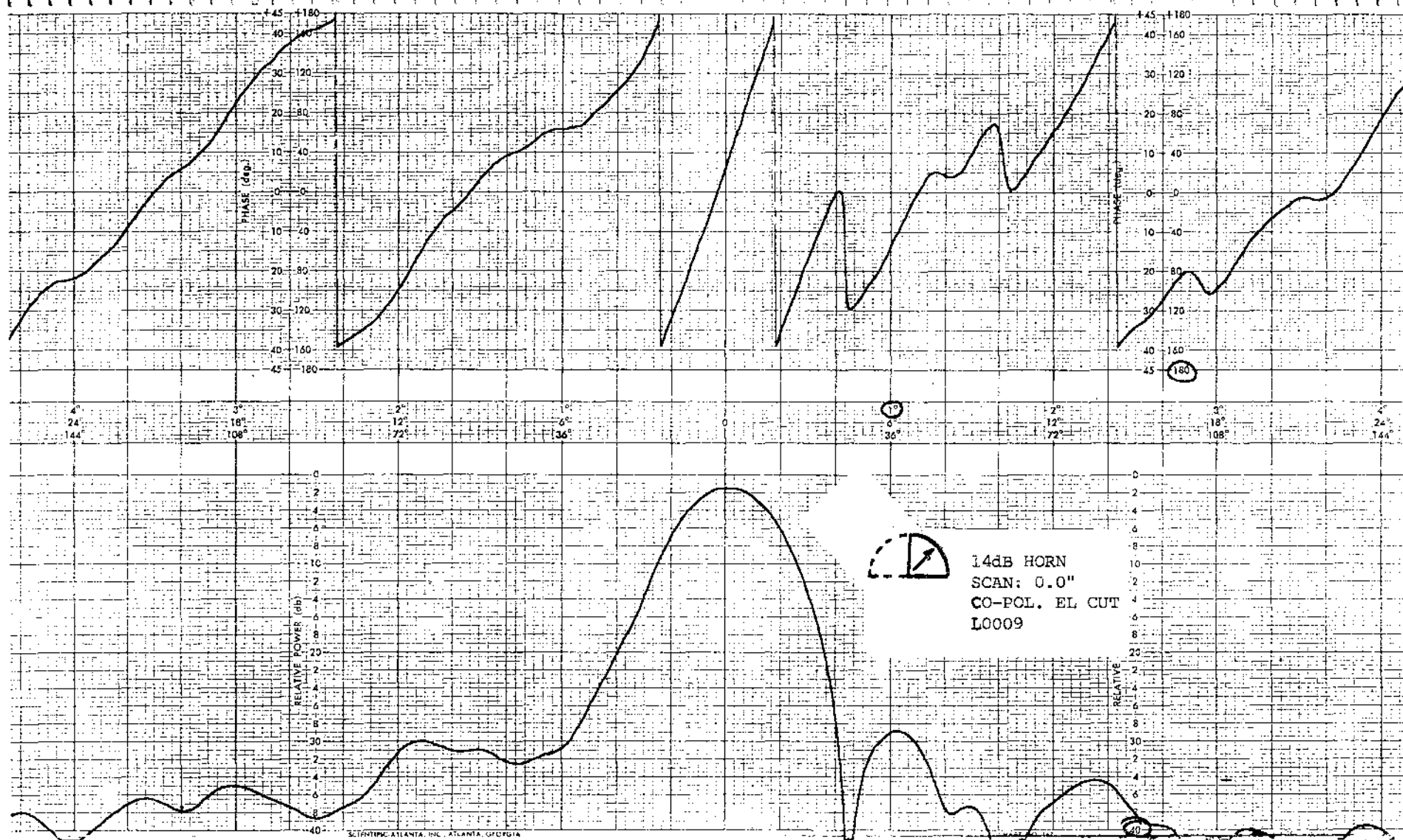


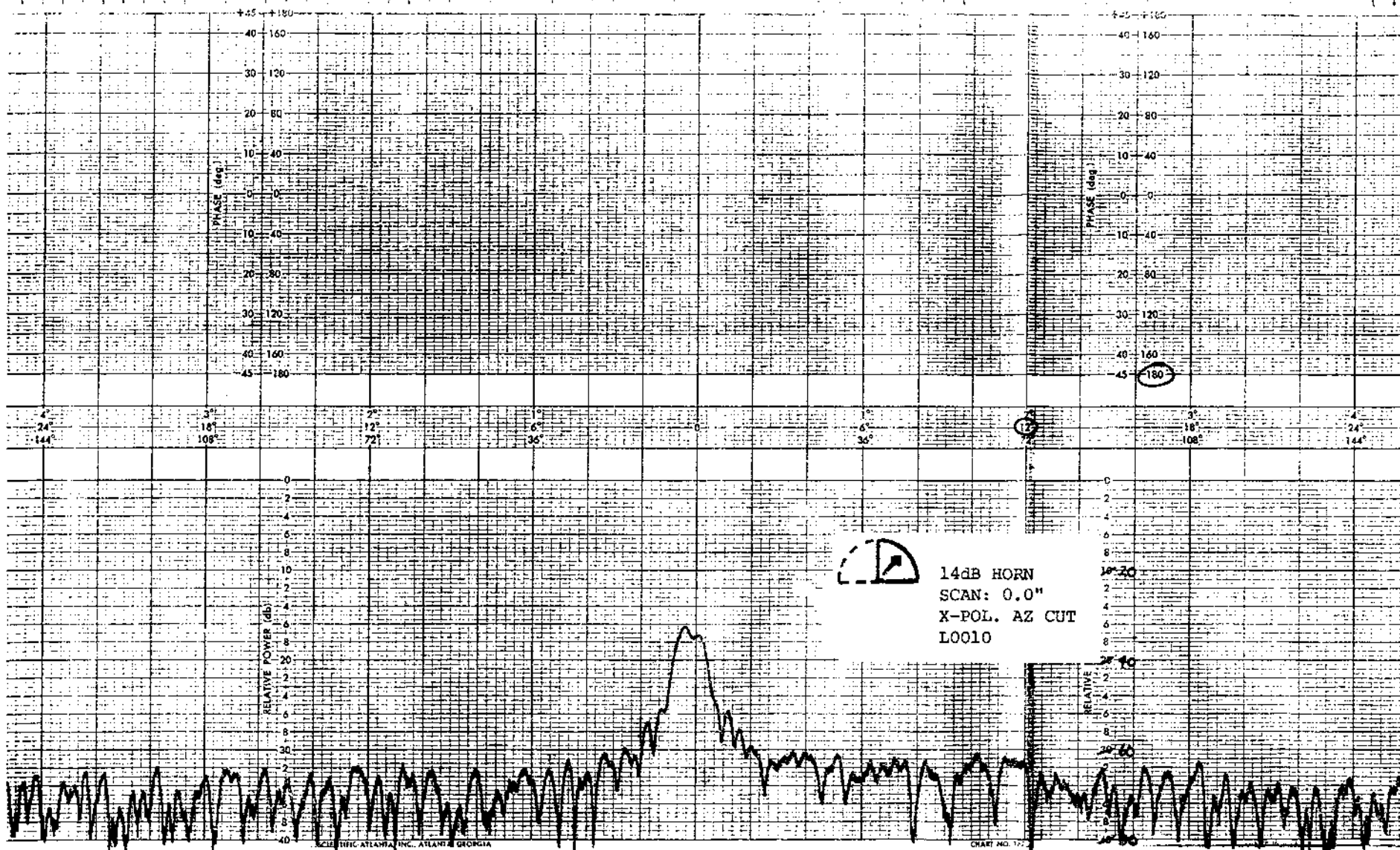
14dB HORN  
 SCAN: 0.0"  
 CO-POL. AZ CUT  
 L0007

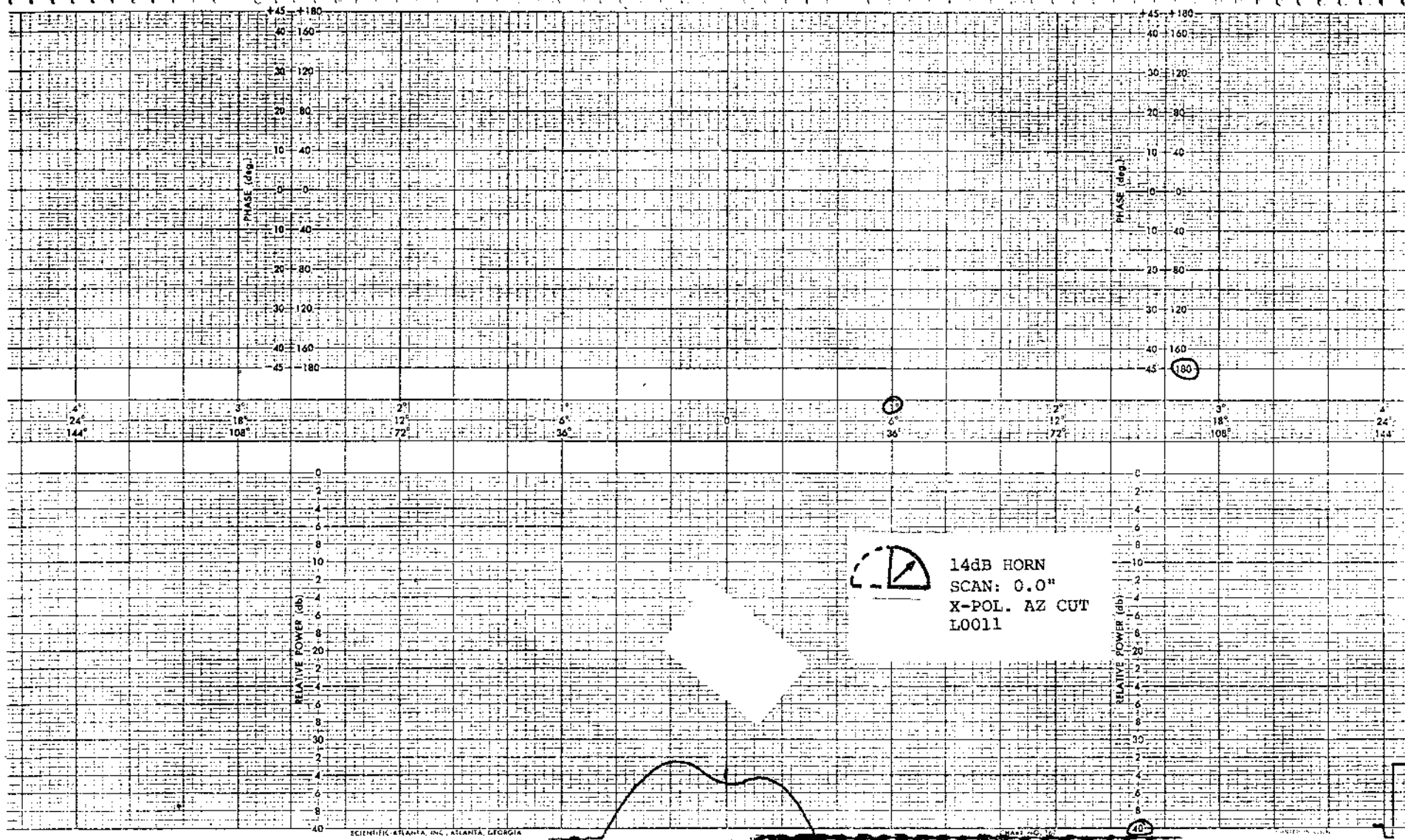
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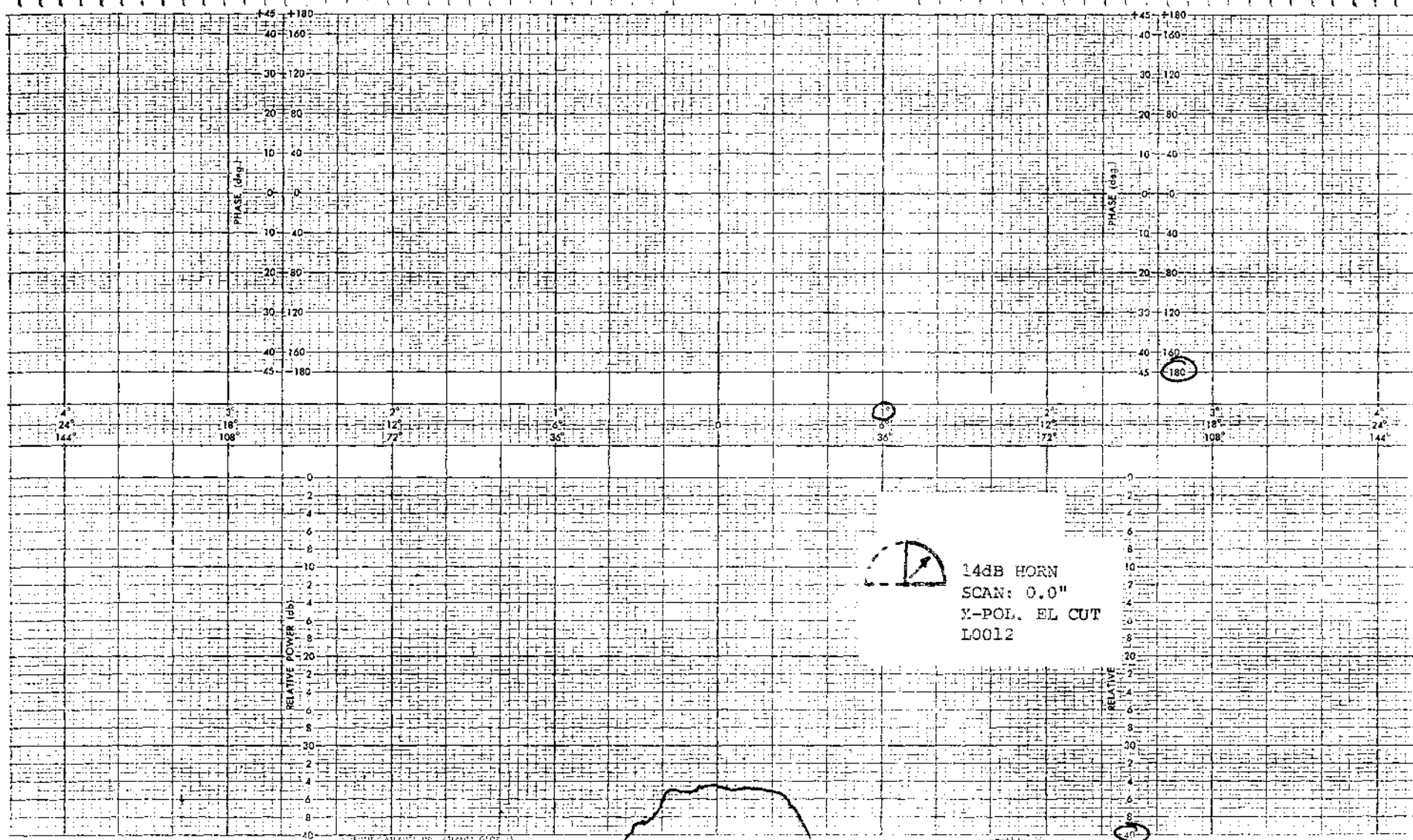
CHART NO. 17



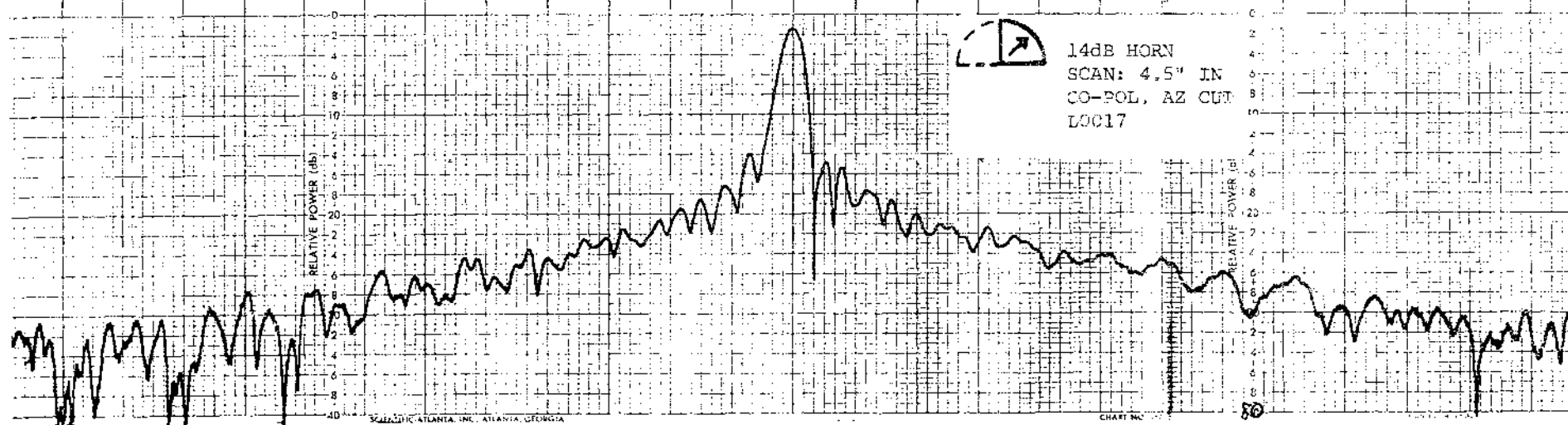
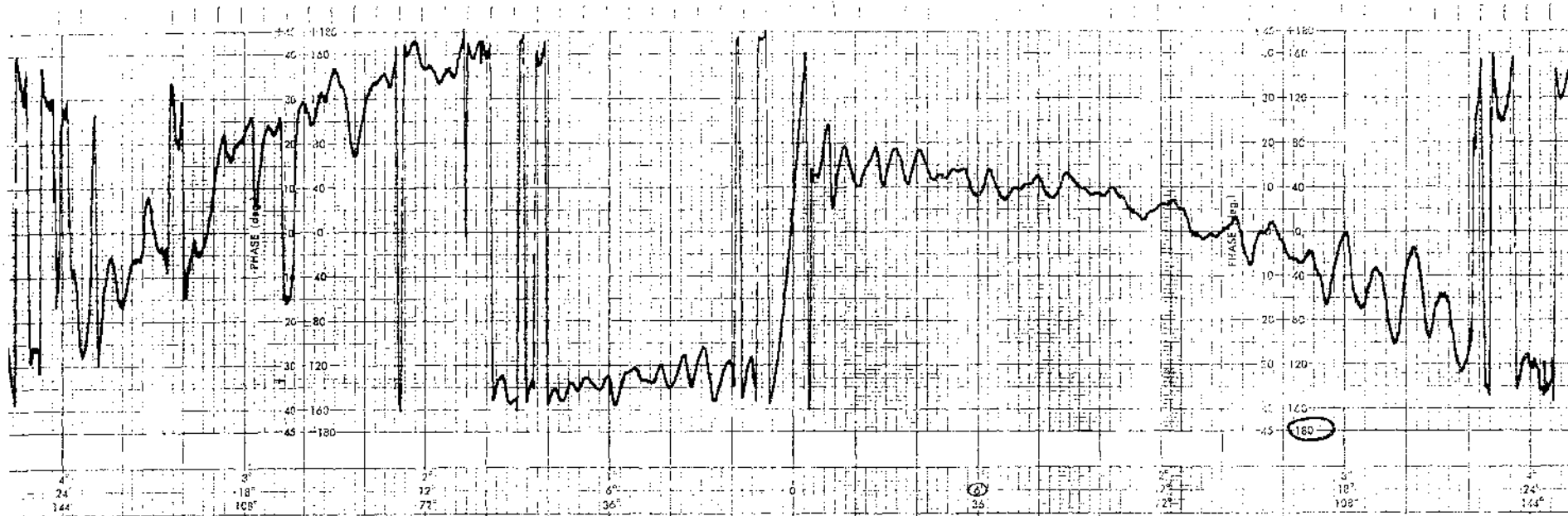




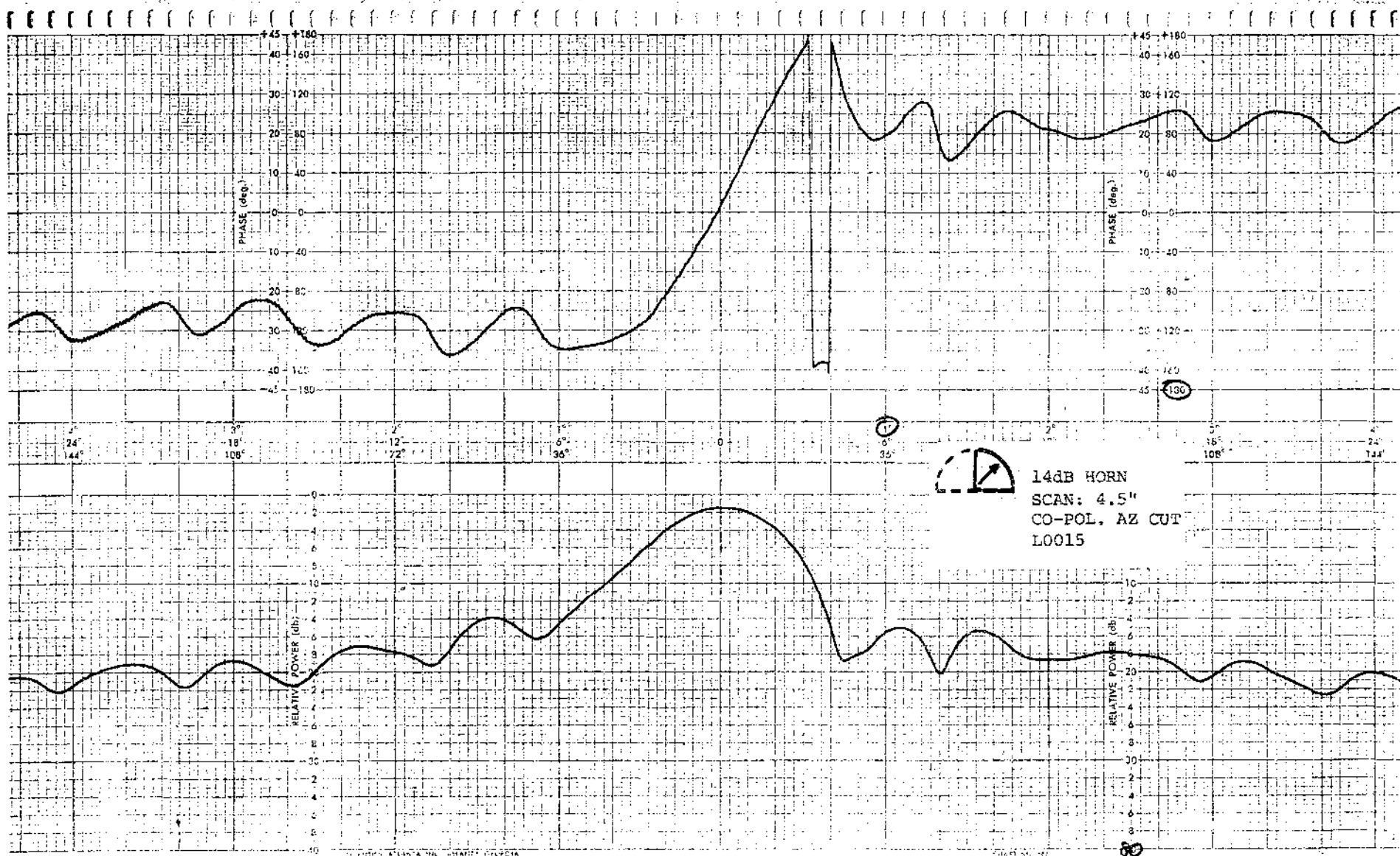


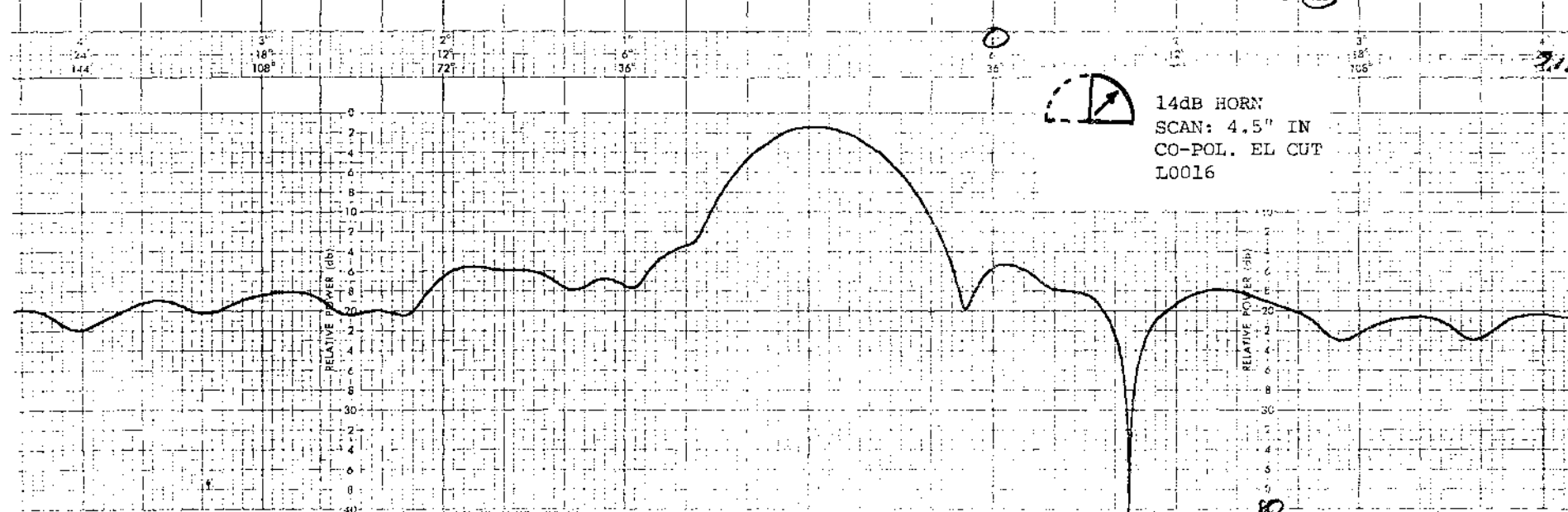
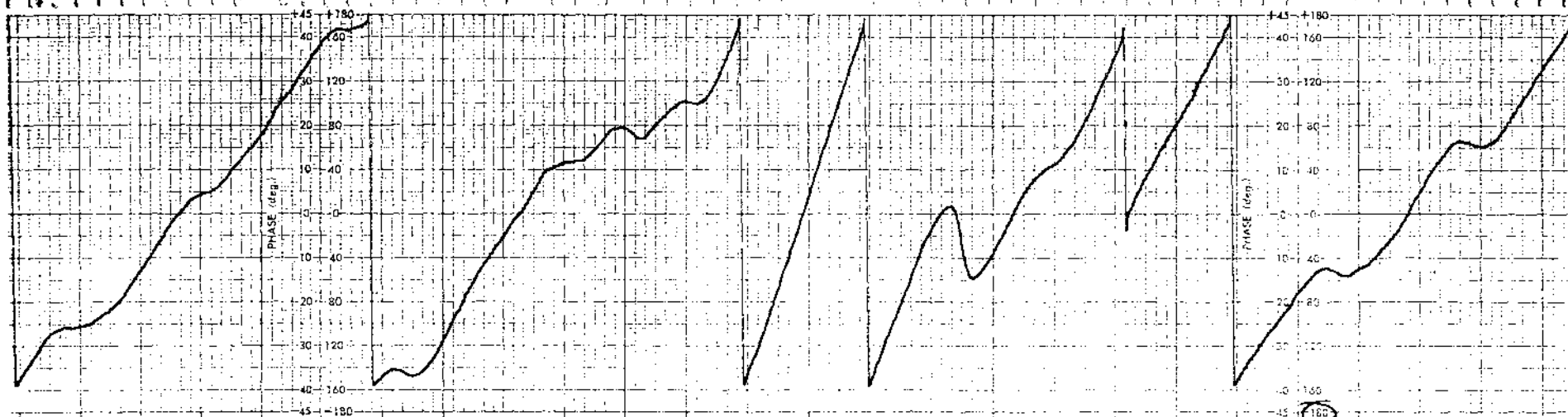




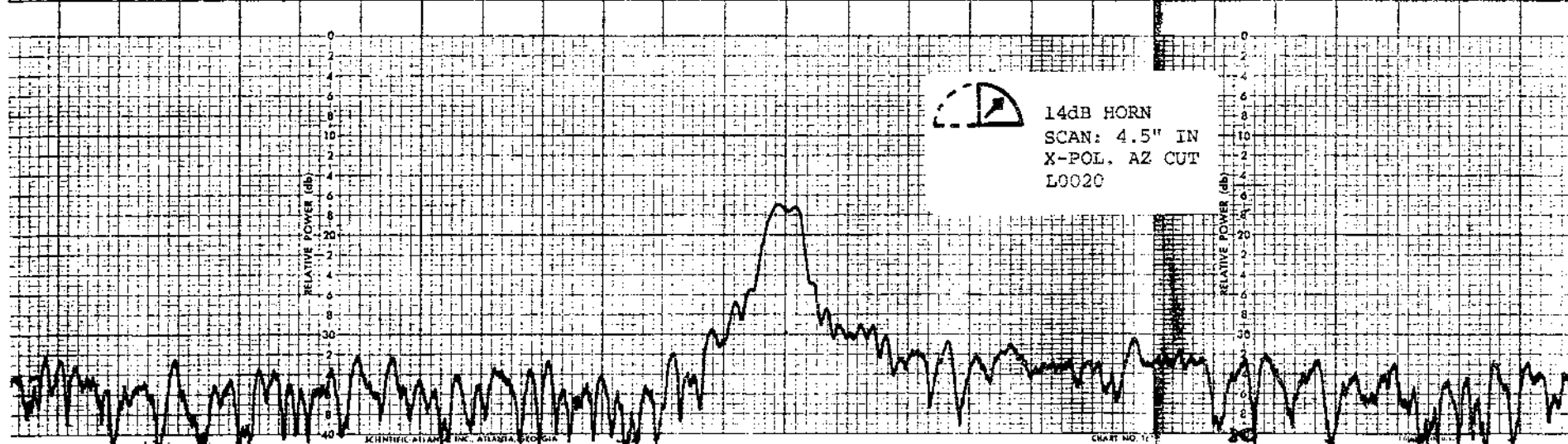
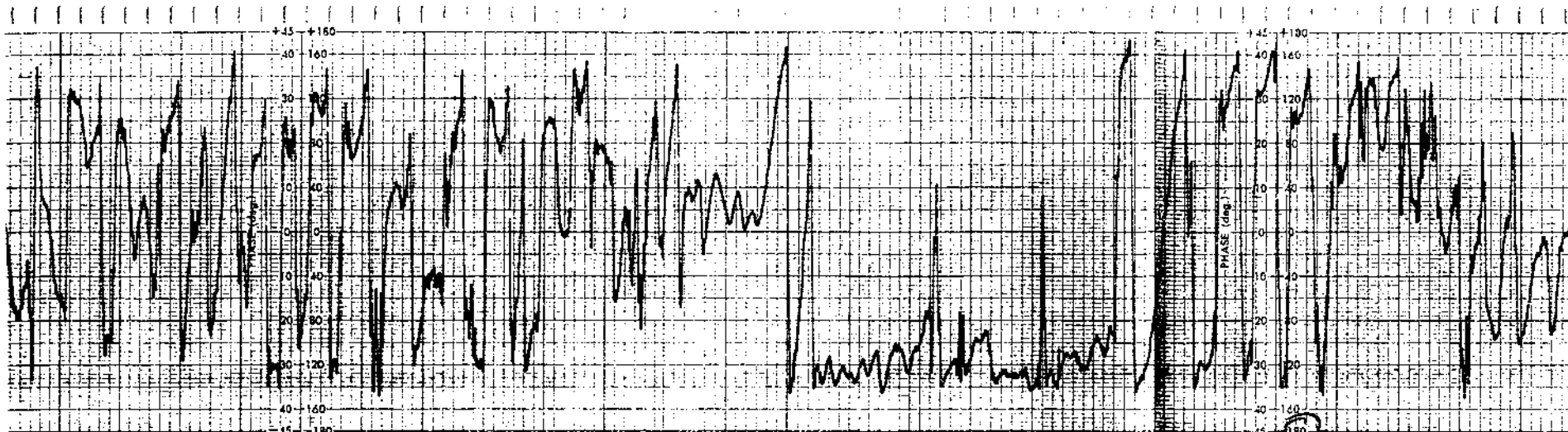






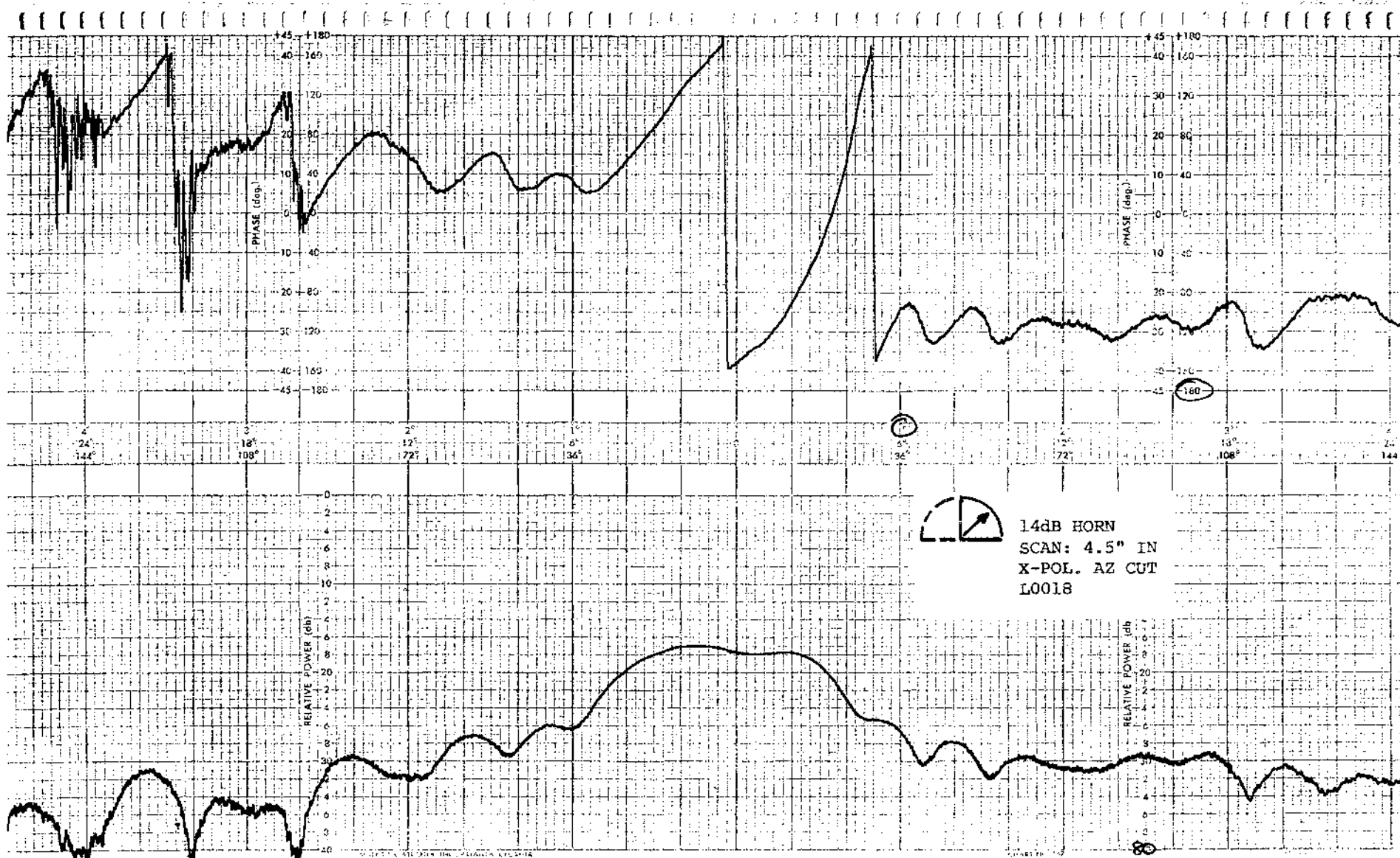


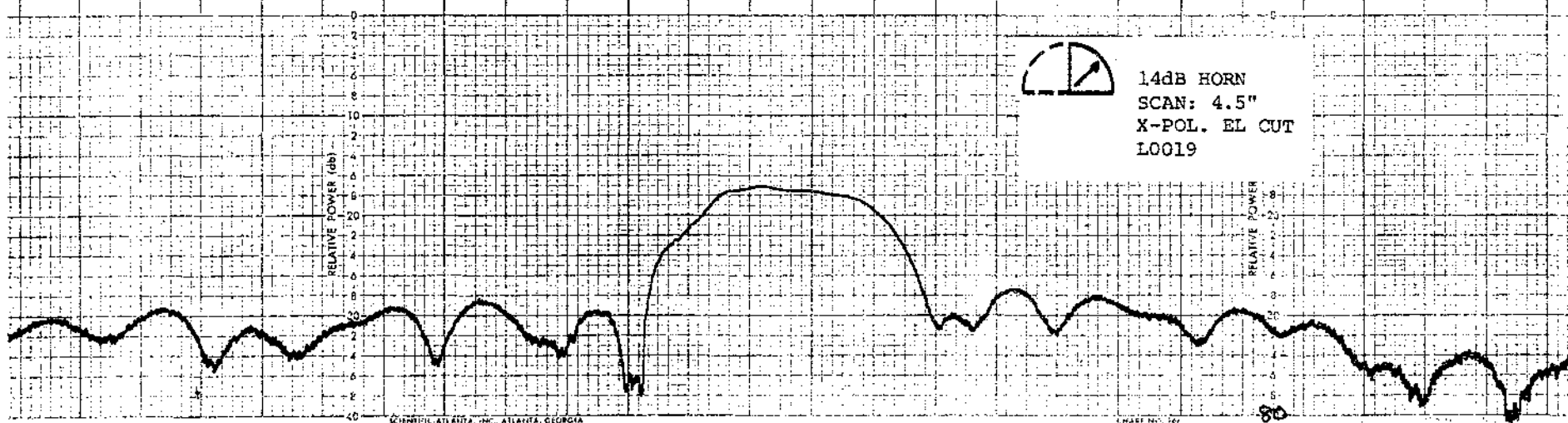
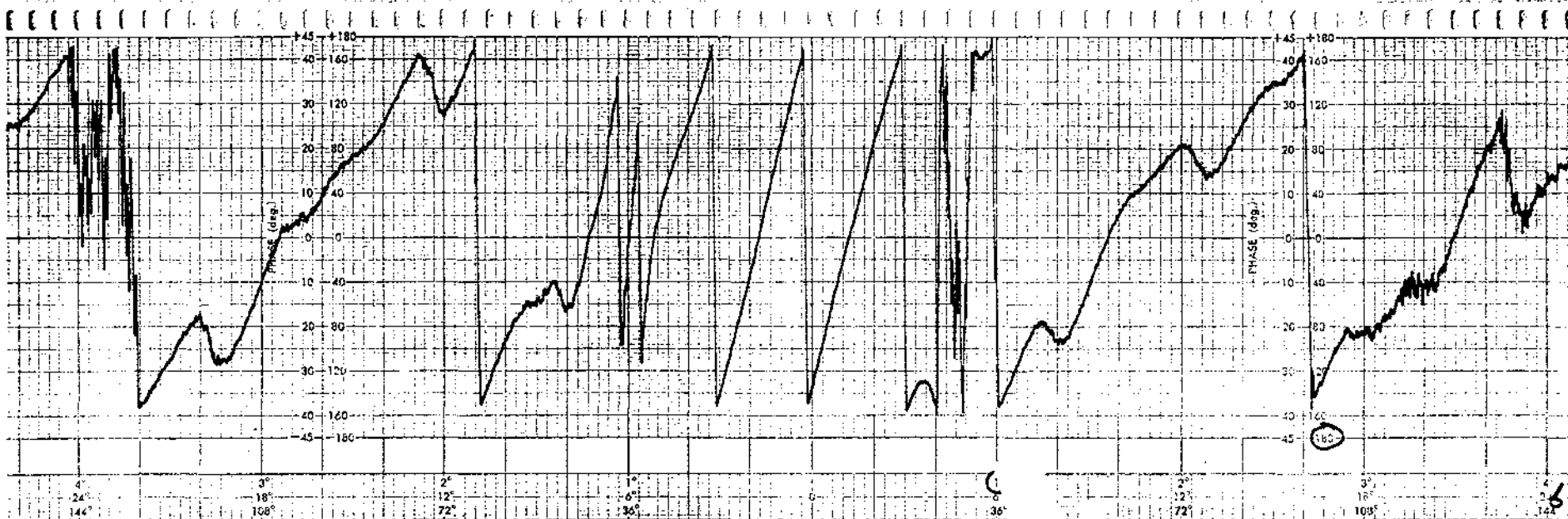
14dB HORN  
SCAN: 4.5" IN  
CO-POL. EL CUT  
L0016

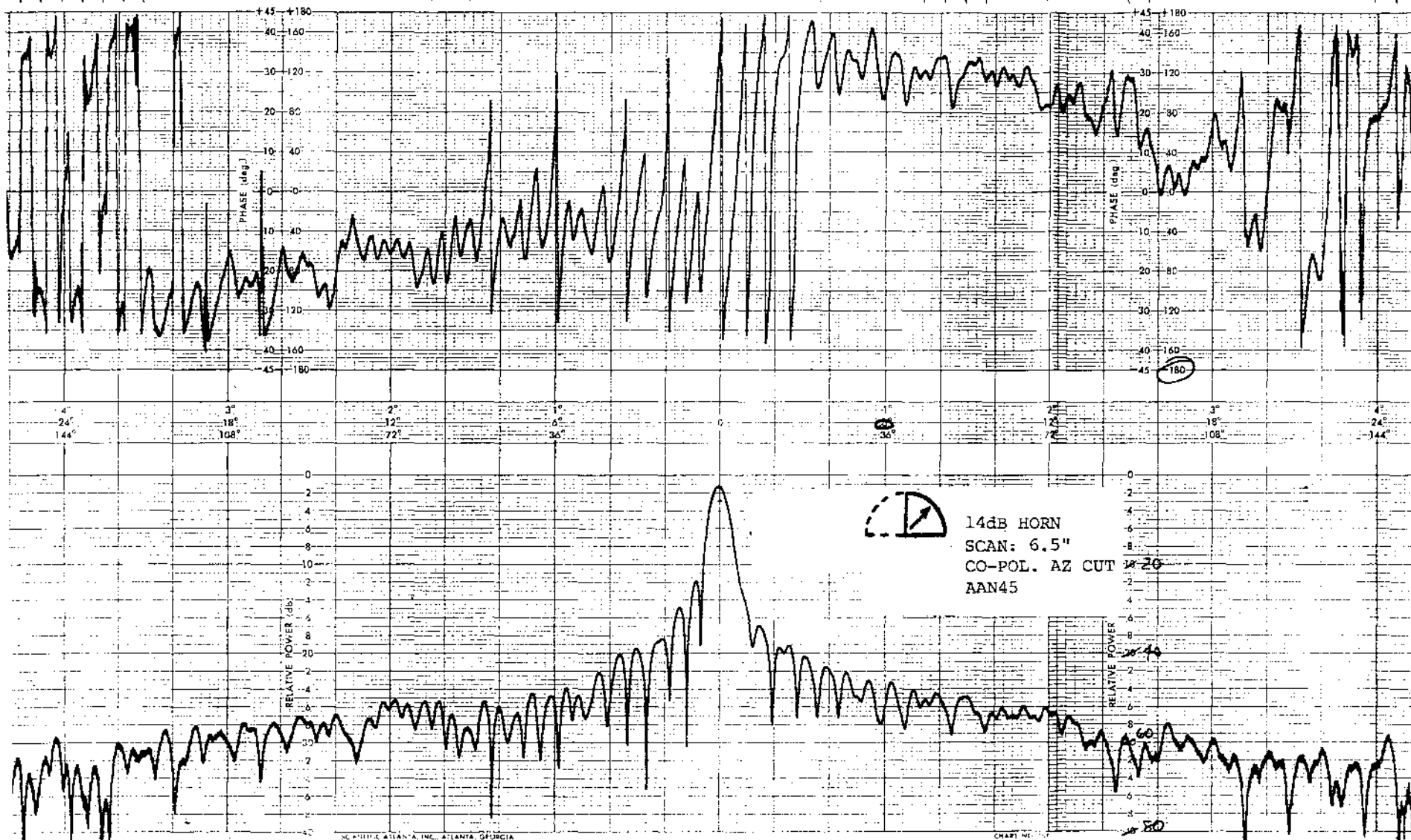


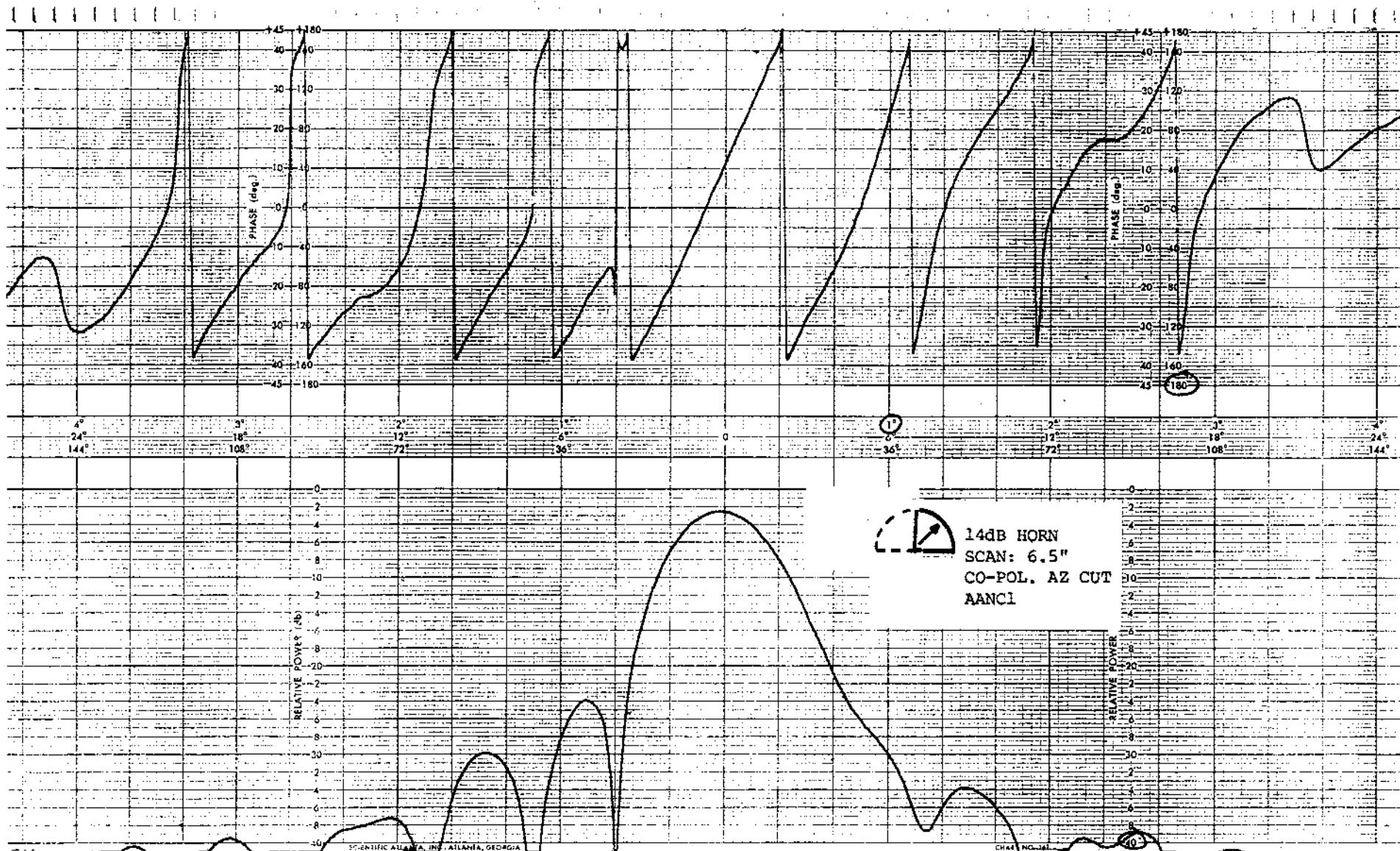
SCIENTIFIC ATTACHE, INC., ATLANTA, GEORGIA

CHART NO. 10

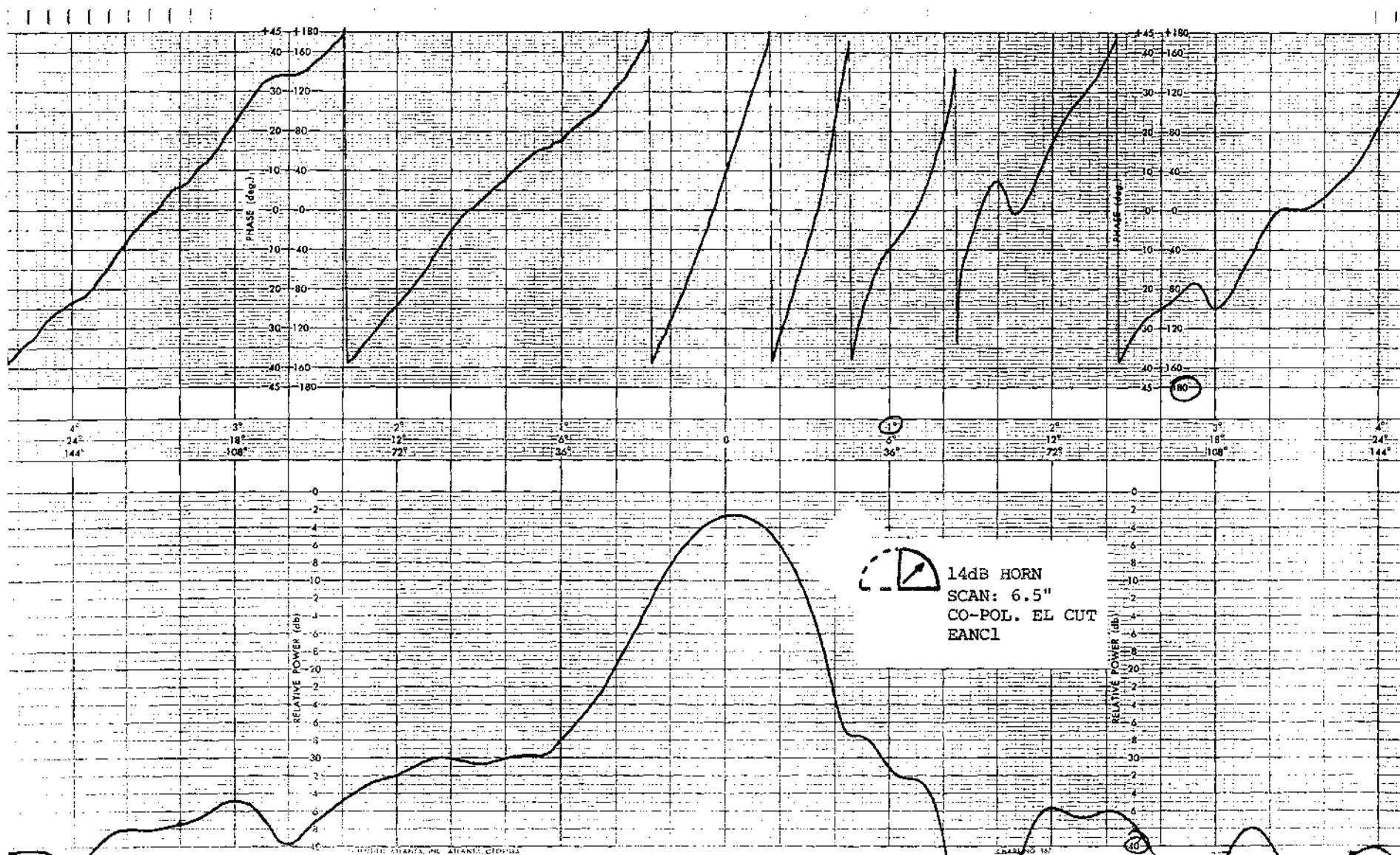




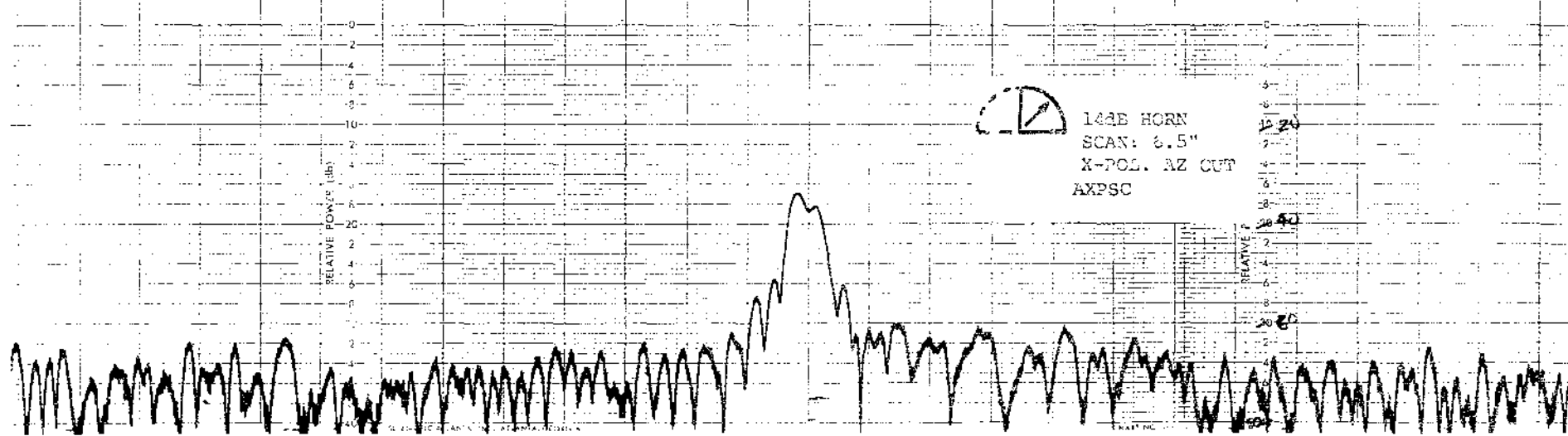
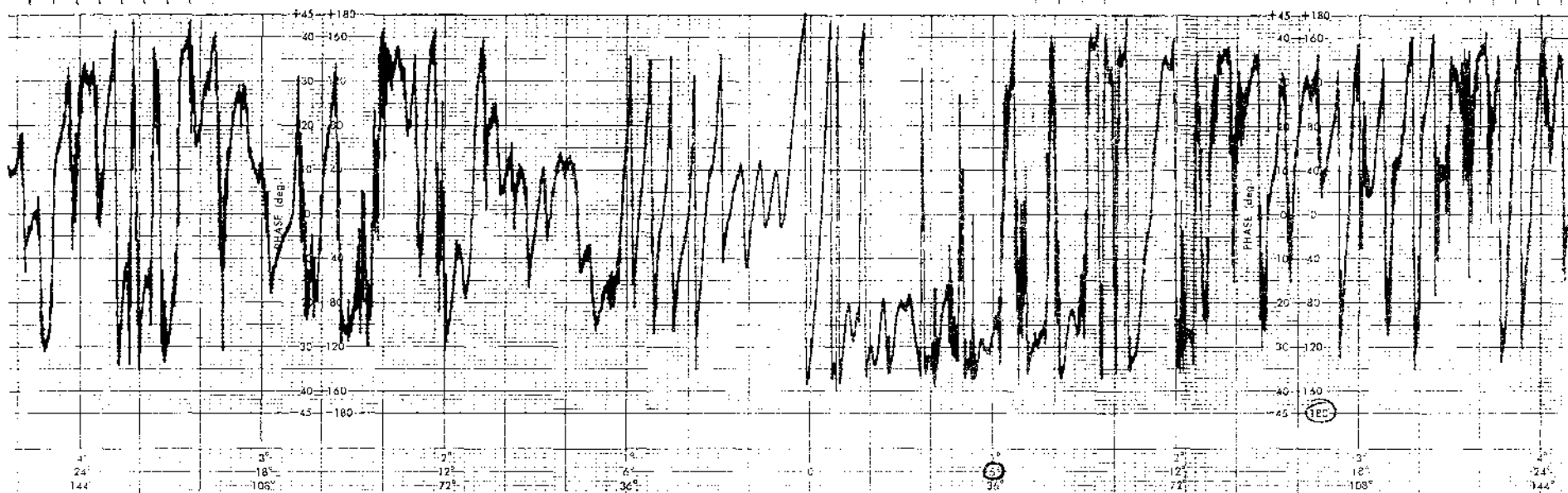


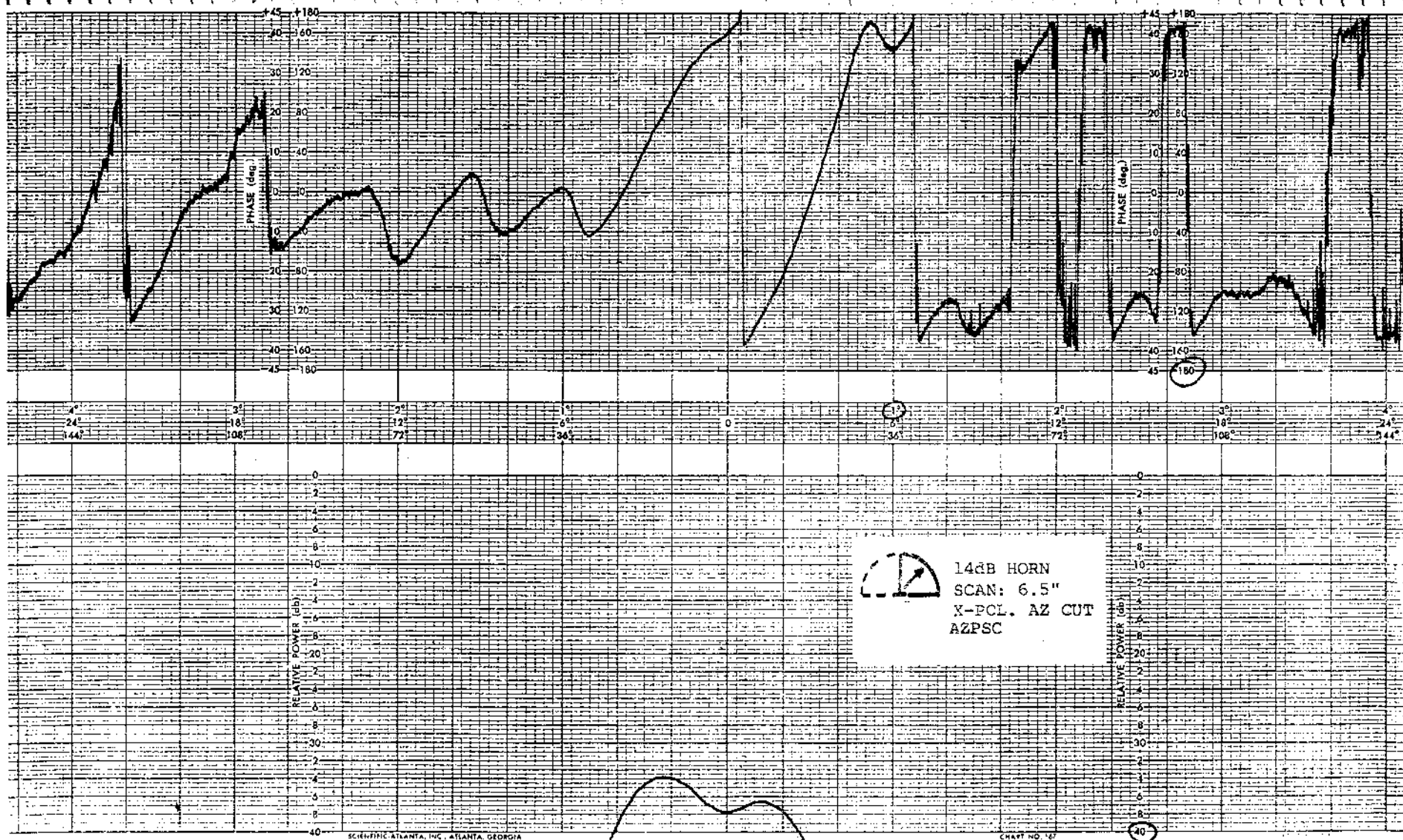




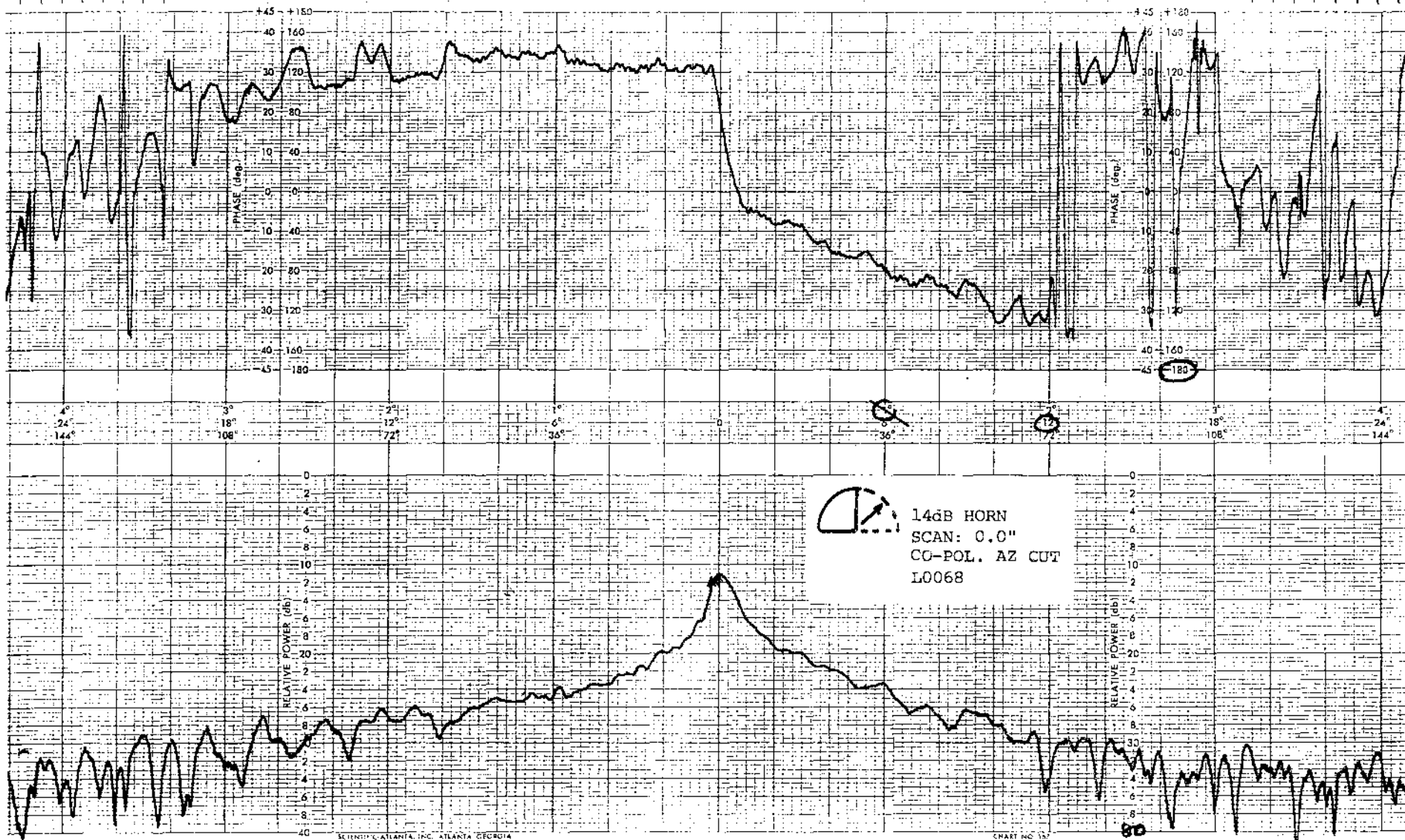


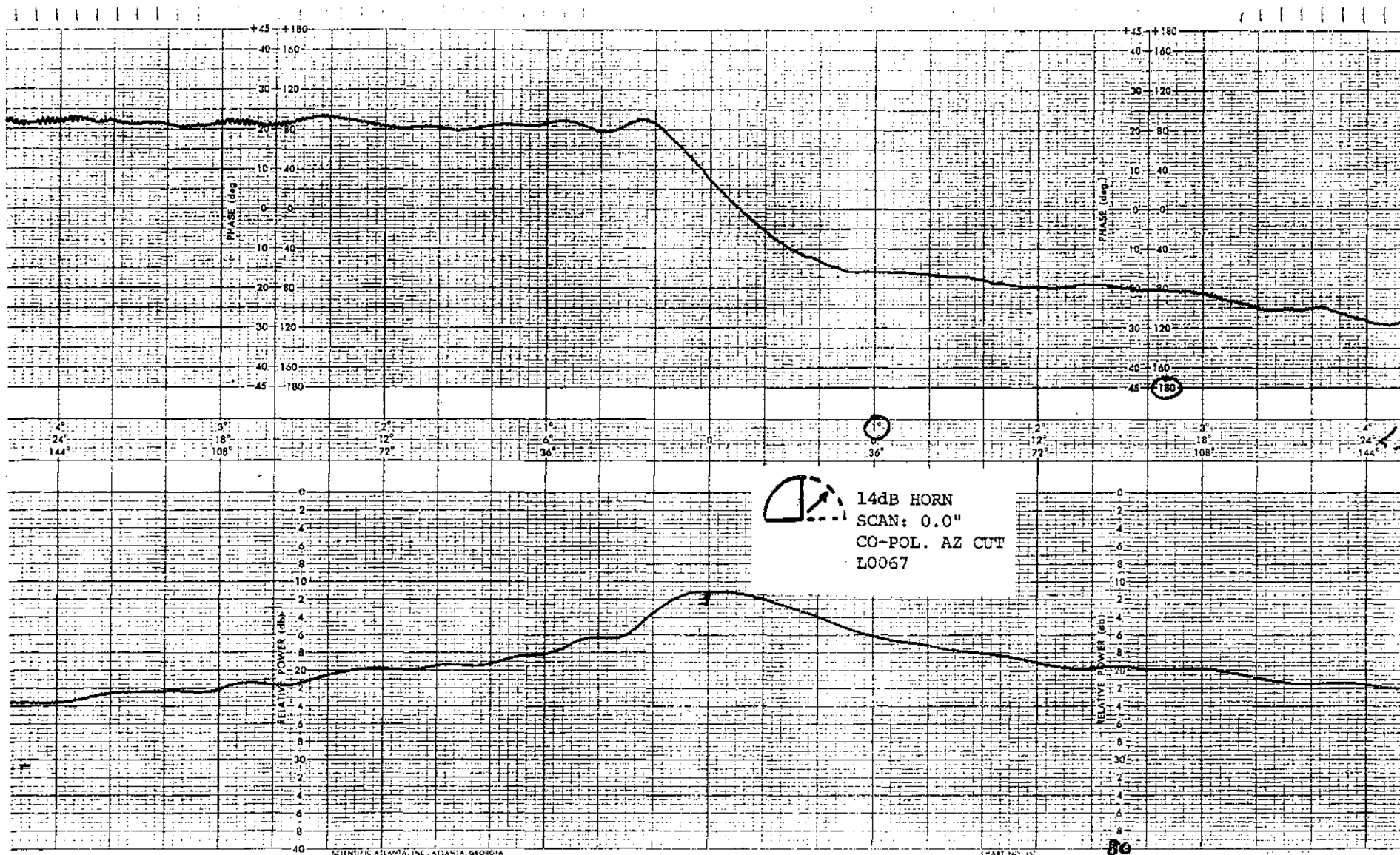


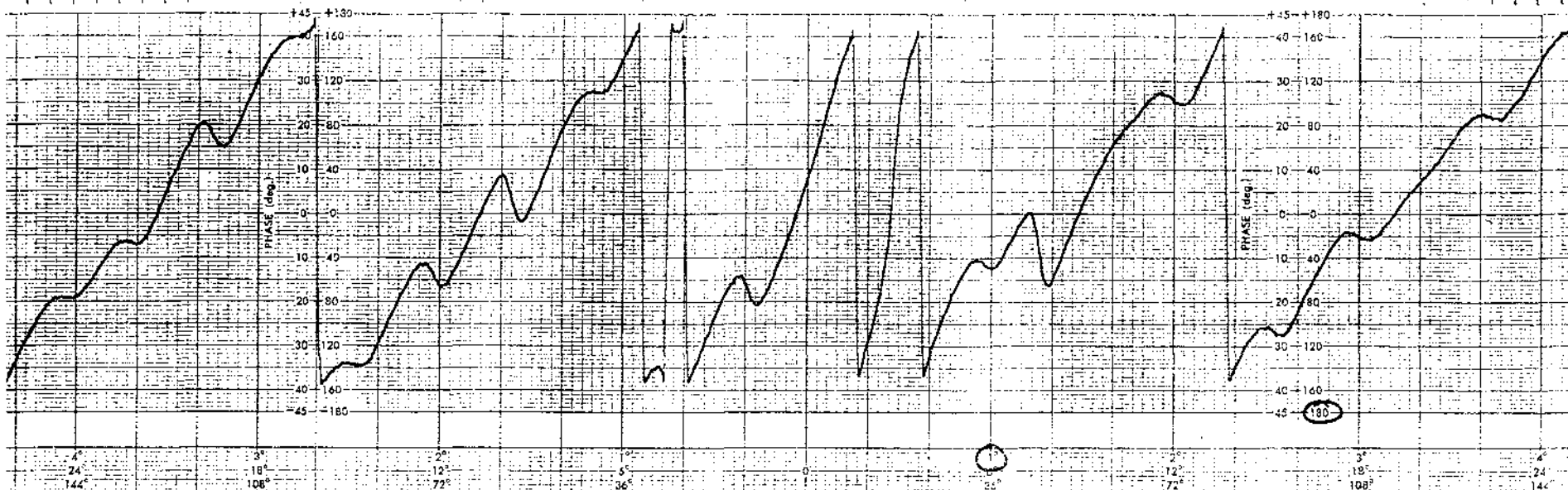




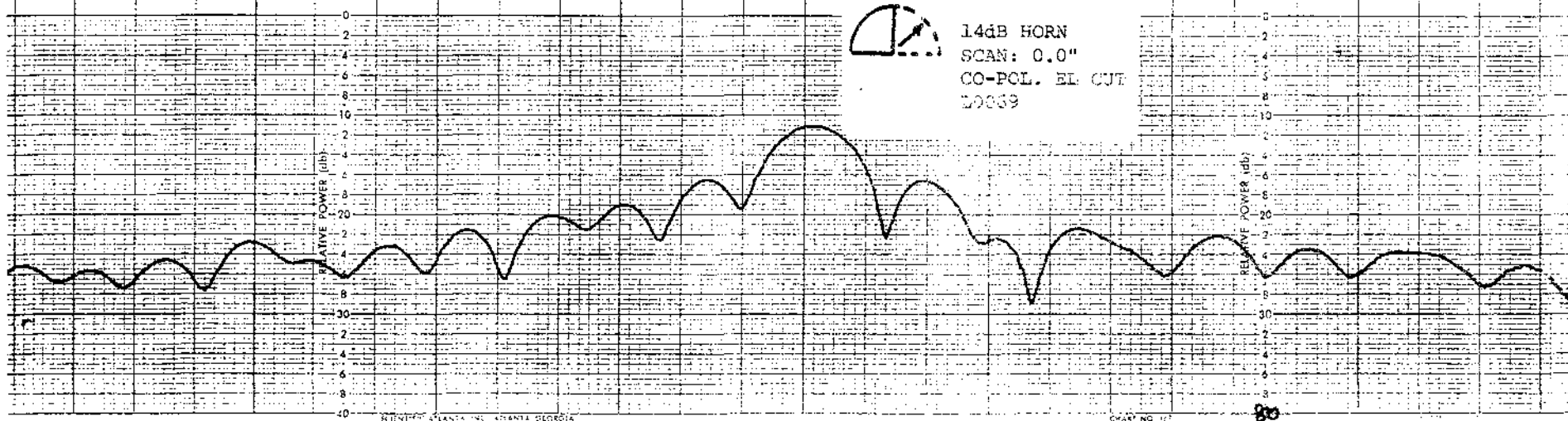




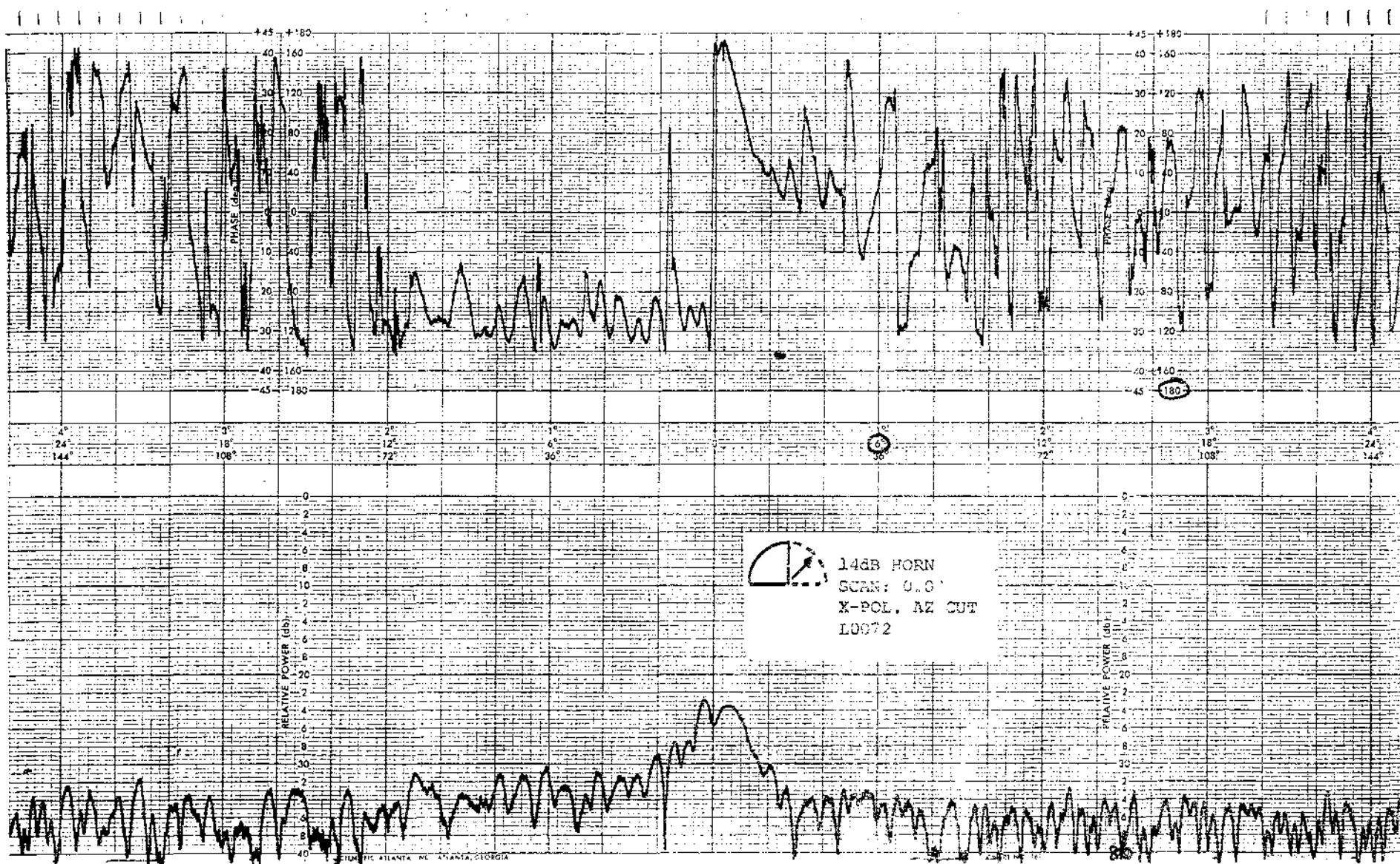


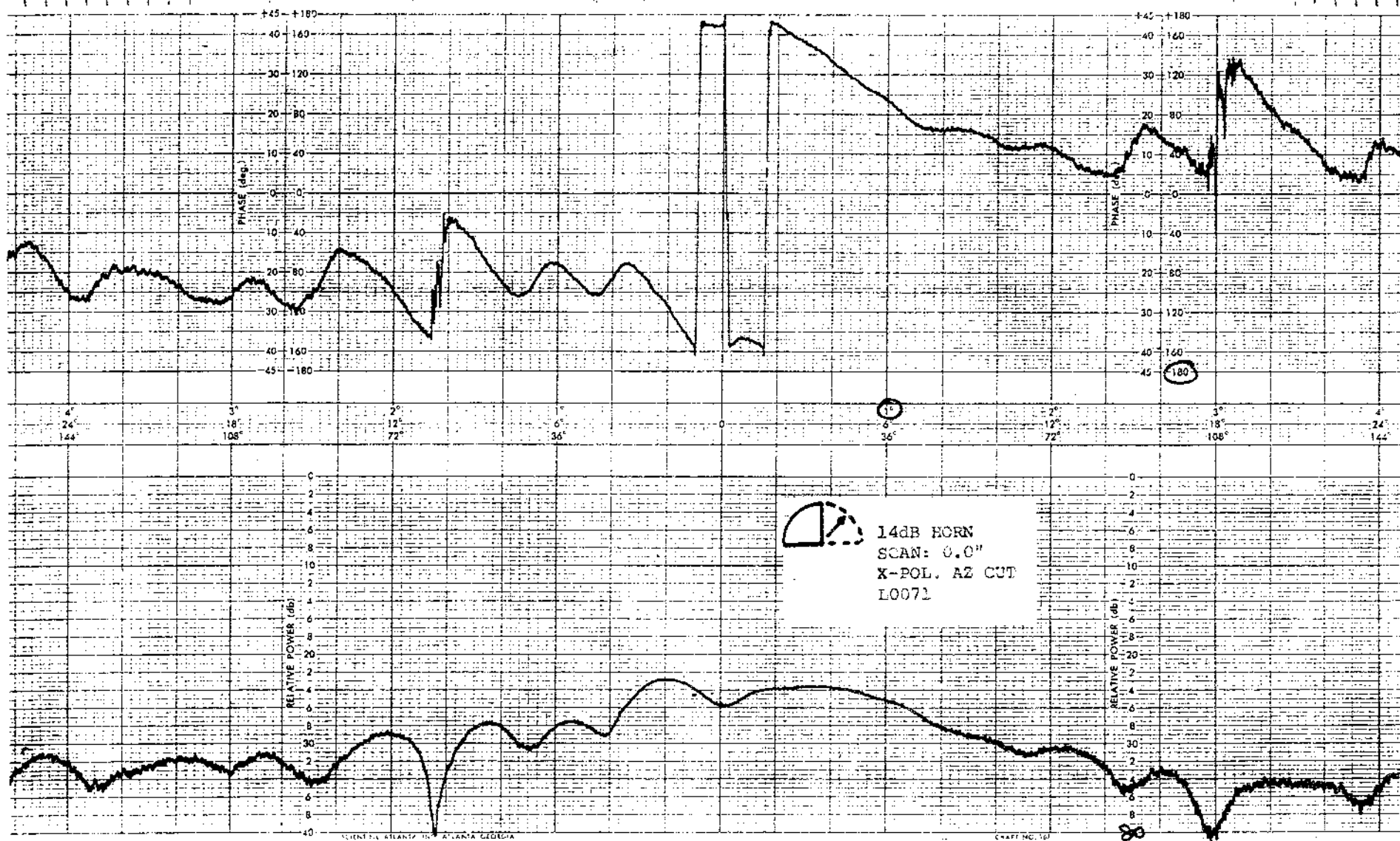


14dB HORN  
SCAN: 0.0"  
CO-POL. EL CUT  
20839

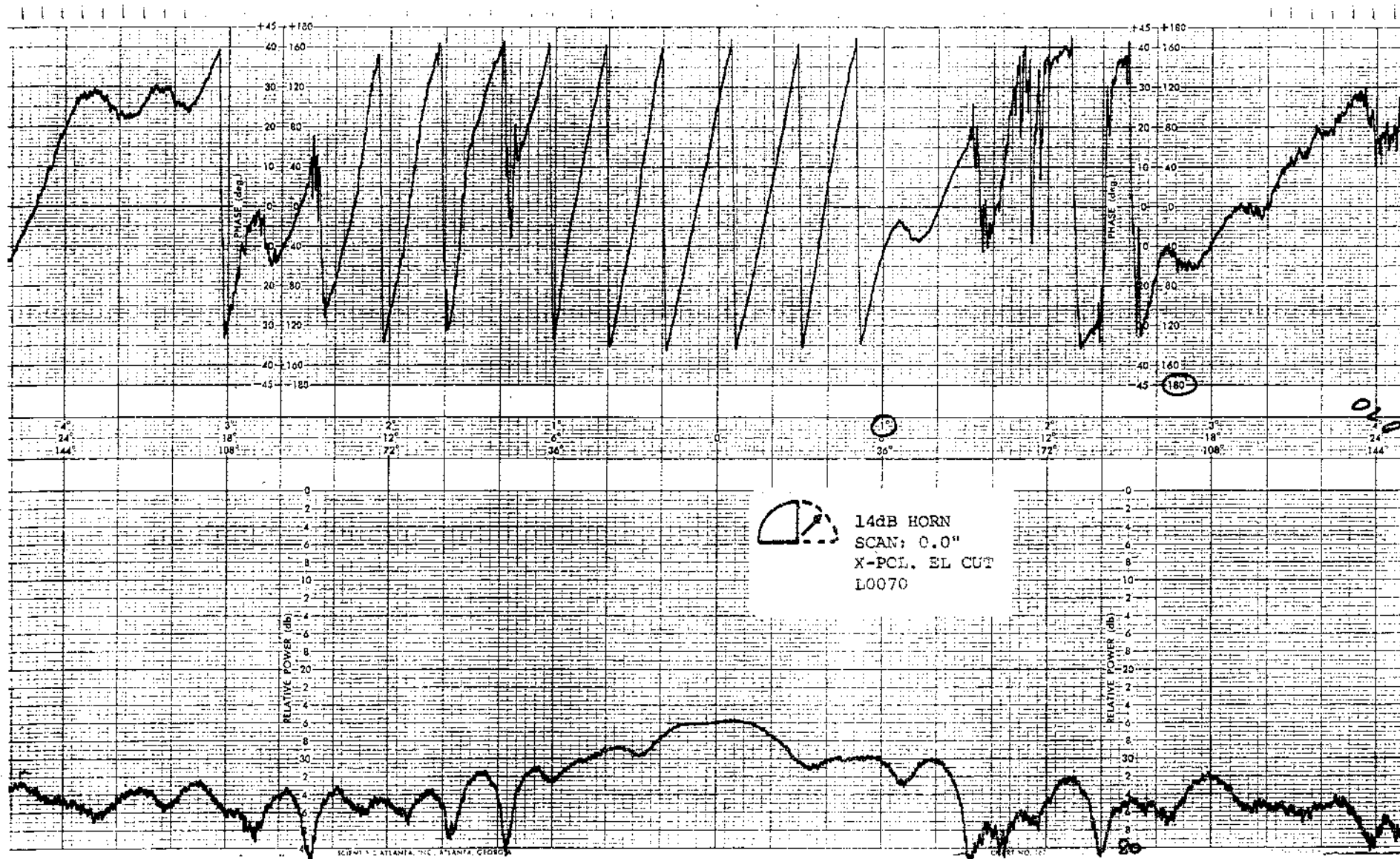


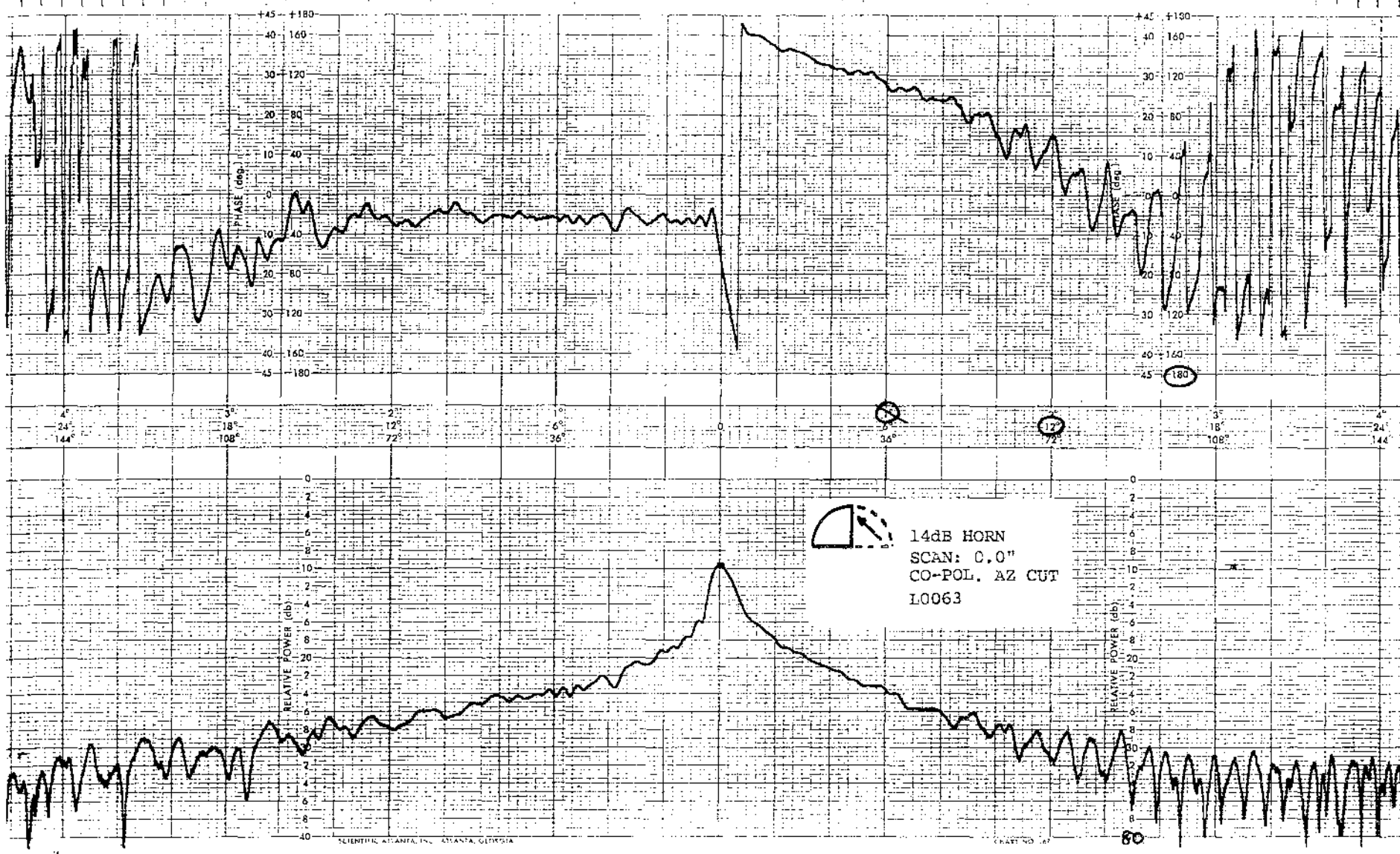


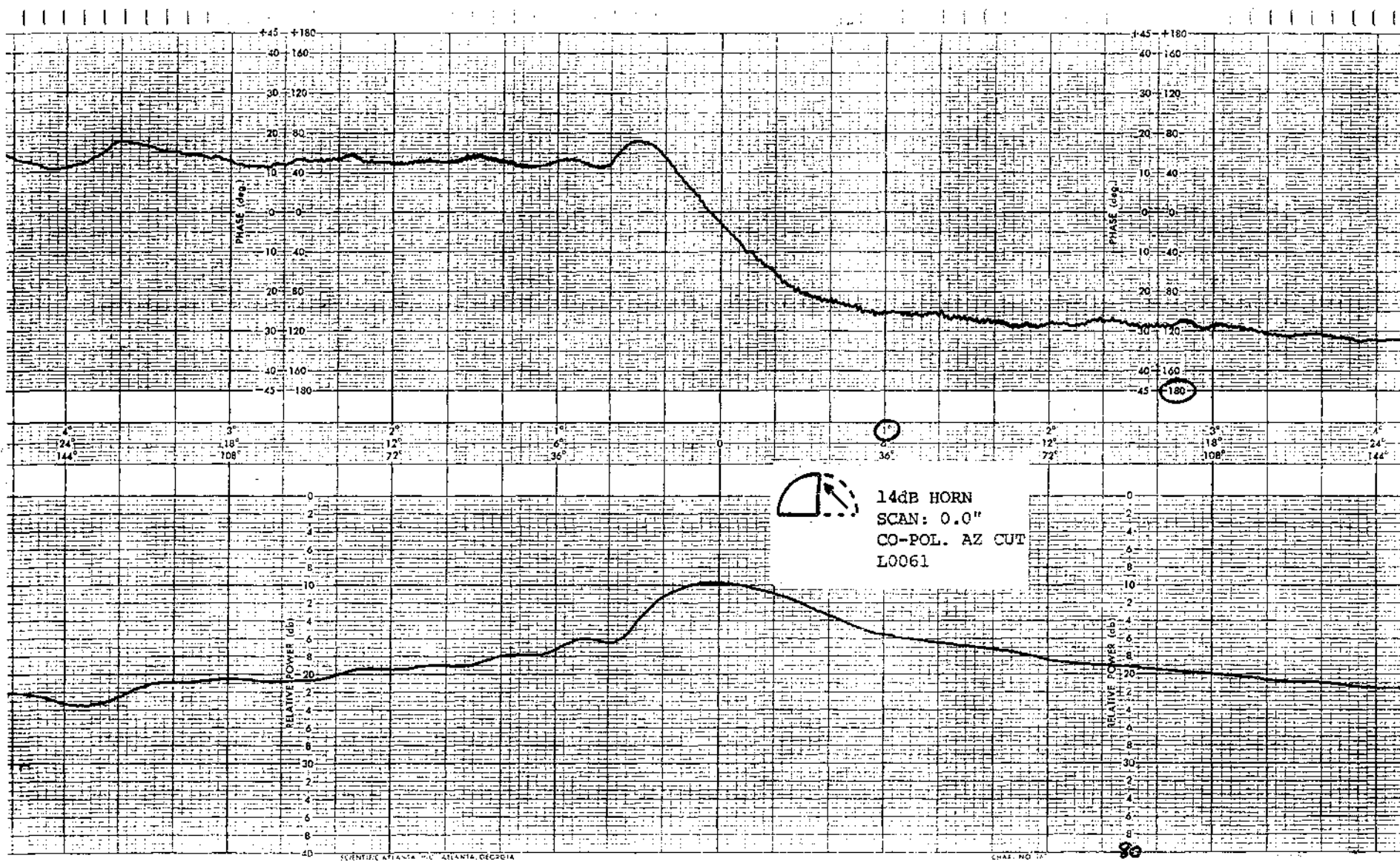


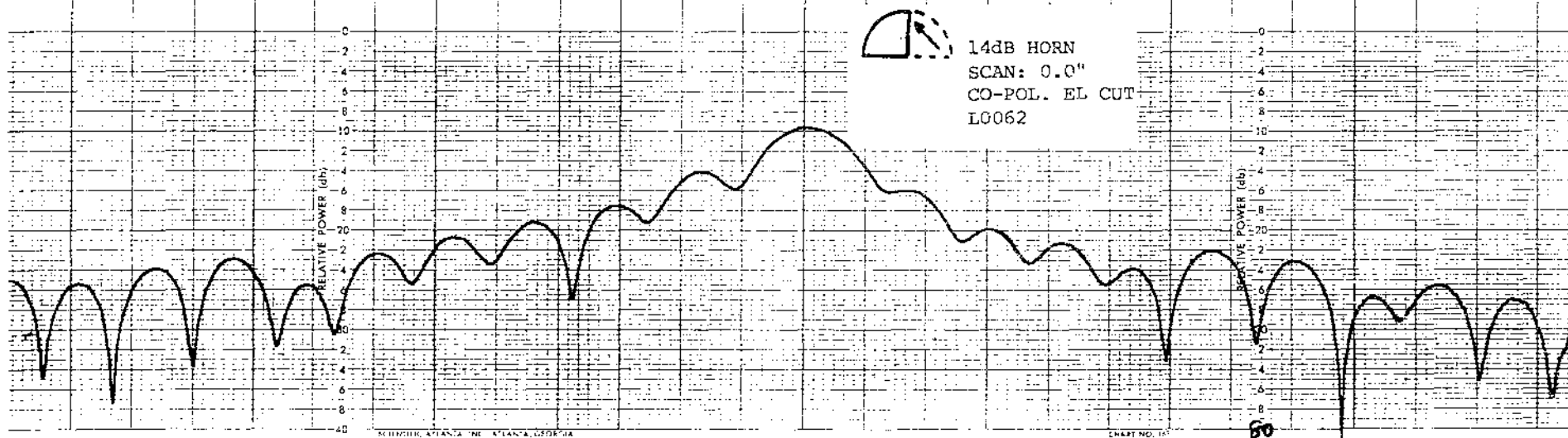
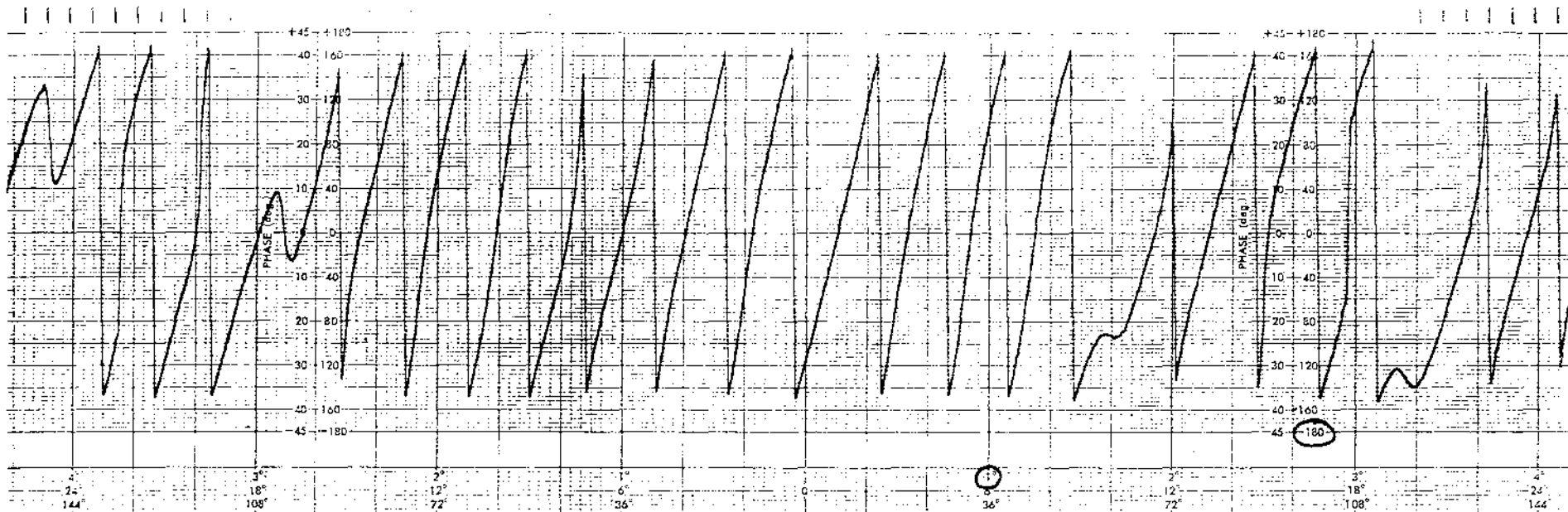


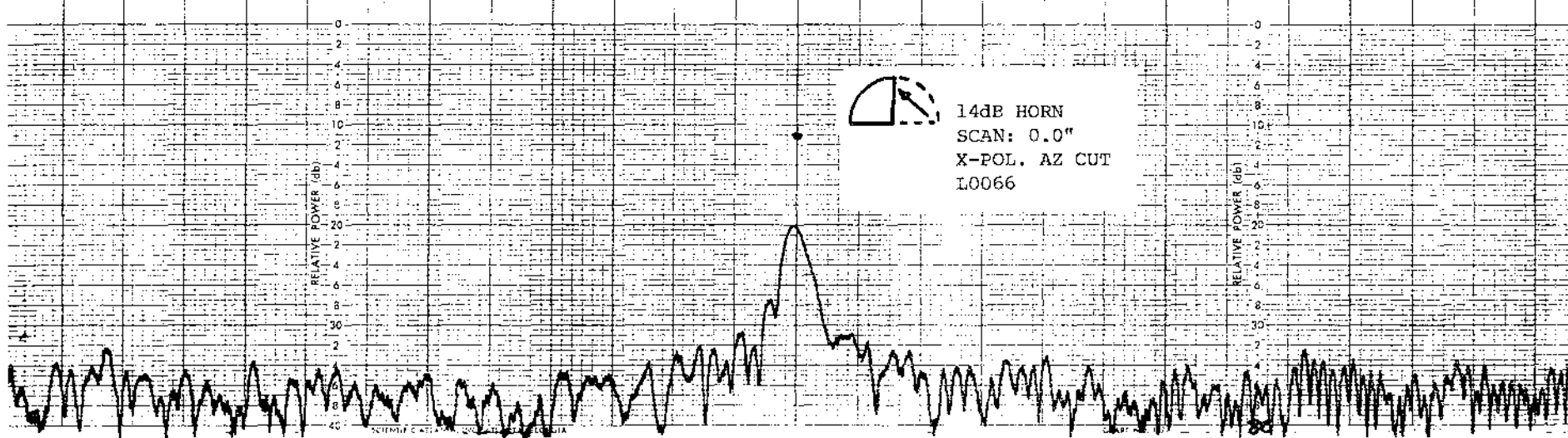
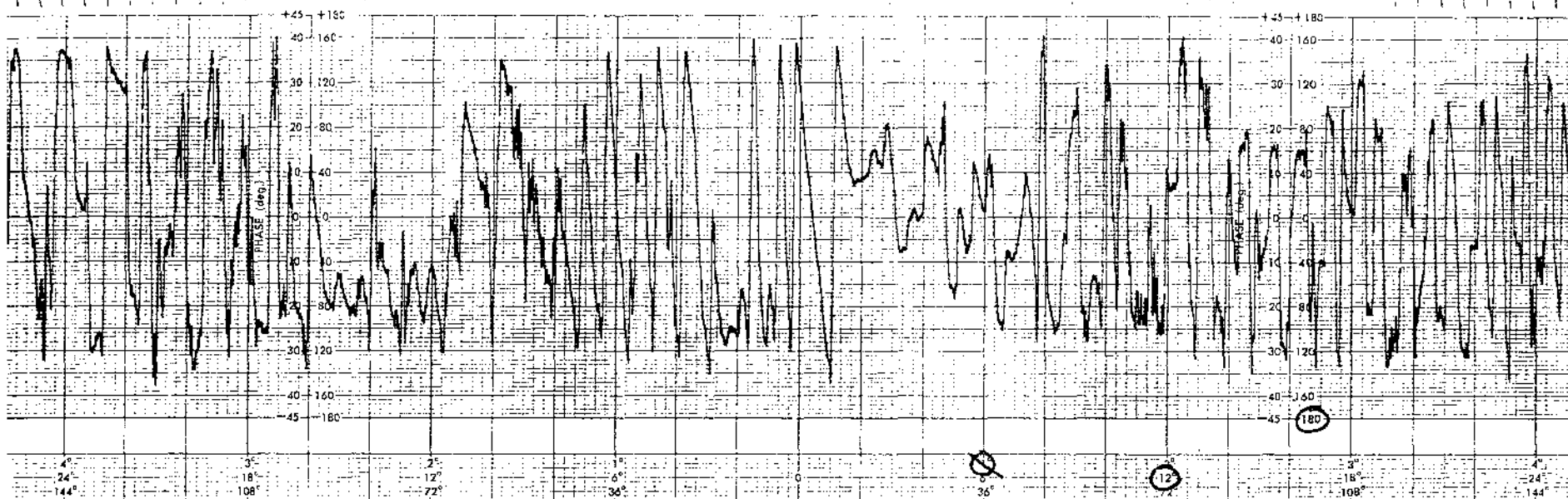


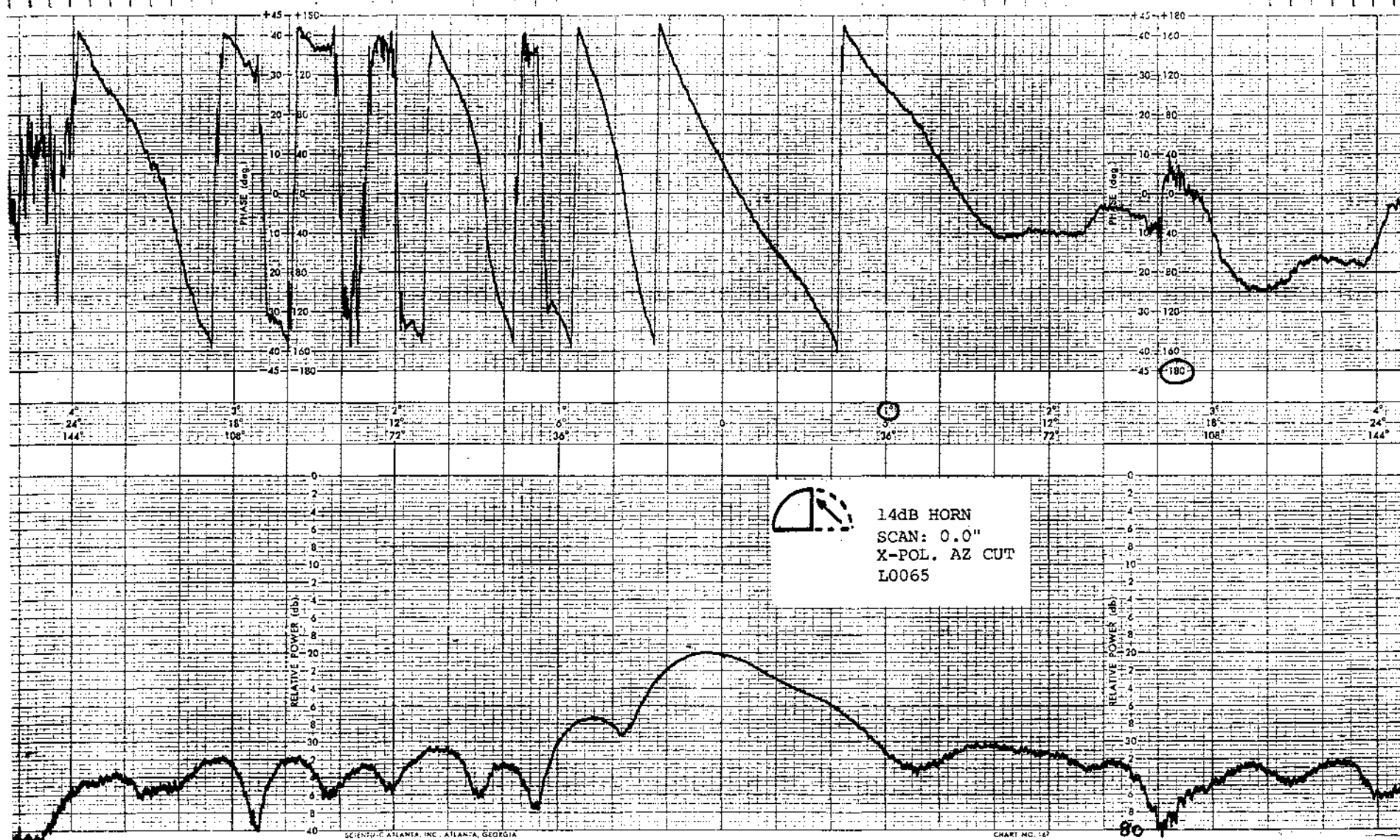




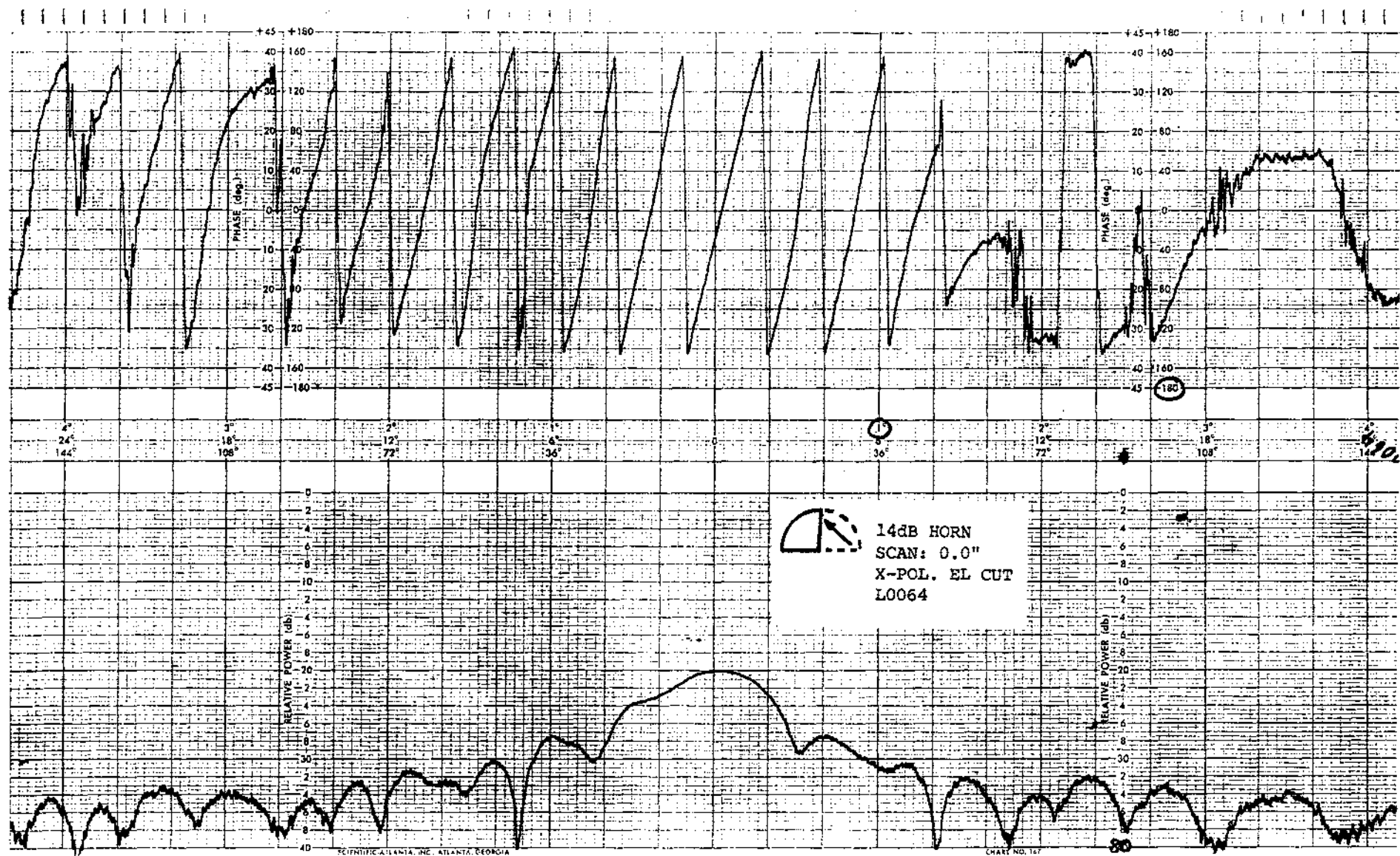







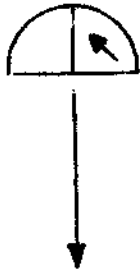




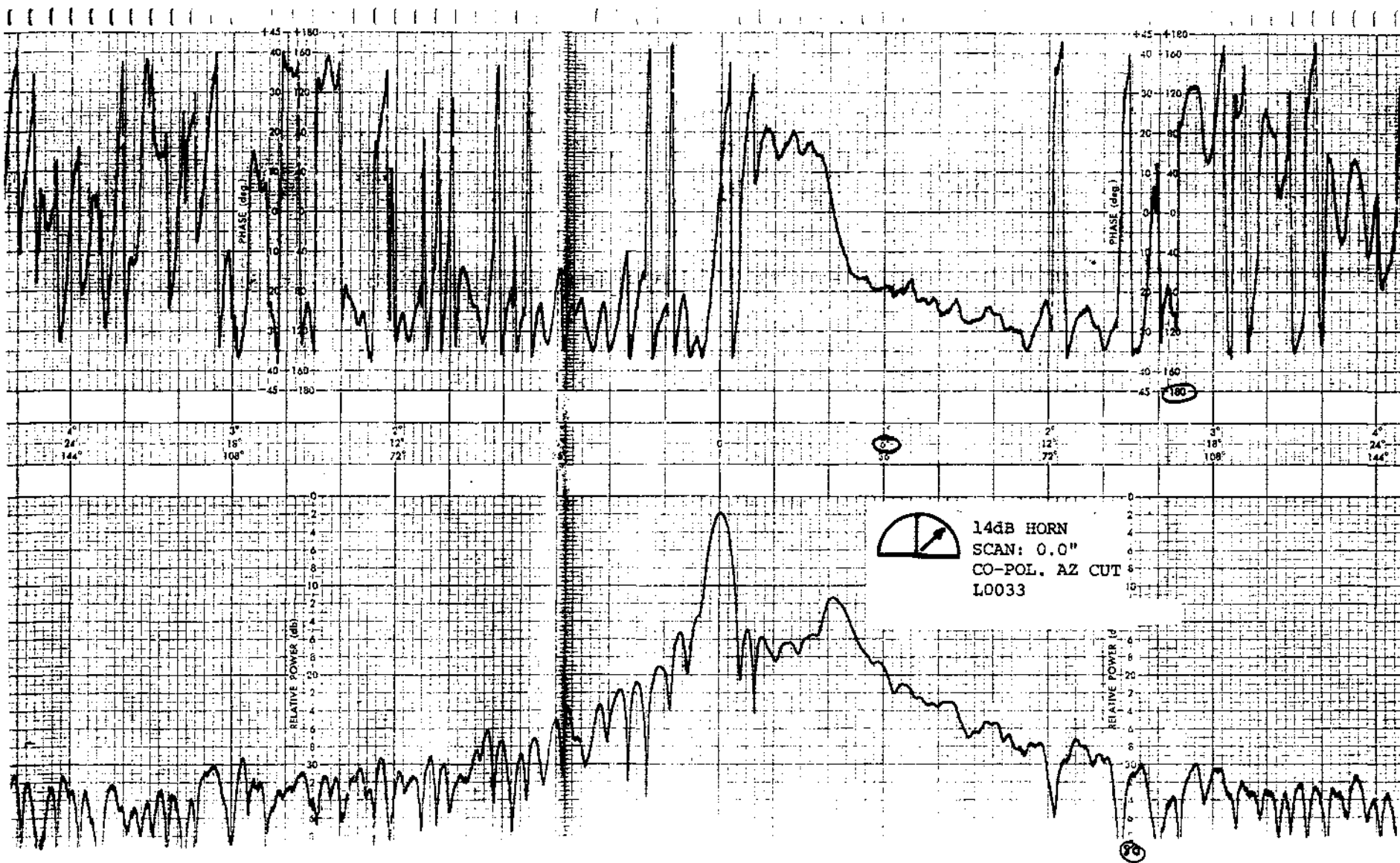


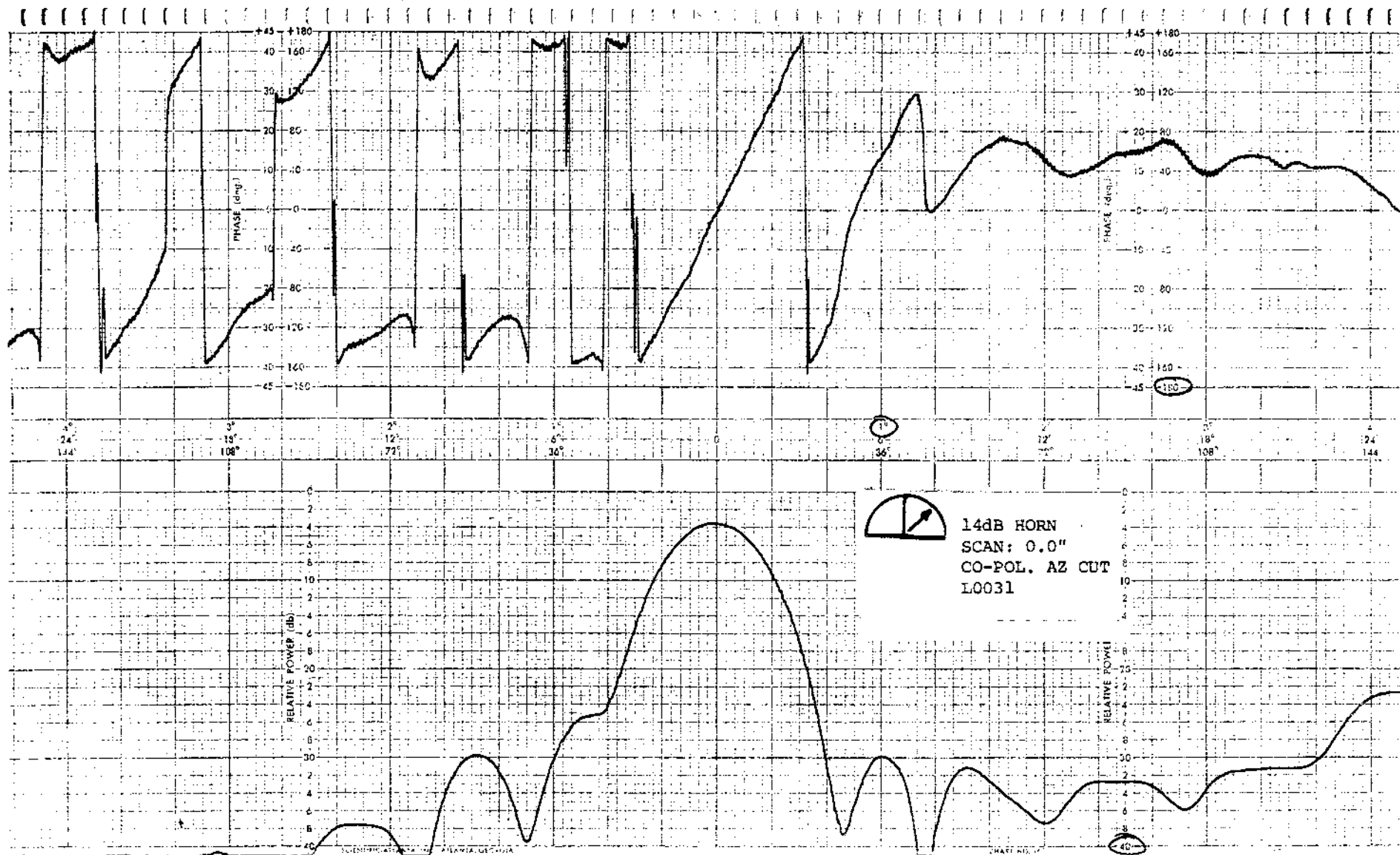
LSST - VIII

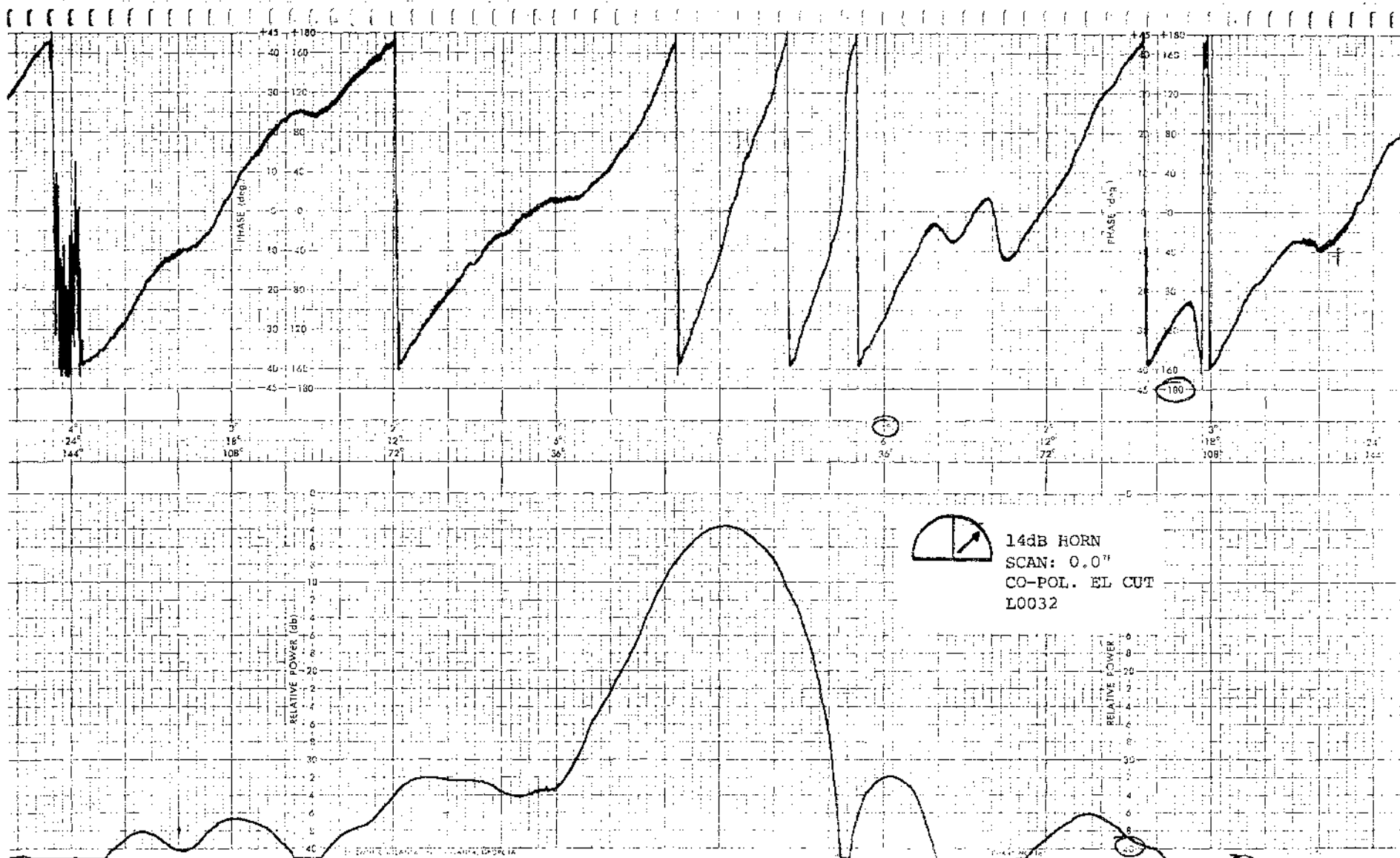
SECONDARY PATTERN LOG

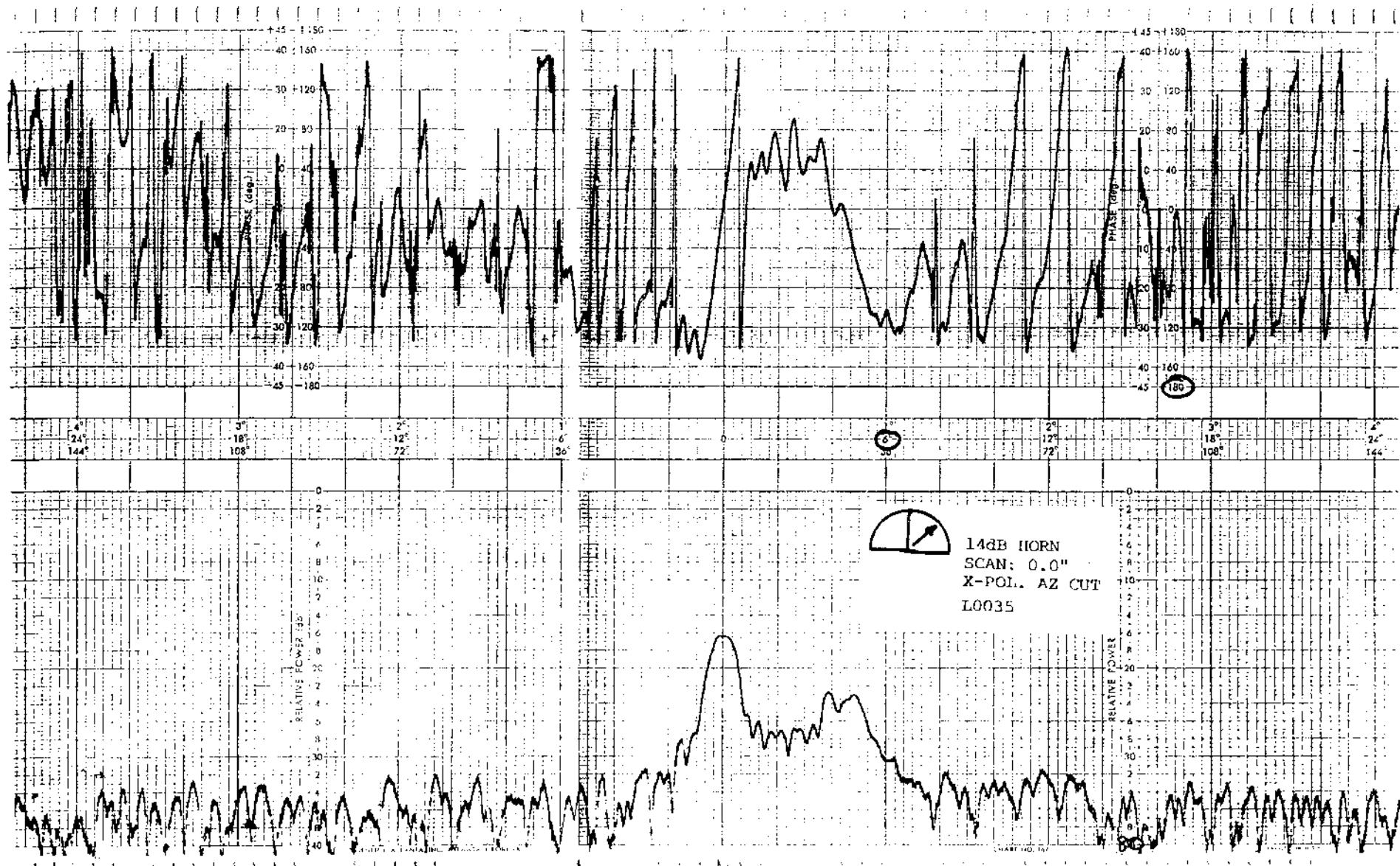
CONFIGURATION	HORN	SCAN	POL.	PK. GAIN	PATTERN	FILE NAME	PAGE NUMBER
	14 dB	0.0"	CO	50.39	$\pm 45^\circ$ AZ	L0033	246
	"	"	CO	"	$\pm 5^\circ$ AZ	L0031	247
	"	"	CO	"	$\pm 5^\circ$ EL	L0032	248
	"	"	X	-	$\pm 45^\circ$ AZ	L0035	249
	"	"	X	-	$\pm 5^\circ$ AZ	L0034	250
	"	"	X	-	$\pm 5^\circ$ EL	L0036	251
	14 dB	0.0"	CO	-	$+3^\circ$ EL $\pm 45^\circ$ AZ	R2101	252
	"	"	"	-	$+2^\circ$ EL "	R2102	253
	"	"	"	-	$+1^\circ$ EL "	R2103	254
	"	"	"	50.55	$0^\circ$ EL "	R2104	255
	"	"	"	-	$-1^\circ$ EL "	R2105	256
	"	"	"	-	$-2^\circ$ EL "	R2106	257
	"	"	"	-	$-3^\circ$ EL "	R2107	258
	14 dB	0.0"	X	-	$+3^\circ$ EL $\pm 45^\circ$ AZ	R2201	259
	"	"	"	-	$+2^\circ$ EL "	R2202	260
	"	"	"	-	$+1^\circ$ EL "	R2203	261
	"	"	"	-	$0^\circ$ EL "	R2204	262
	"	"	"	-	$-1^\circ$ EL "	R2205	263
	"	"	"	-	$-2^\circ$ EL "	R2206	264
	"	"	"	-	$-3^\circ$ EL "	R2207	265
	14 dB	4.5"	CO	50.00	$\pm 45^\circ$ AZ	L0039	266
	"	"	CO	"	$\pm 5^\circ$ AZ	L0037	267
	"	"	CO	"	$\pm 5^\circ$ EL	L0038	268
	"	"	X	-	$\pm 45^\circ$ AZ	L0042	269
	"	"	X	-	$\pm 5^\circ$ AZ	L0040	270
	"	"	X	-	$\pm 5^\circ$ EL	L0041	271
	14 dB	0.0"	CO	50.55	$\pm 45^\circ$ AZ	L0057	272
	"	"	CO	"	$\pm 5^\circ$ AZ	L0055	273
	"	"	CO	"	$\pm 5^\circ$ EL	L0056	274
	"	"	X	-	$\pm 45^\circ$ AZ	L0060	275
	"	"	X	-	$\pm 5^\circ$ AZ	L0058	276
	"	"	X	-	$\pm 5^\circ$ EL	L0059	277

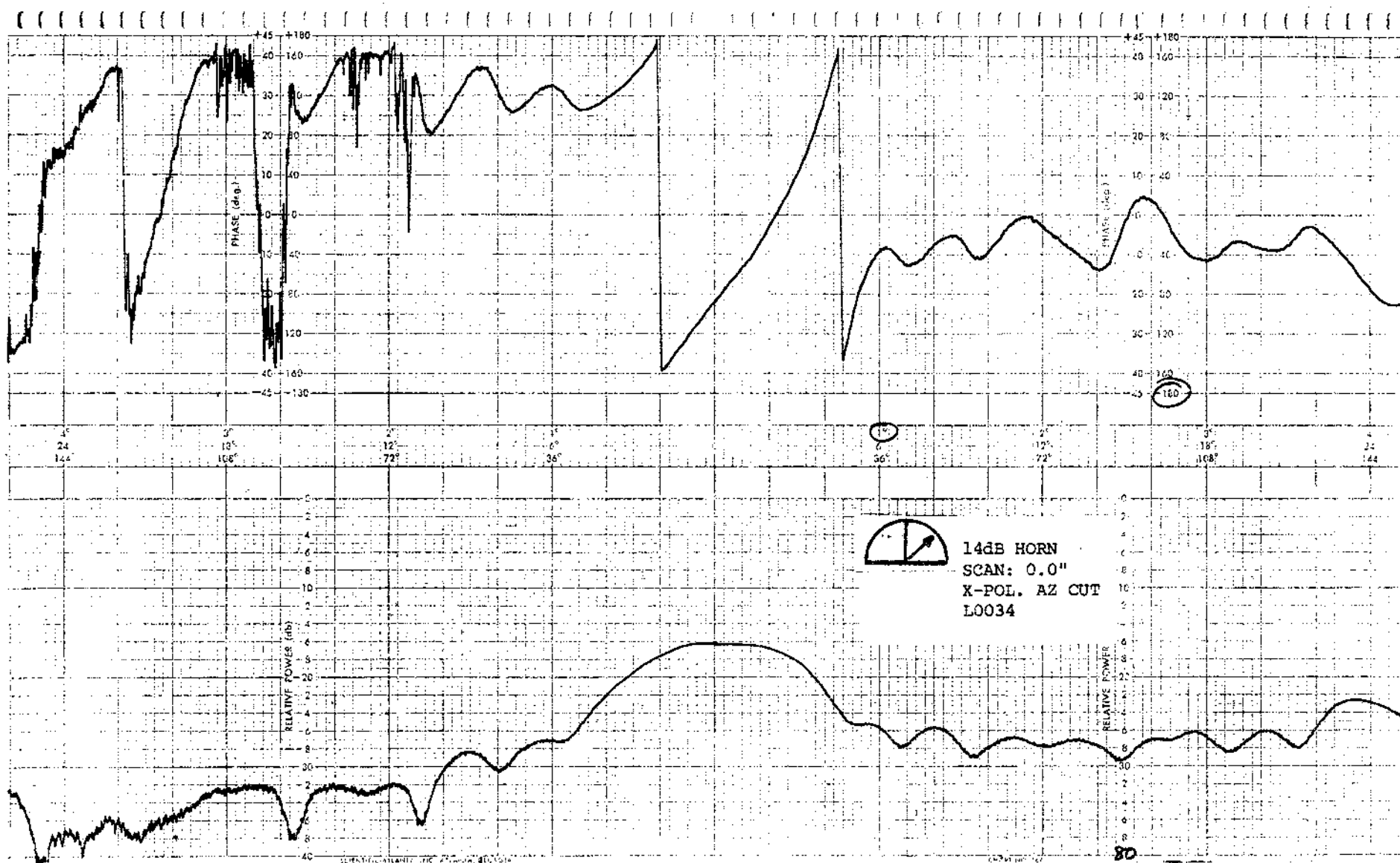


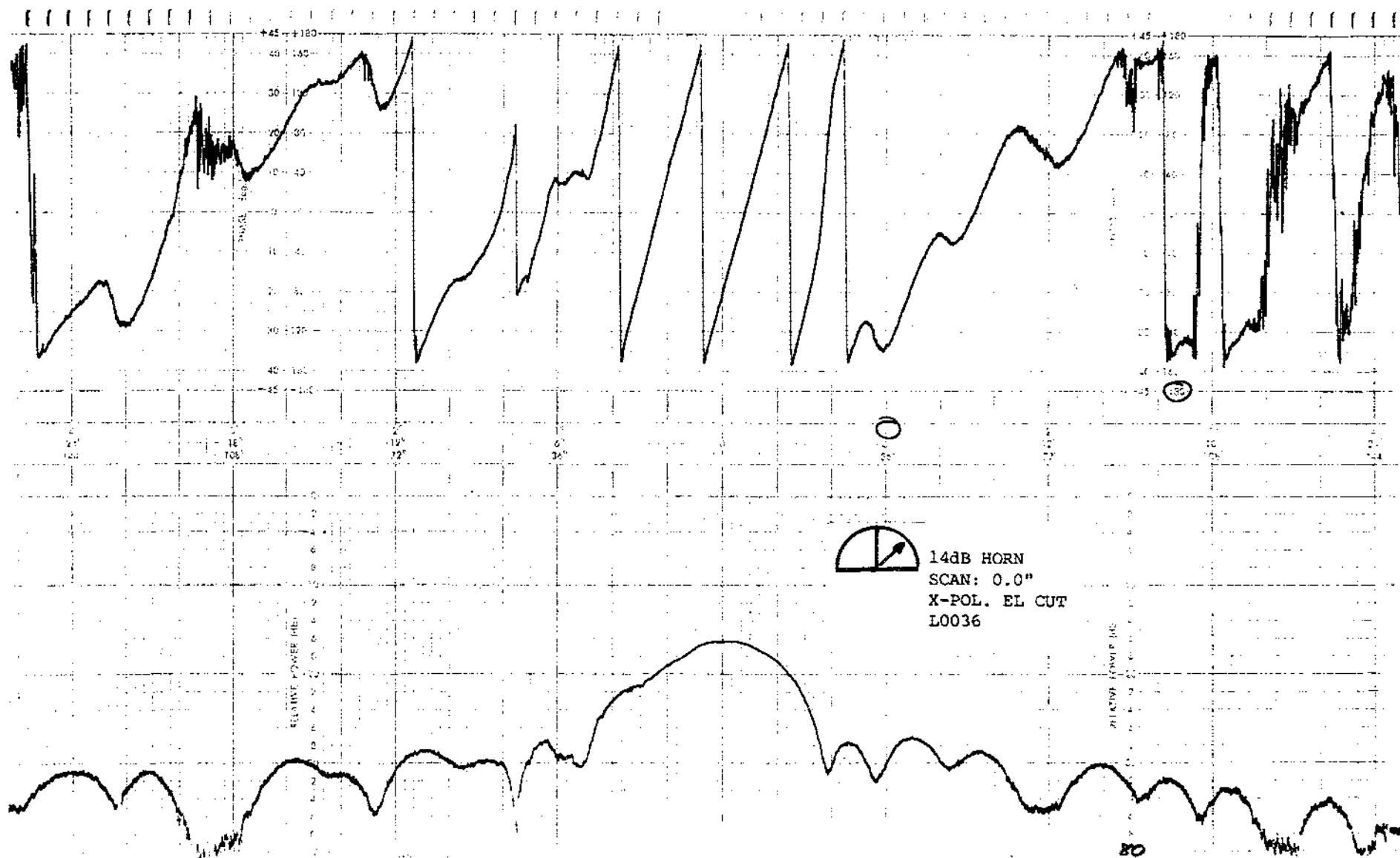


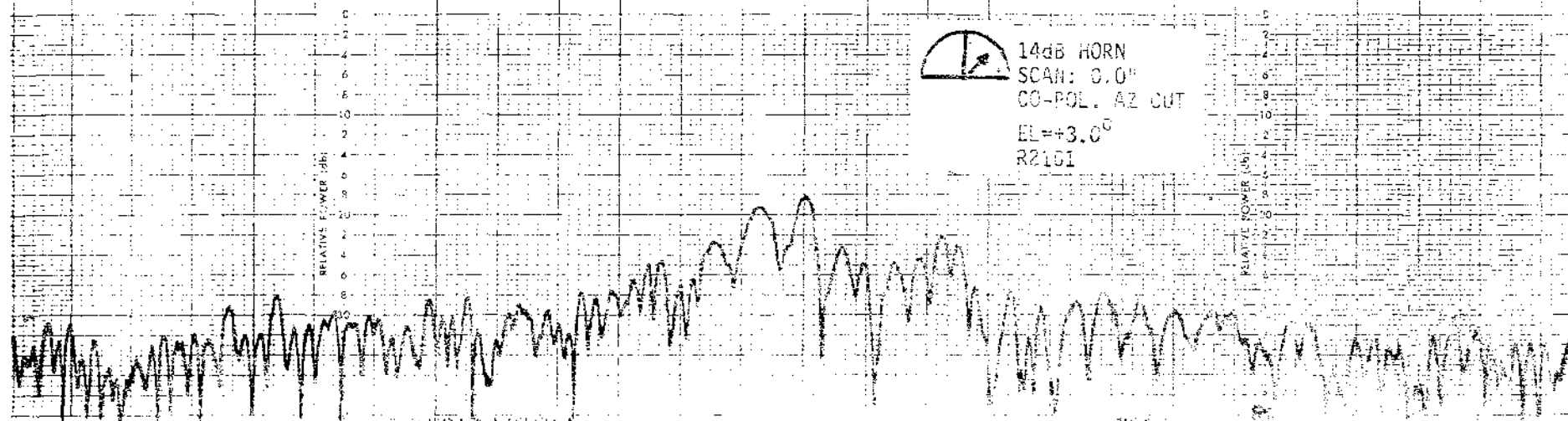
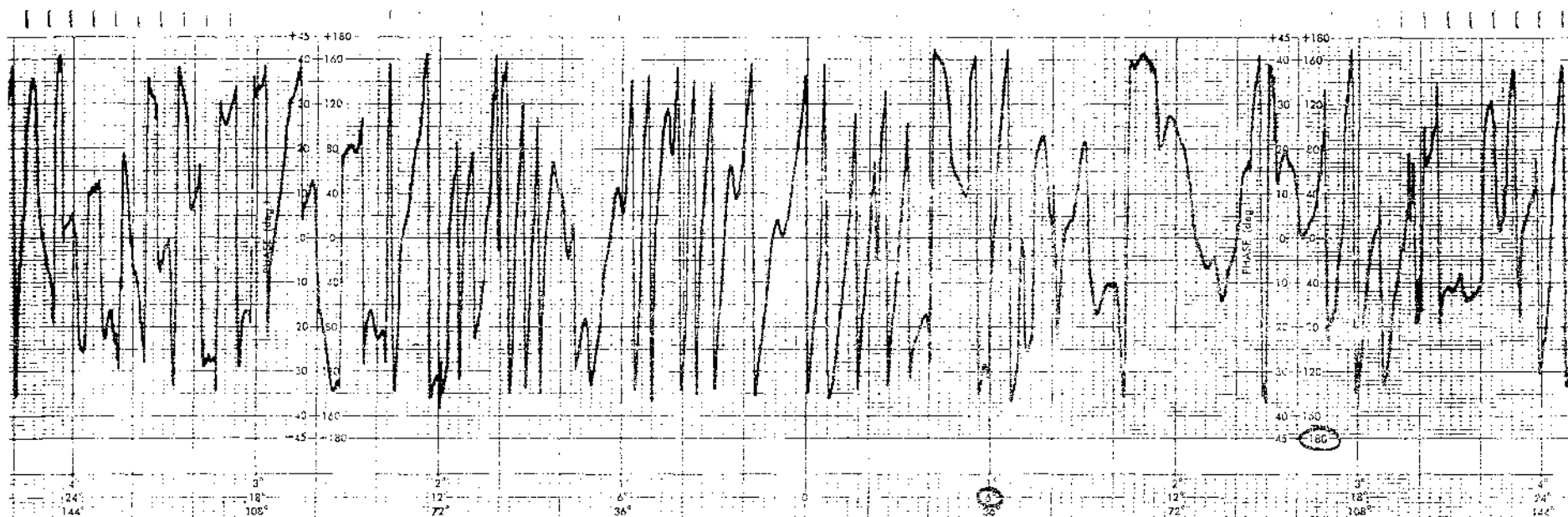


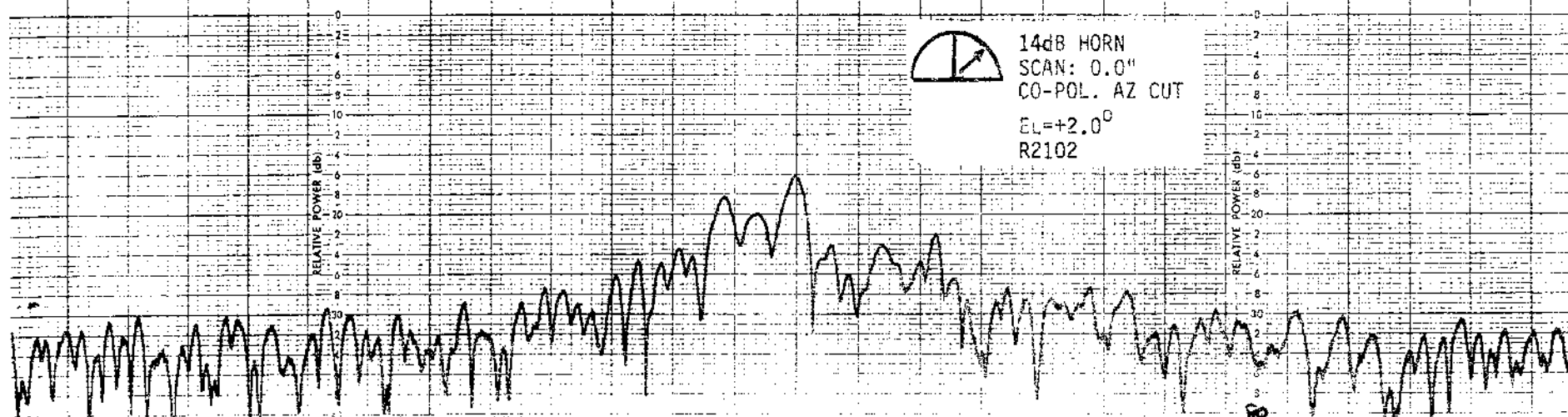




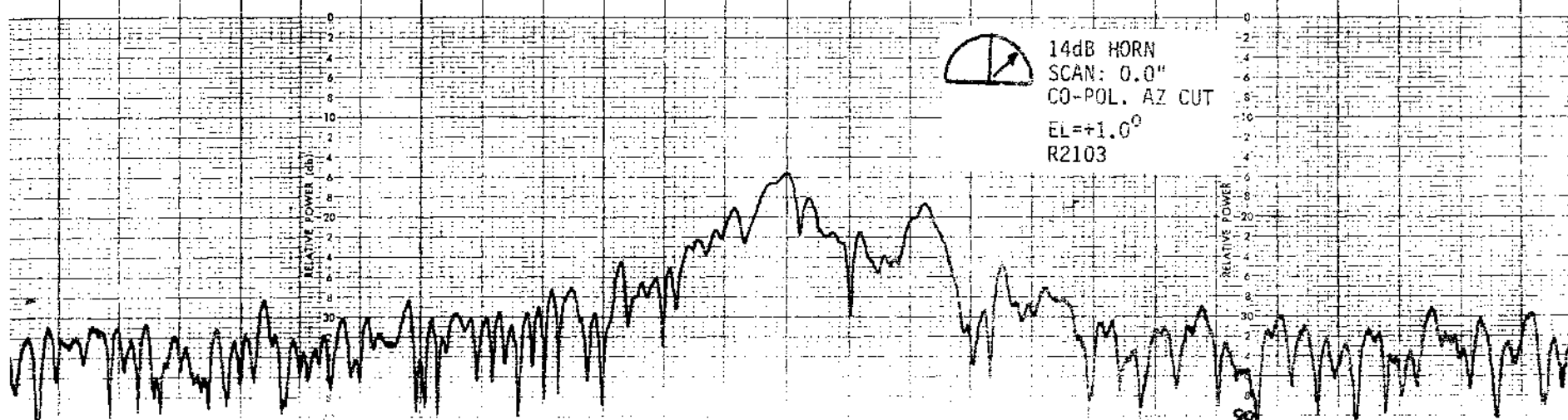
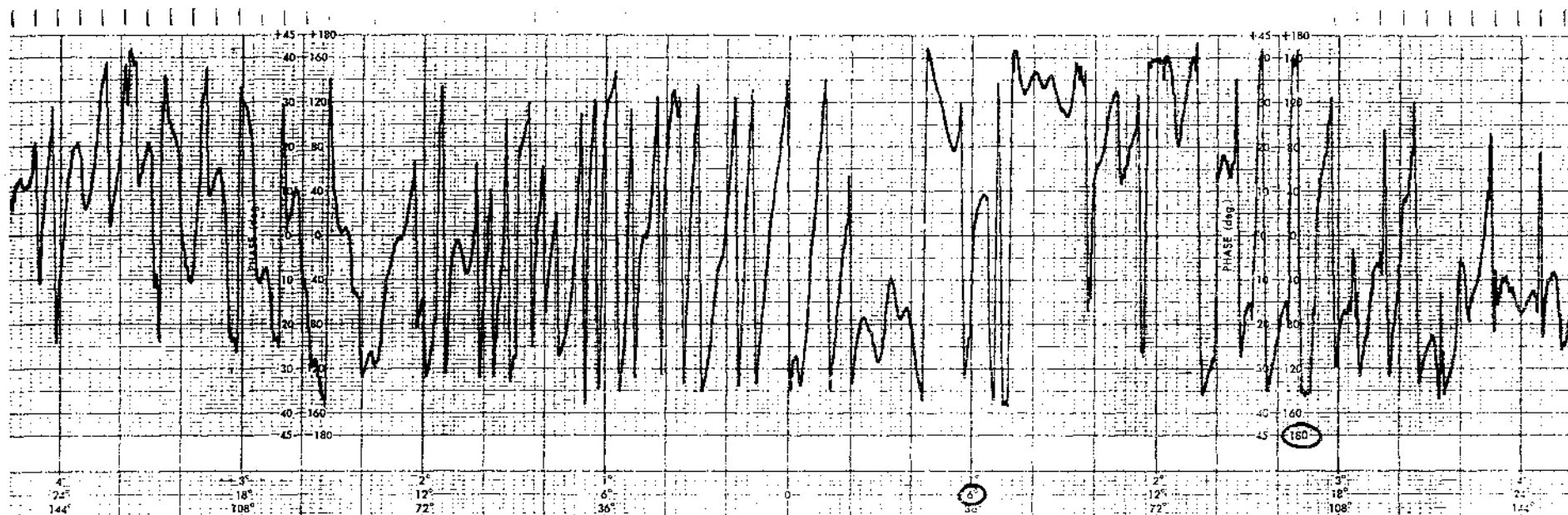




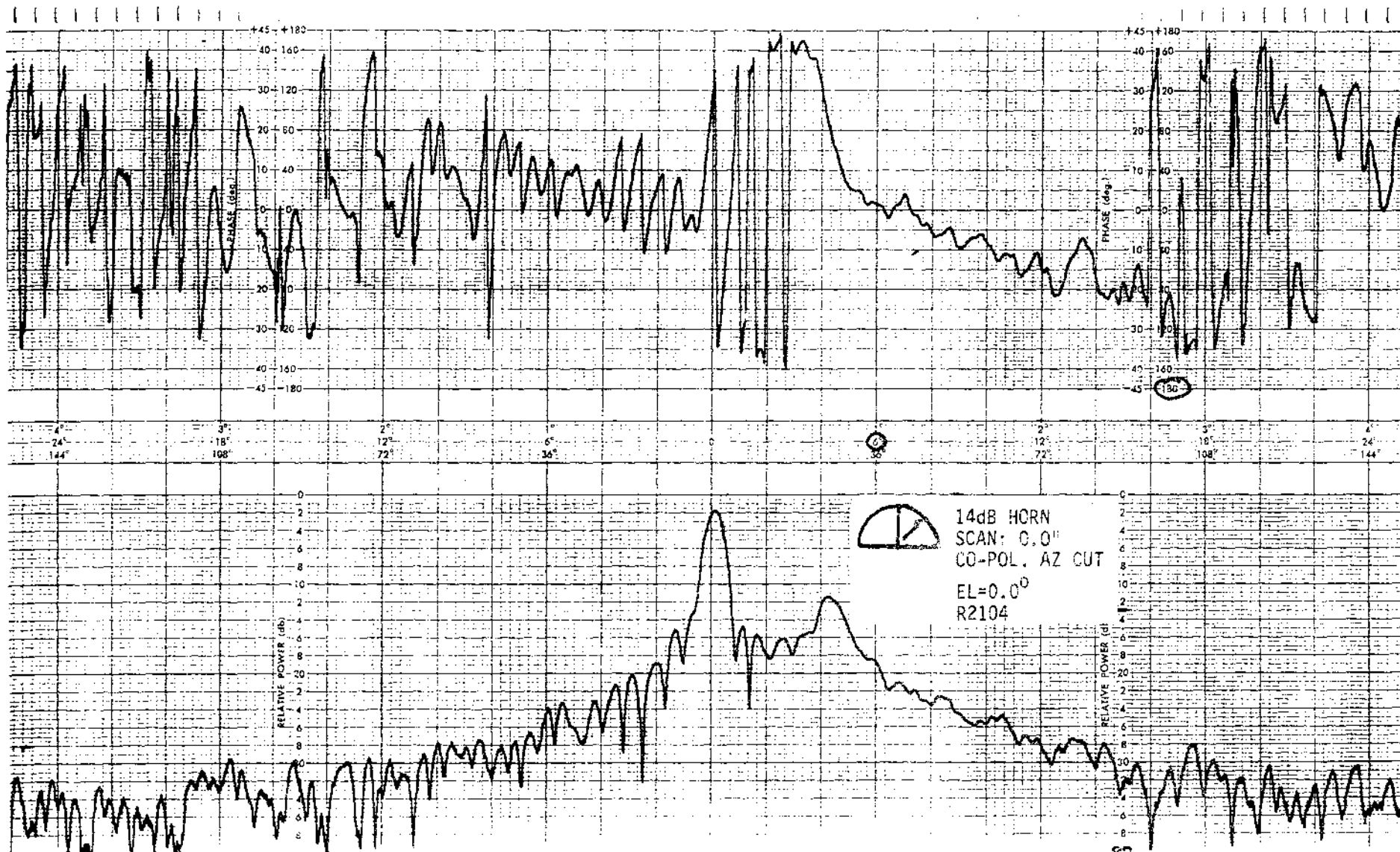


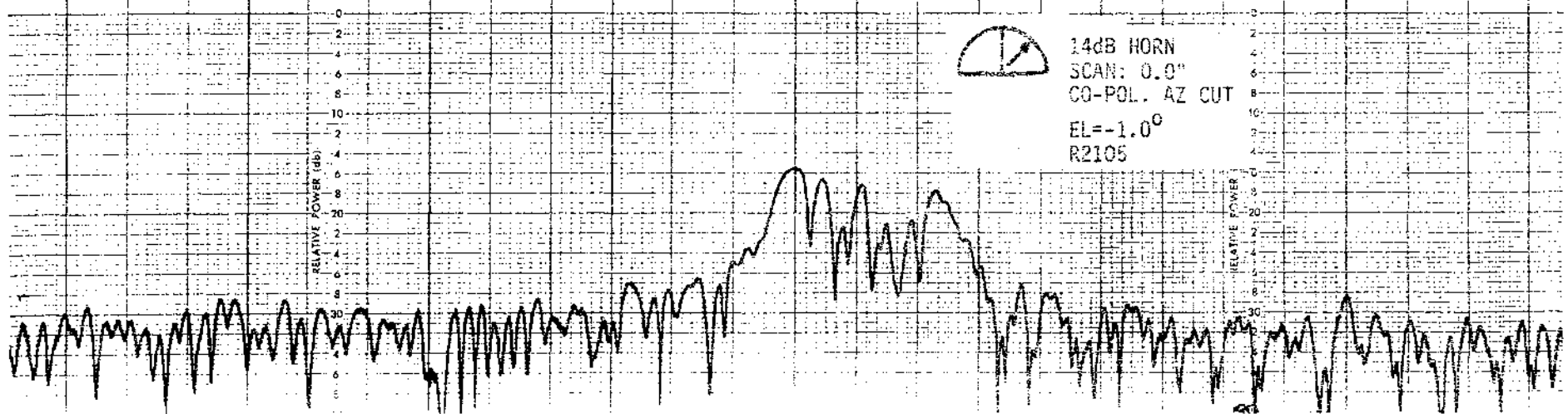
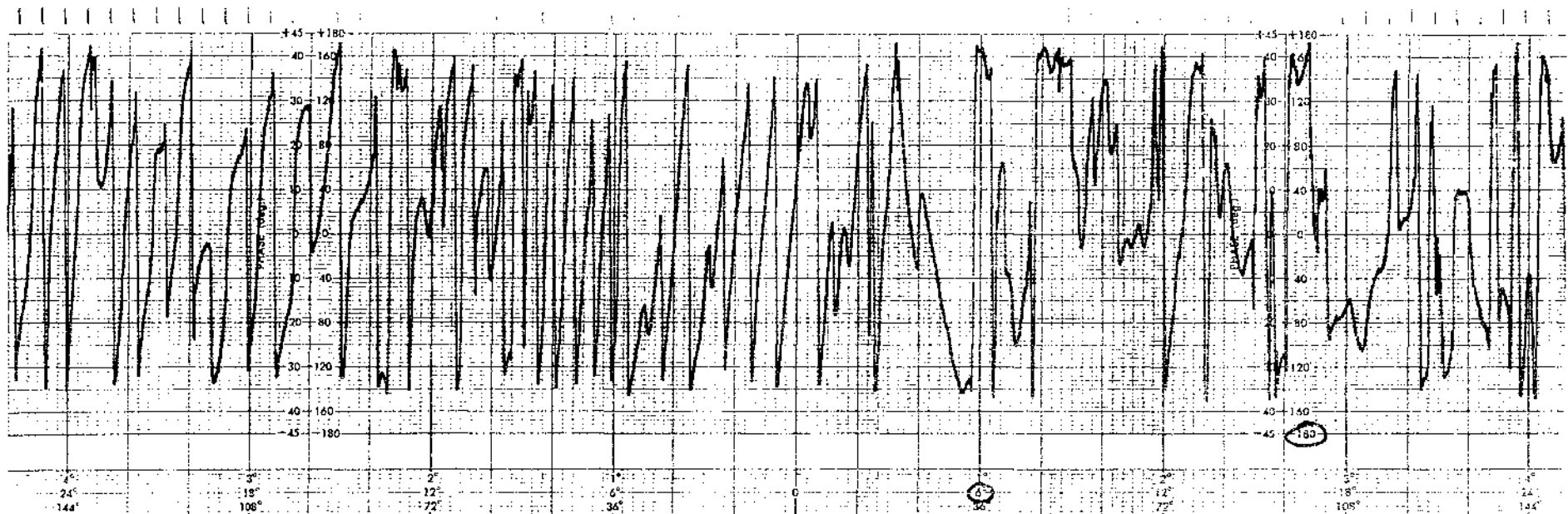




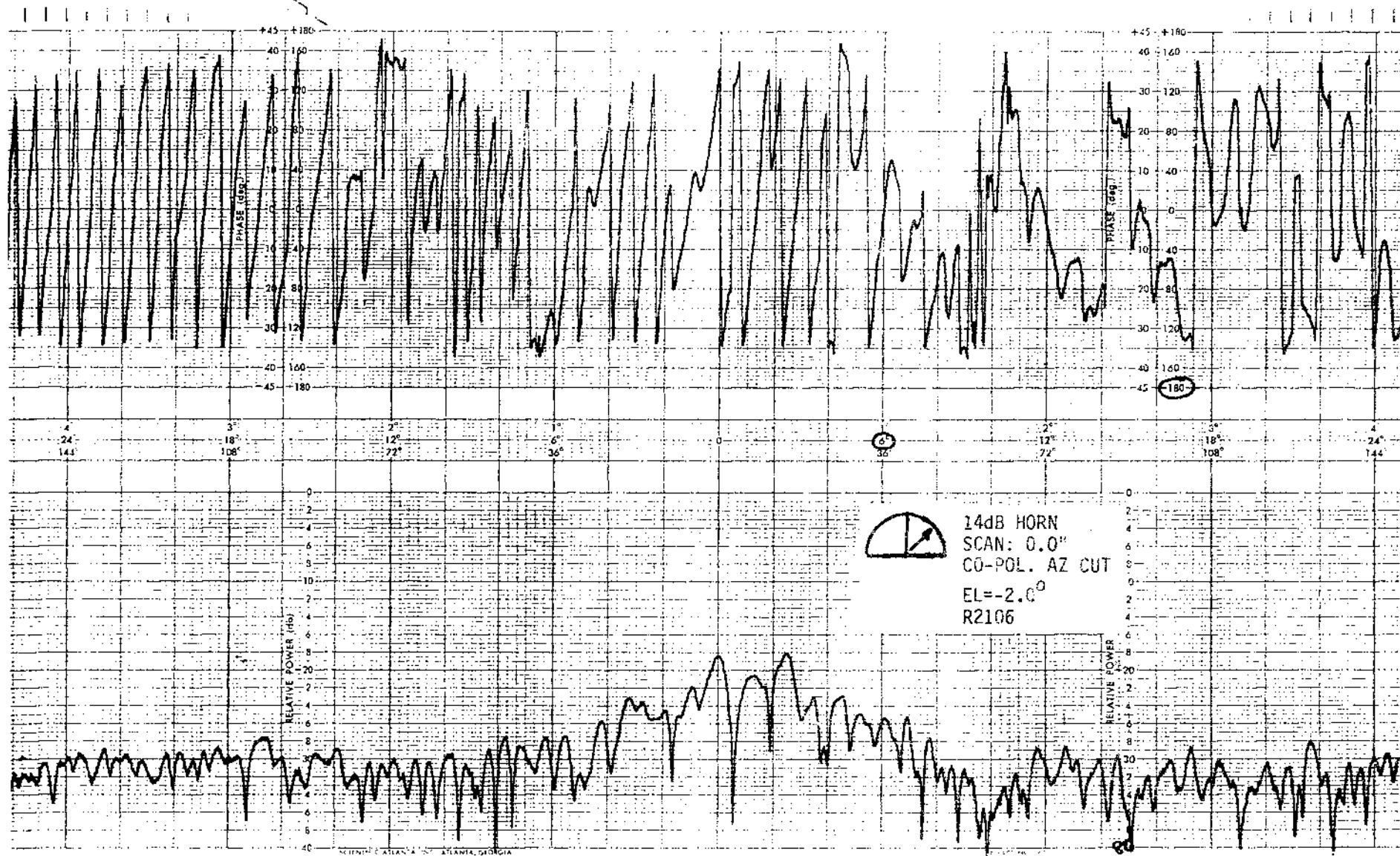


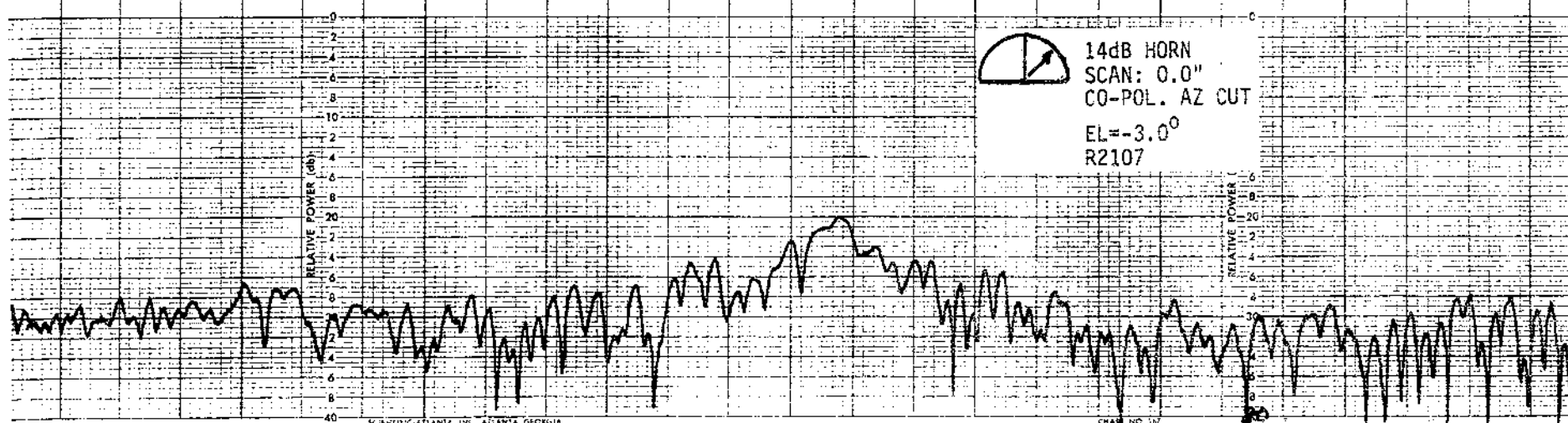
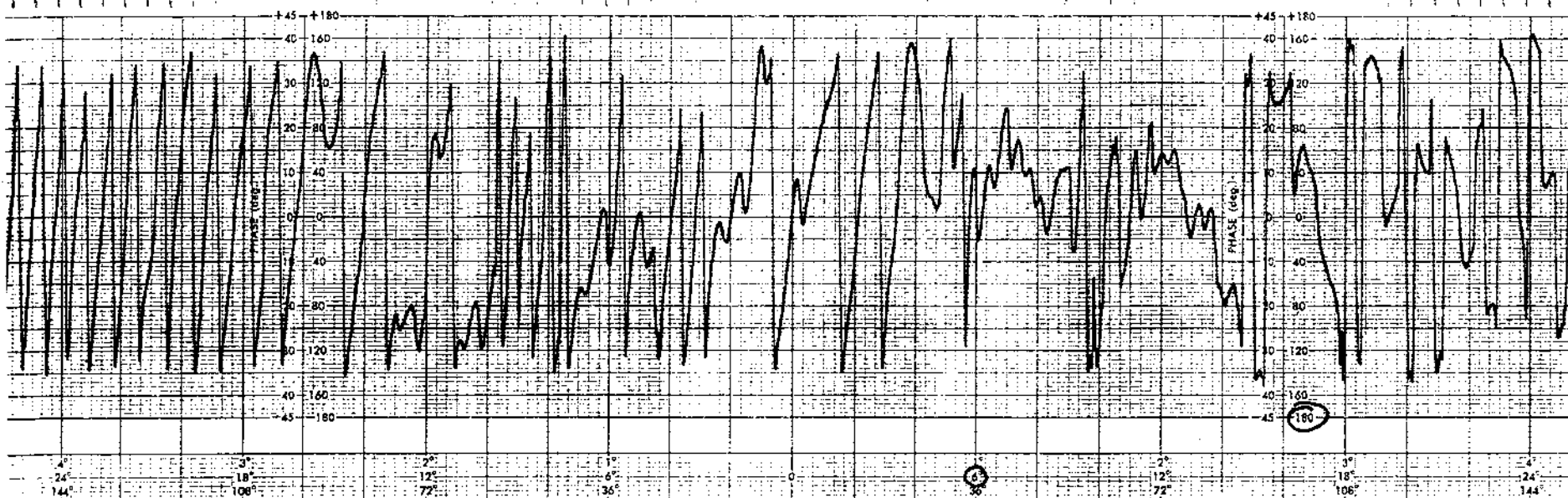
14dB HORN  
 SCAN: 0.0"  
 CO-POL. AZ CUT  
 EL=+1.0°  
 R2103

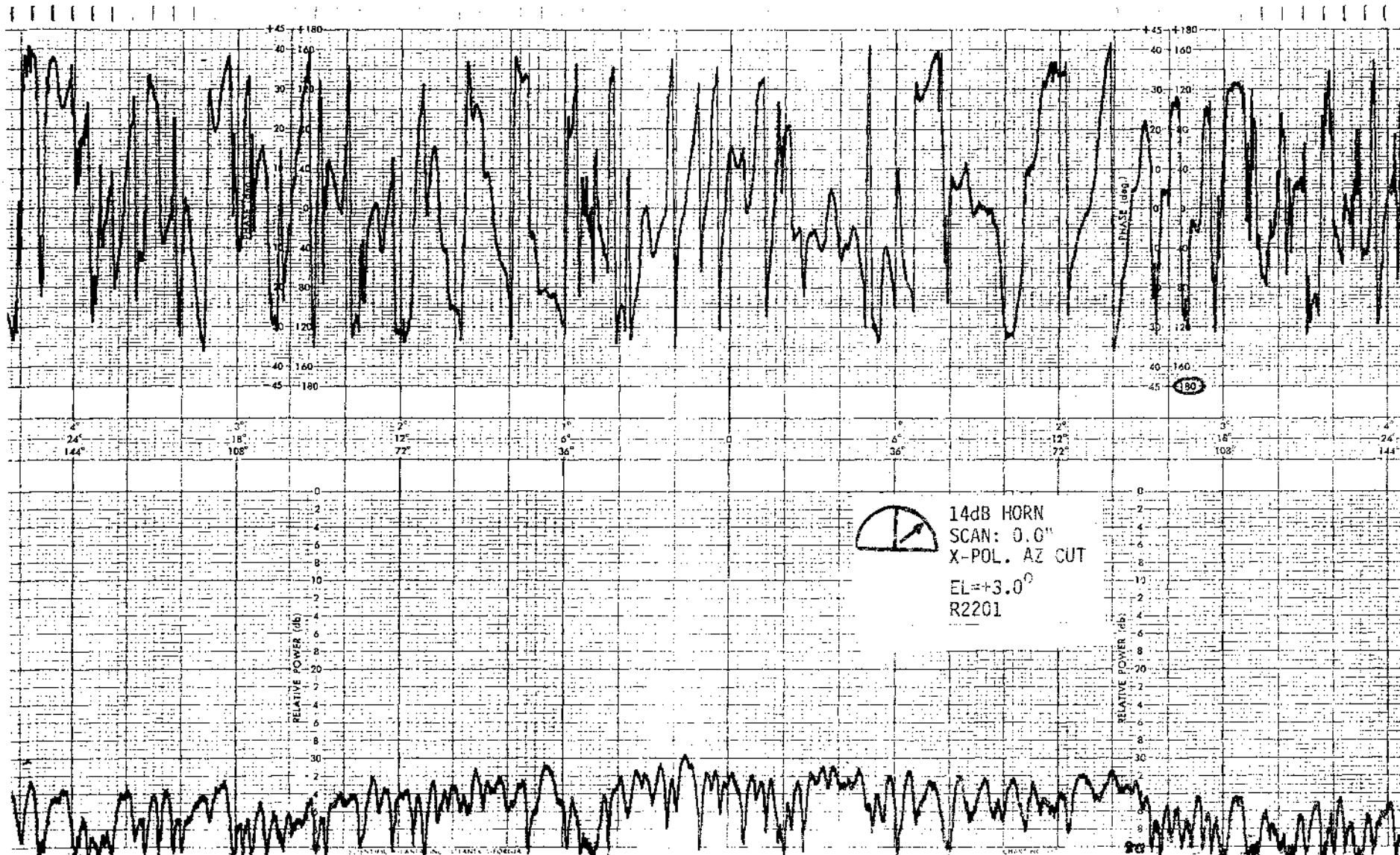


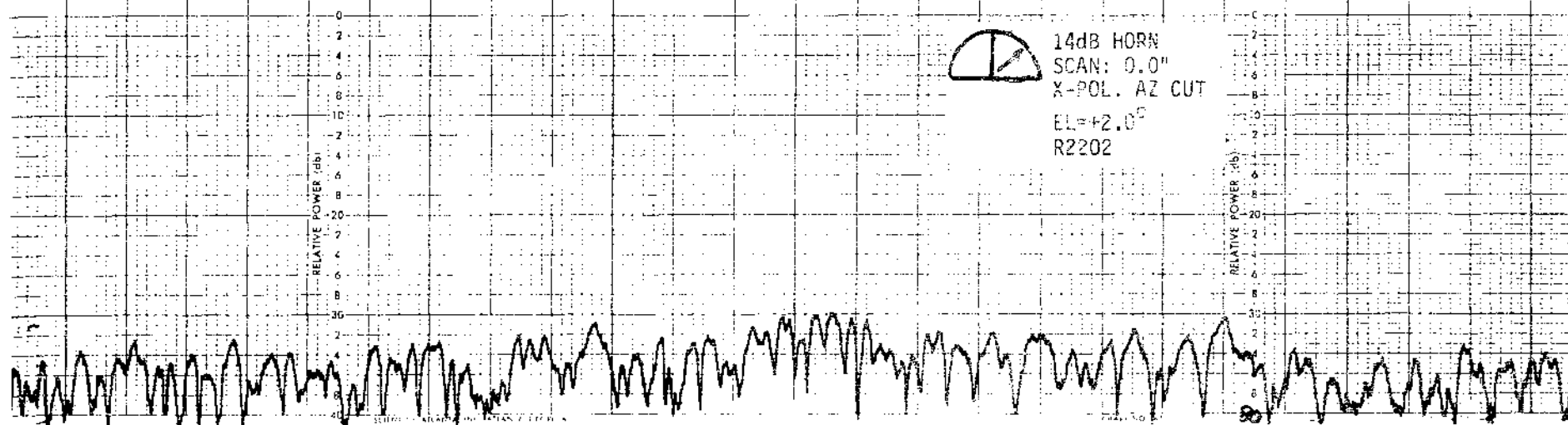
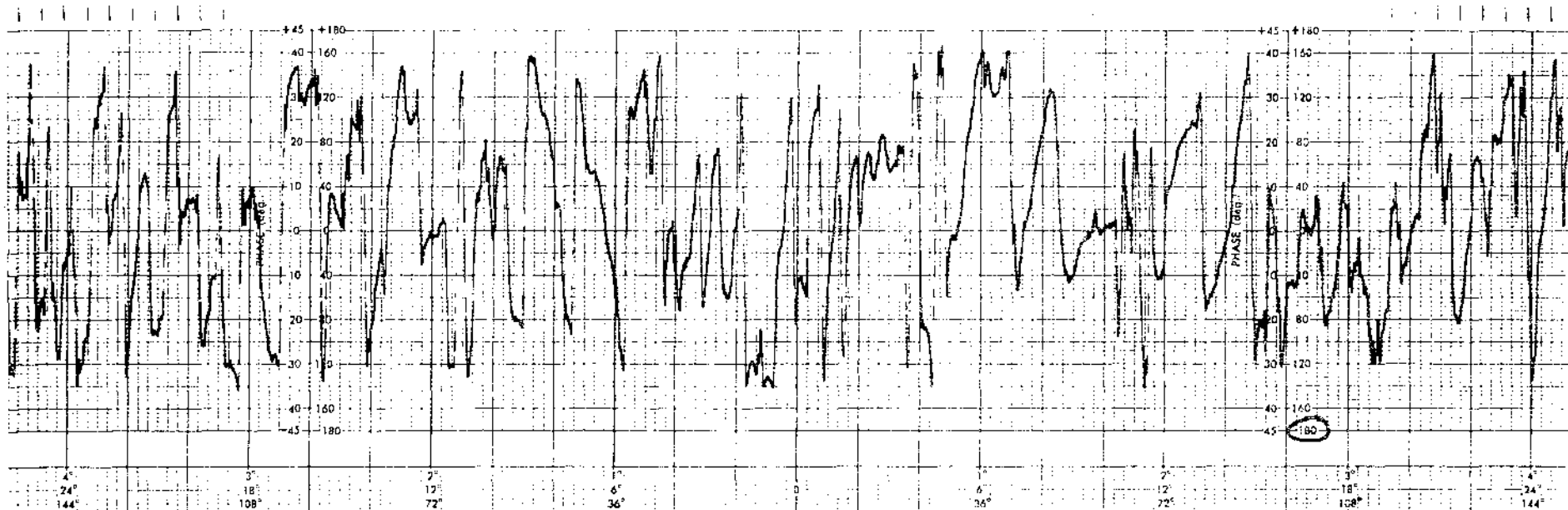


14dB HORN  
 SCAN: 0.0°  
 CO-POL. AZ CUT  
 EL=-1.0°  
 R2105

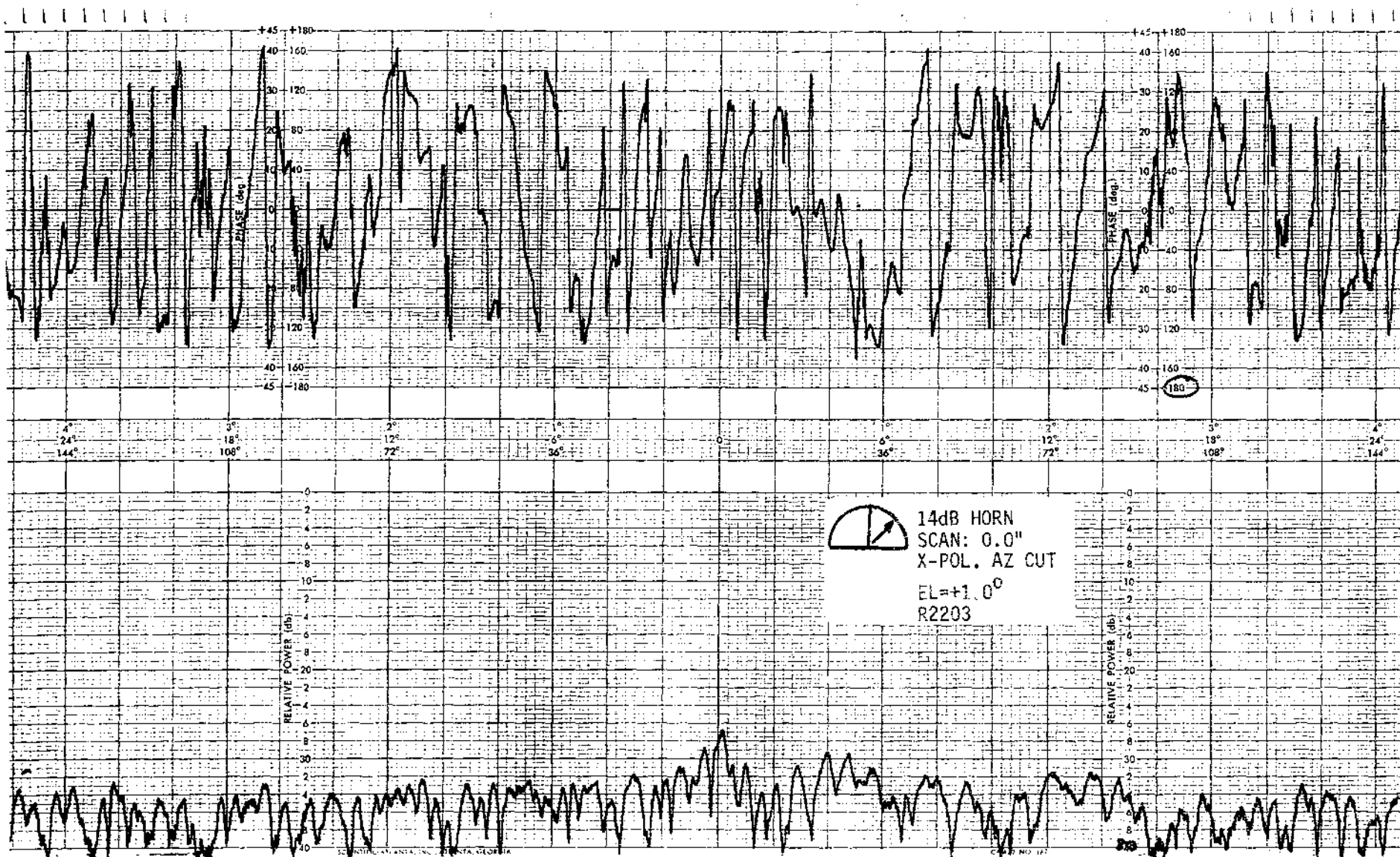




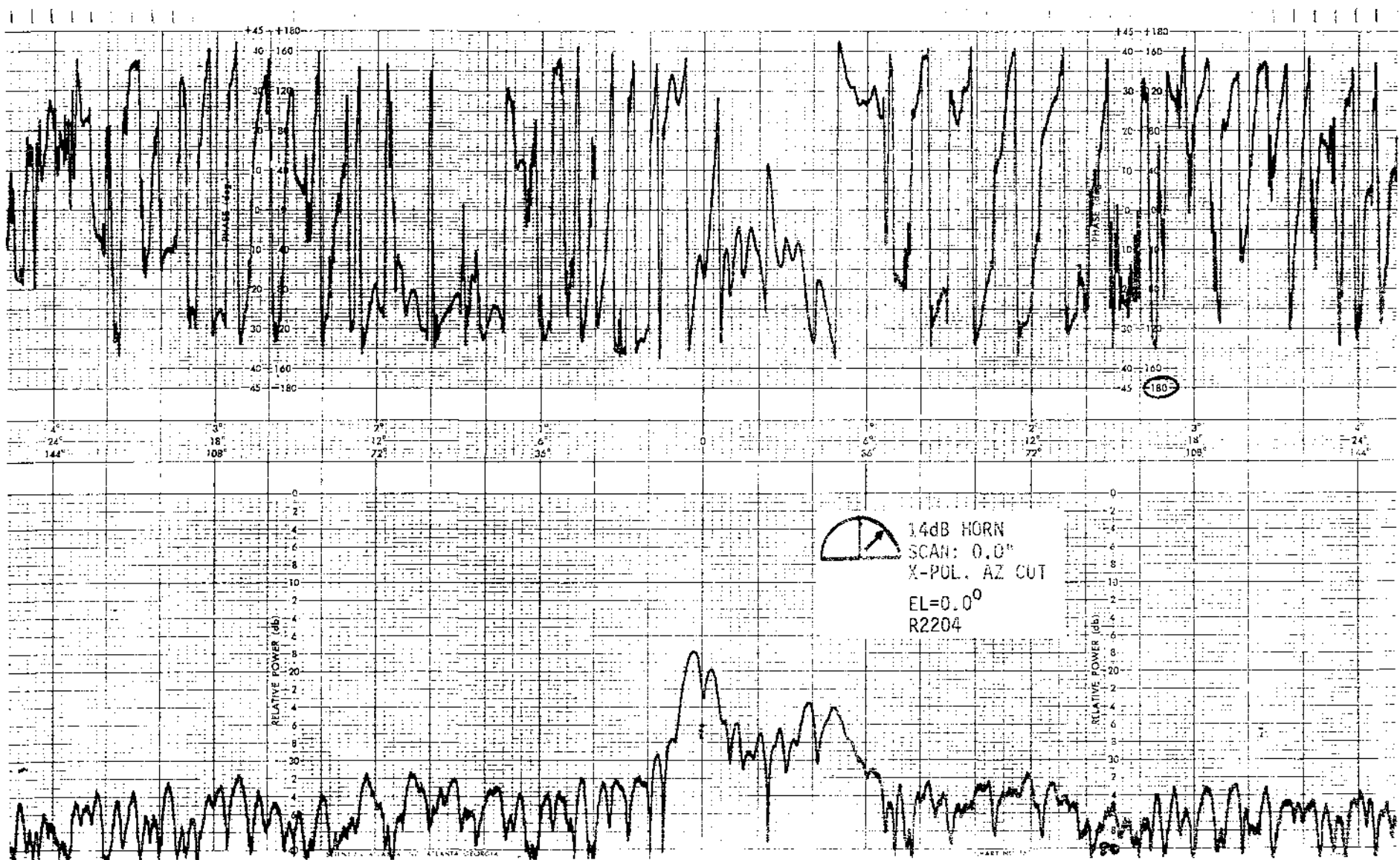


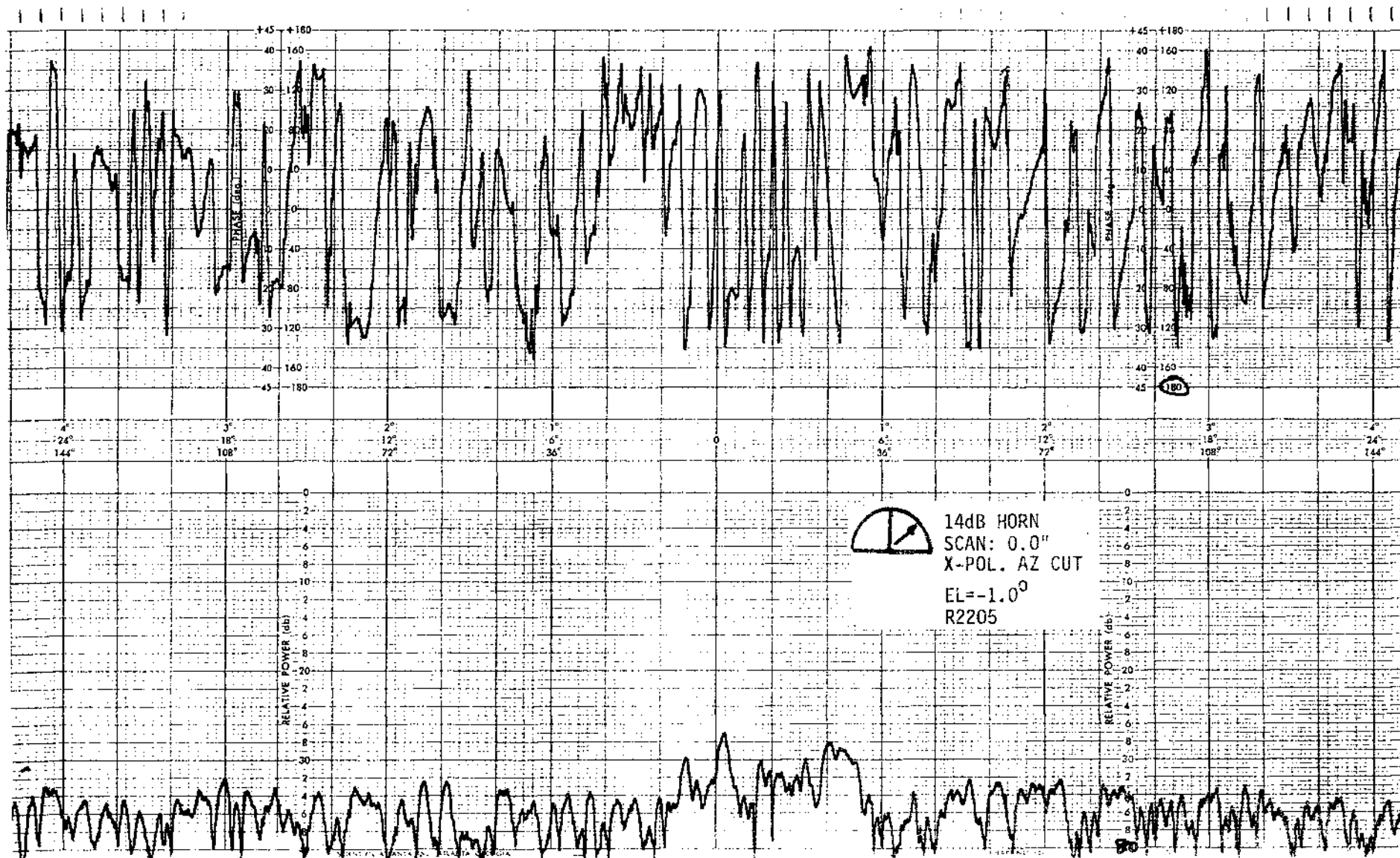


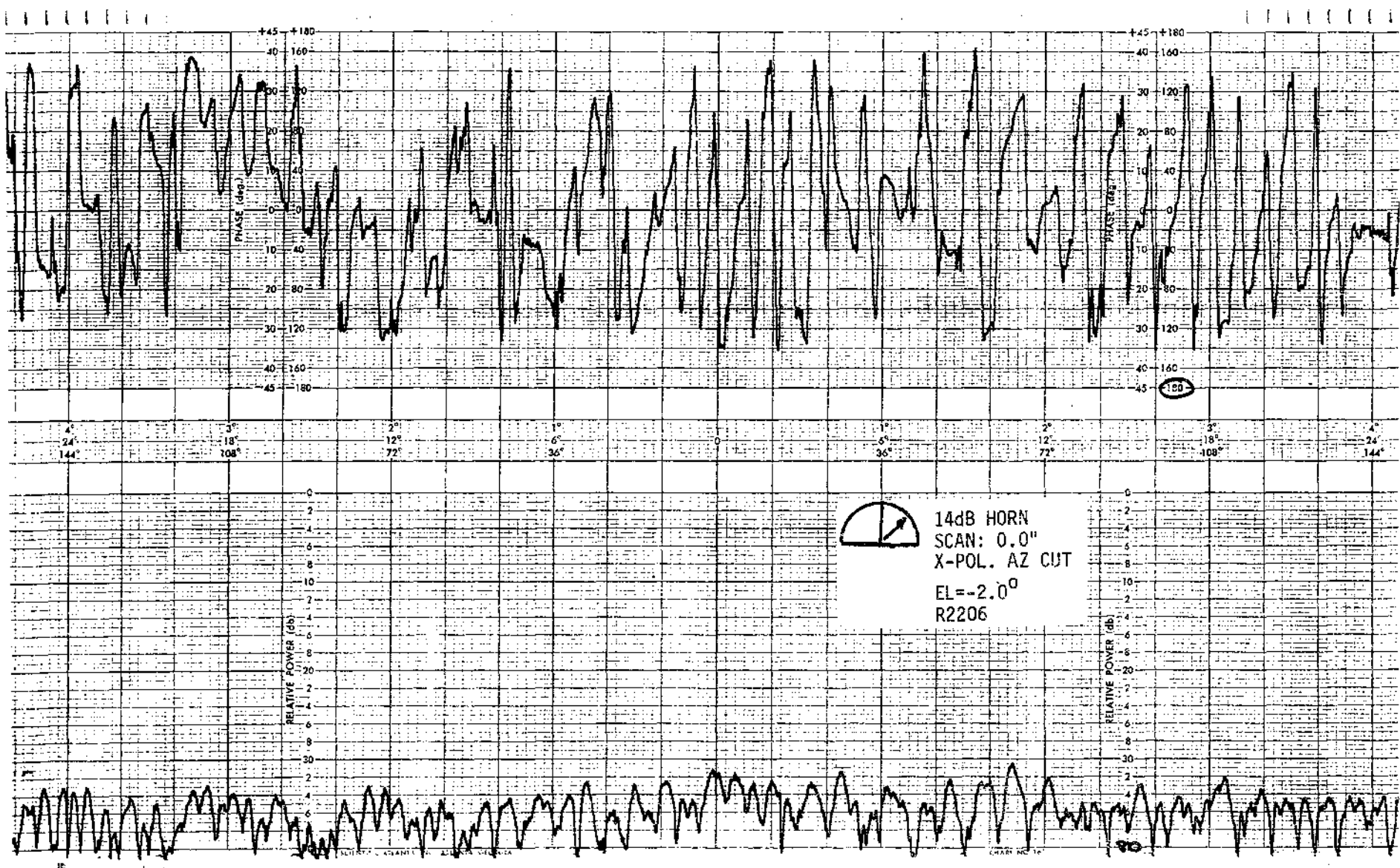


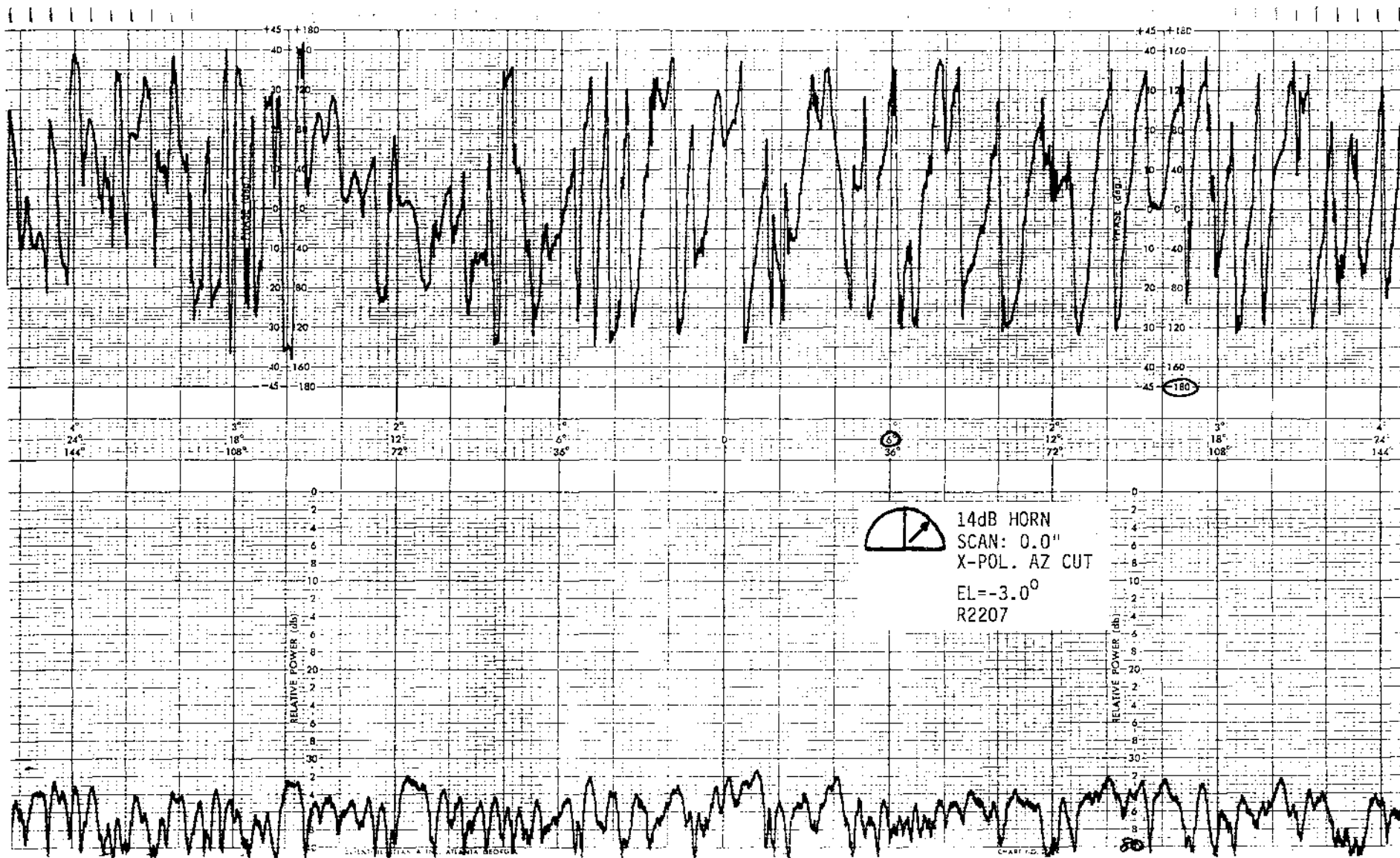


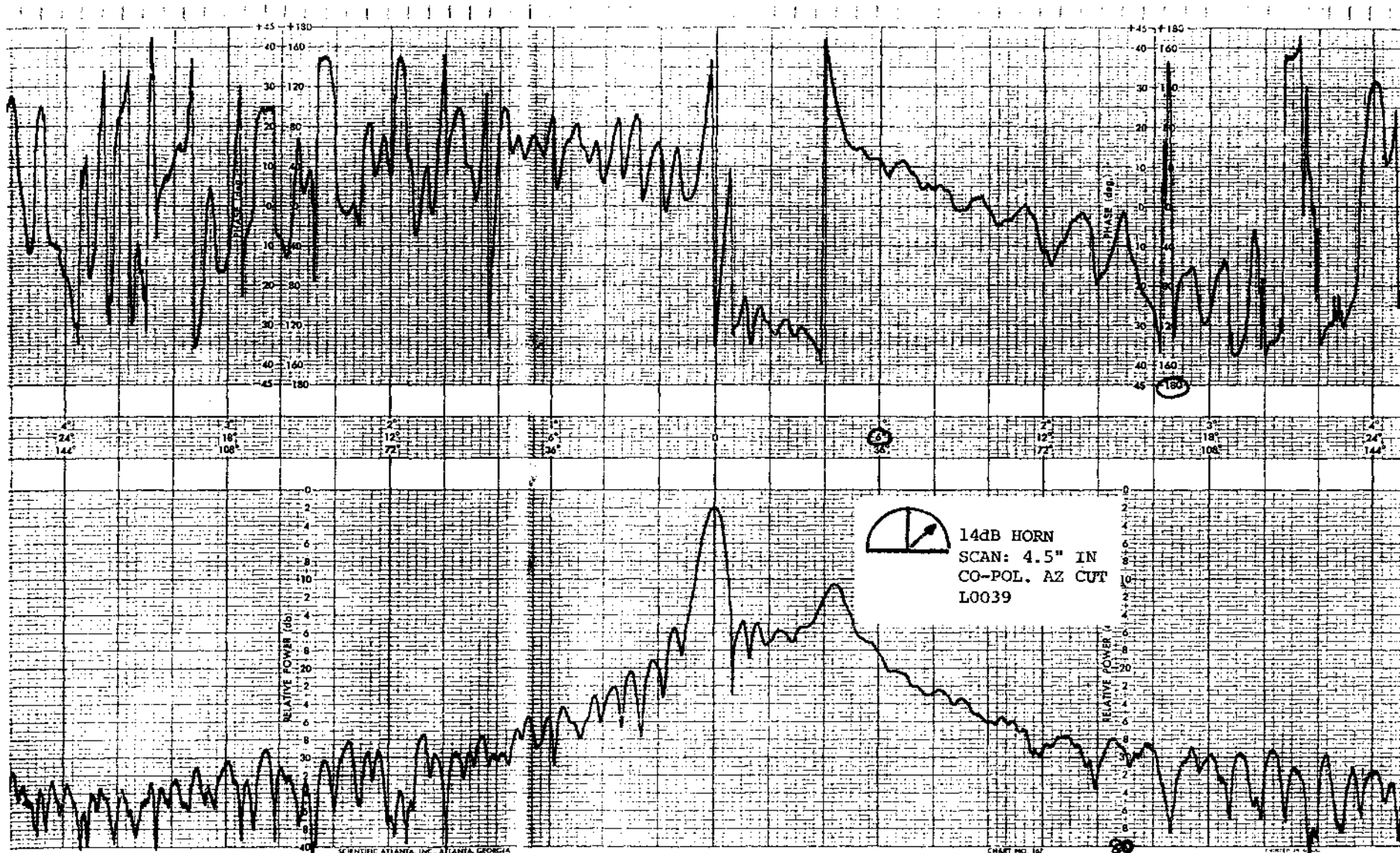


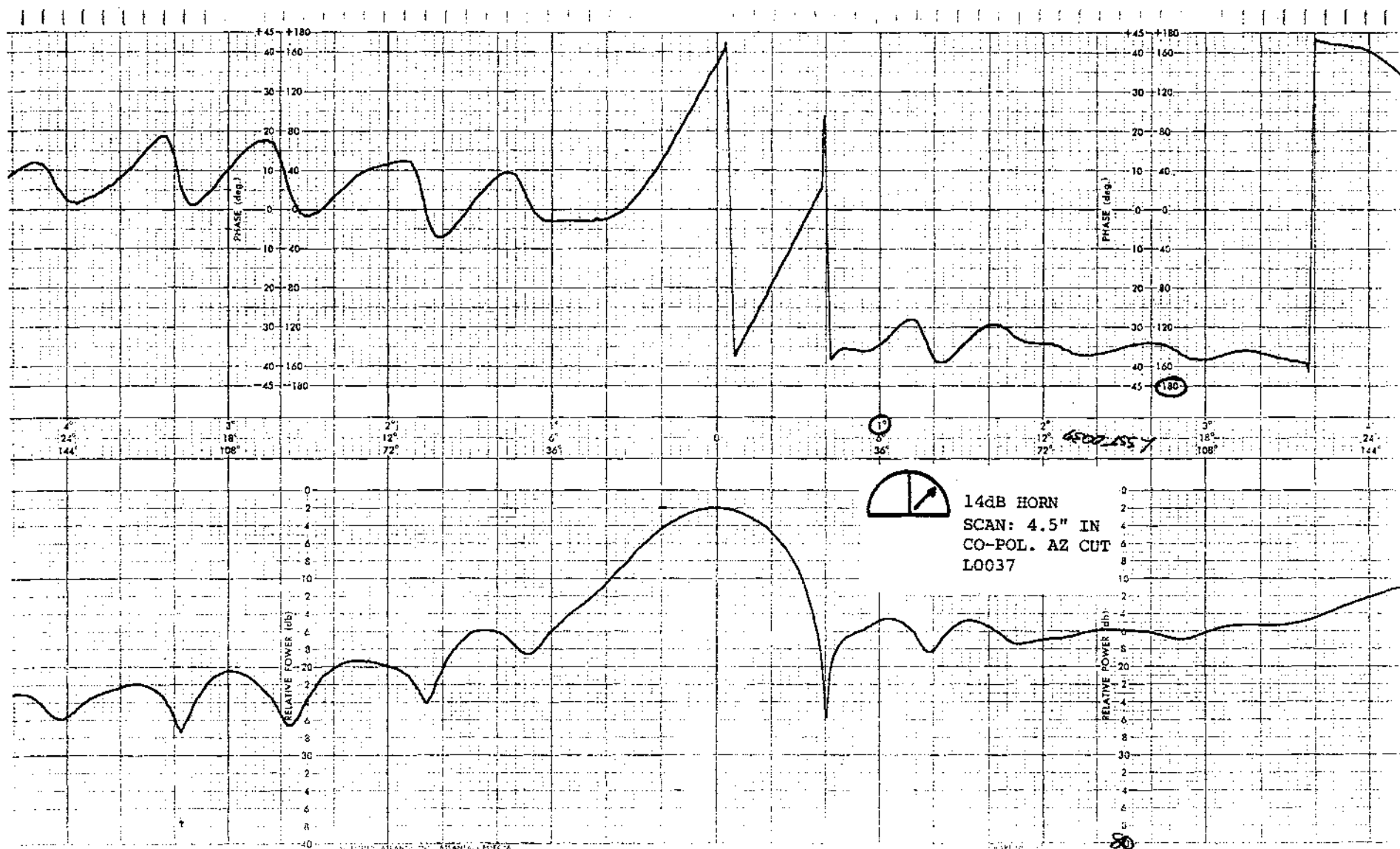


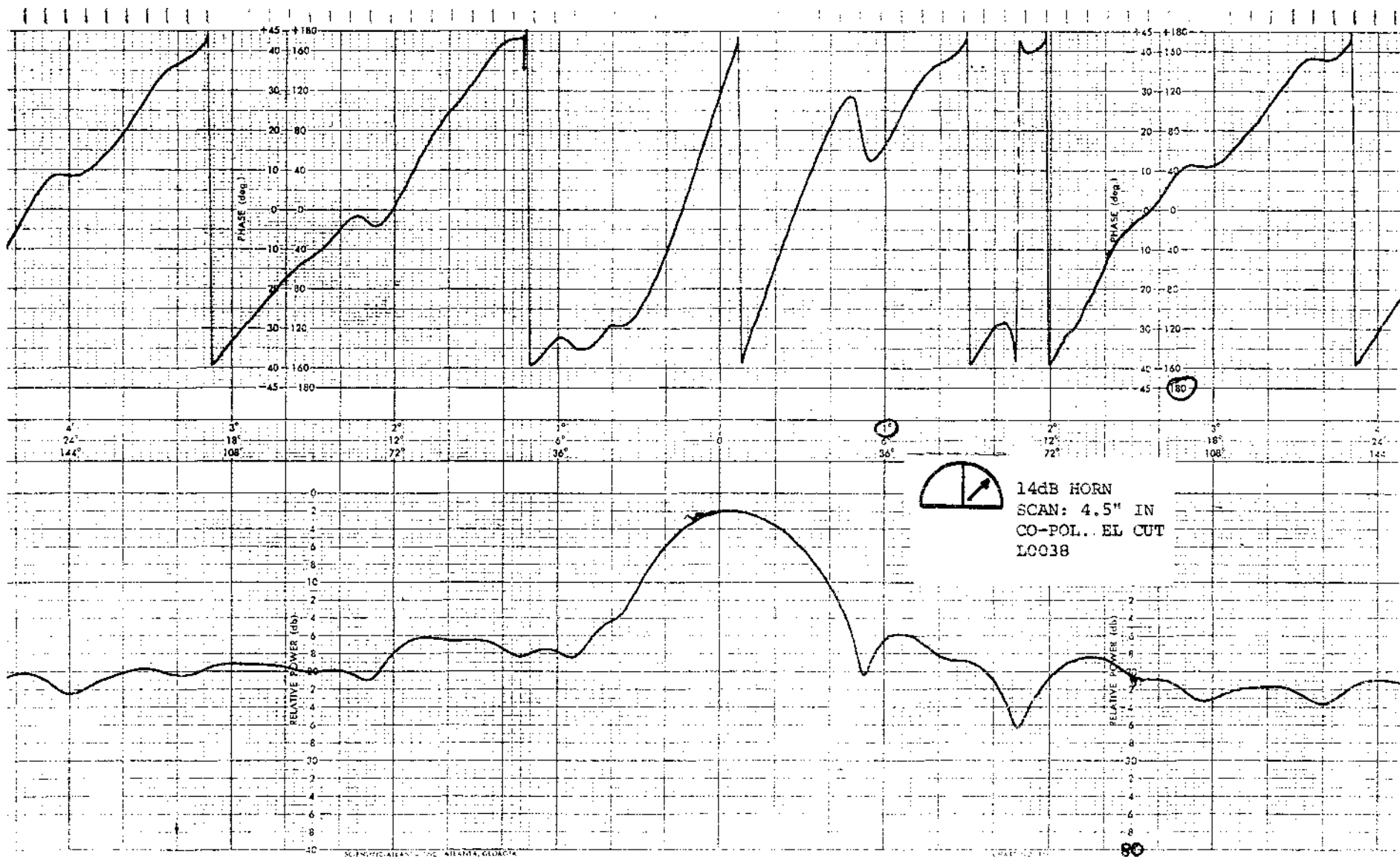




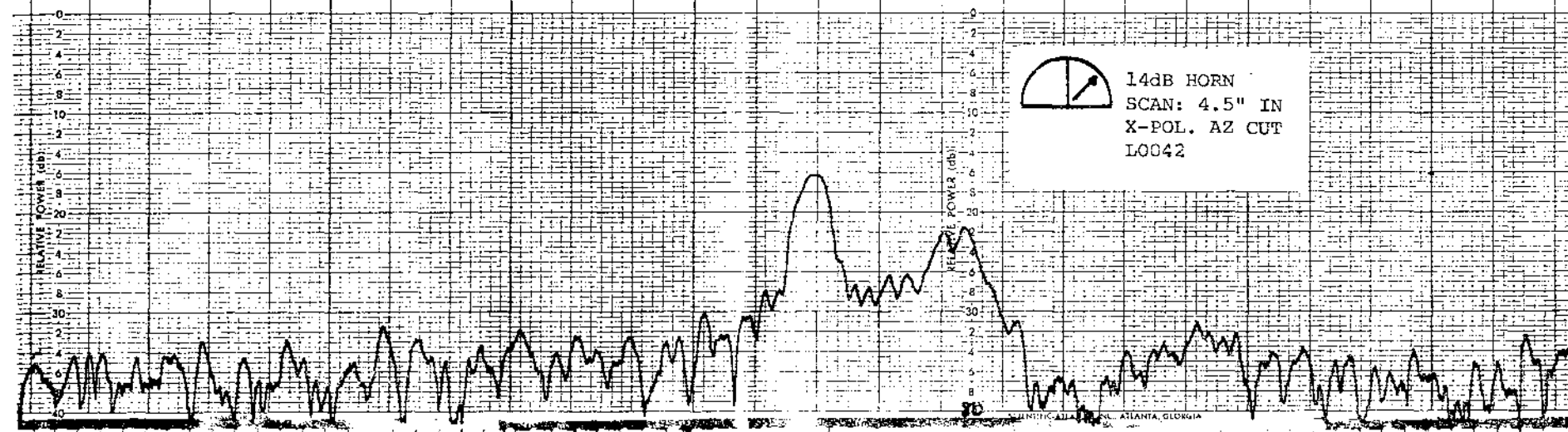
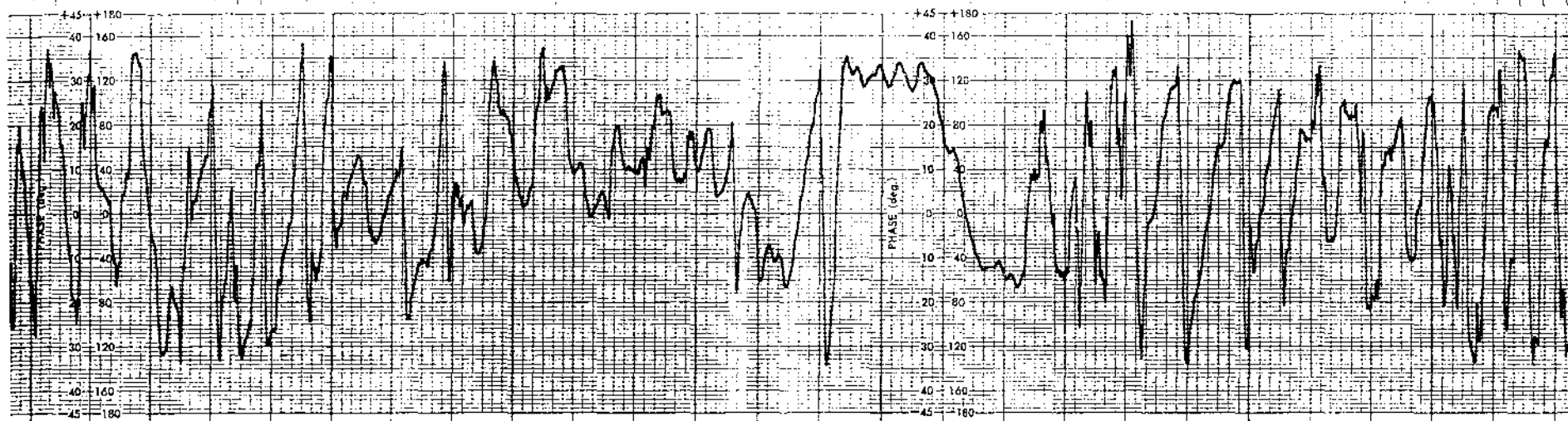




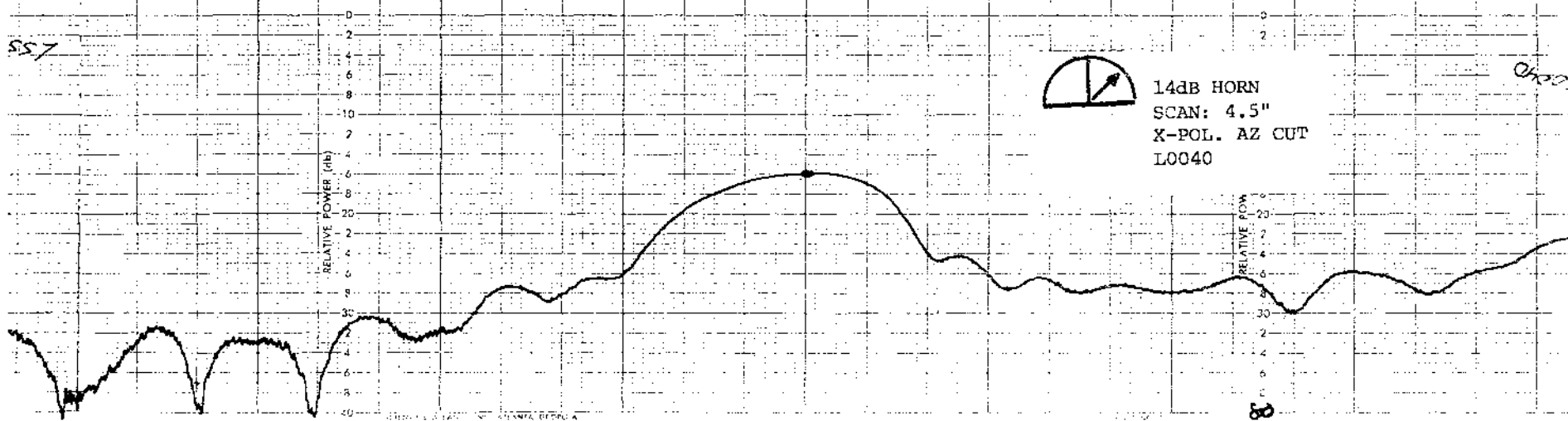
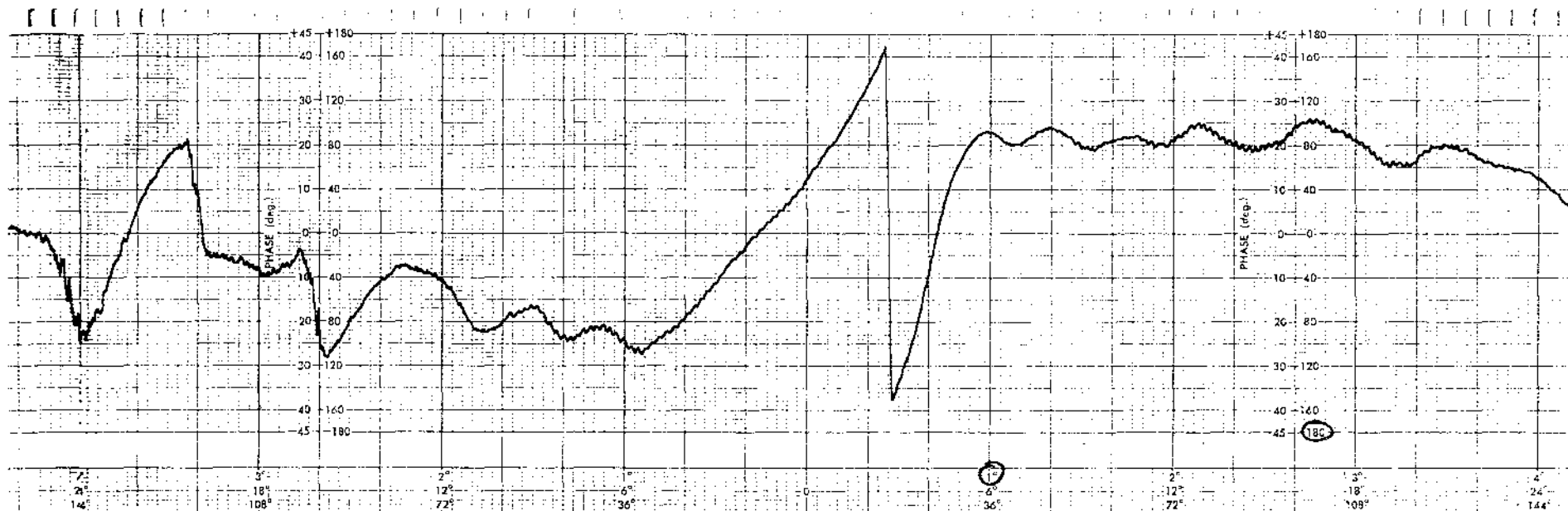


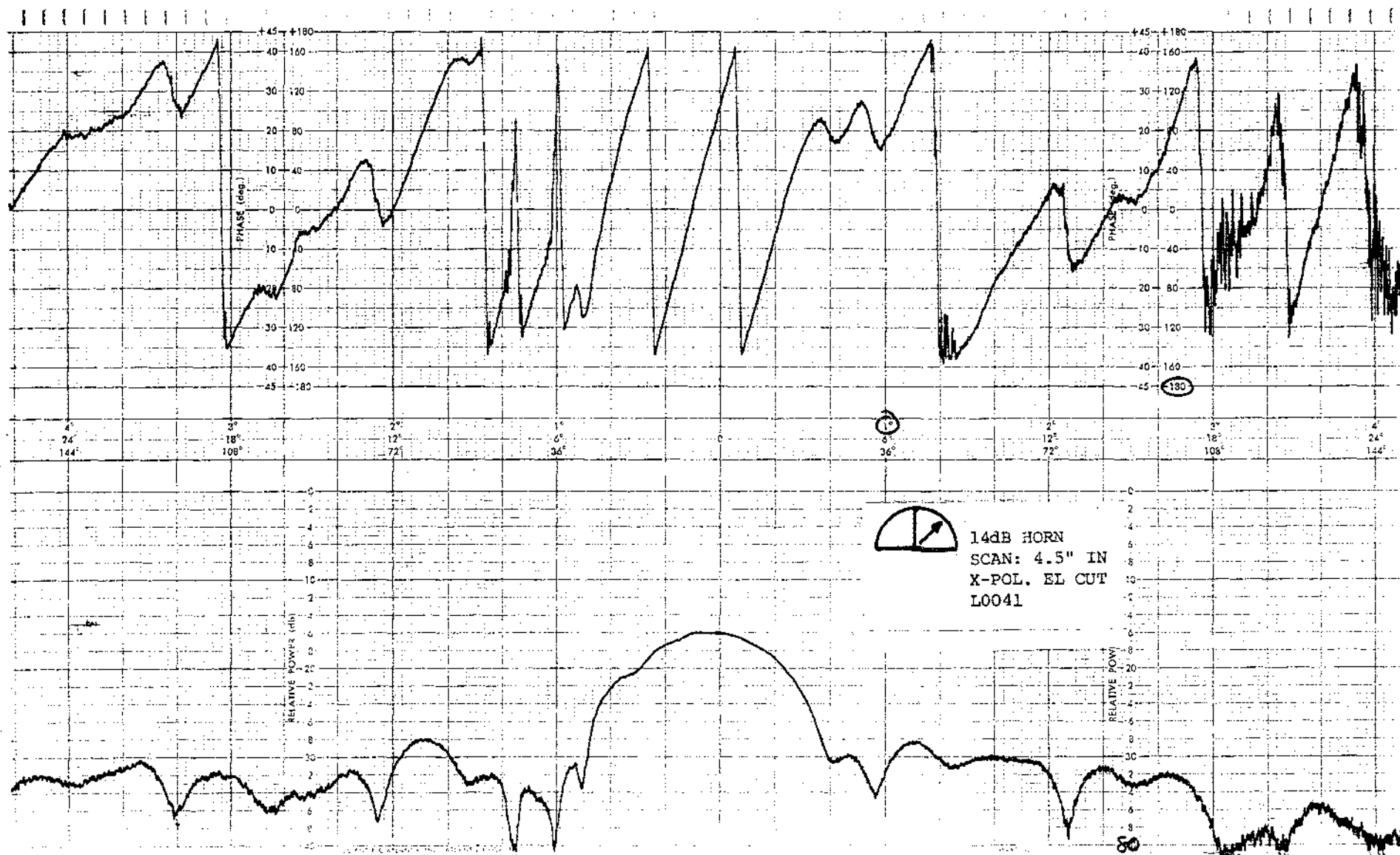


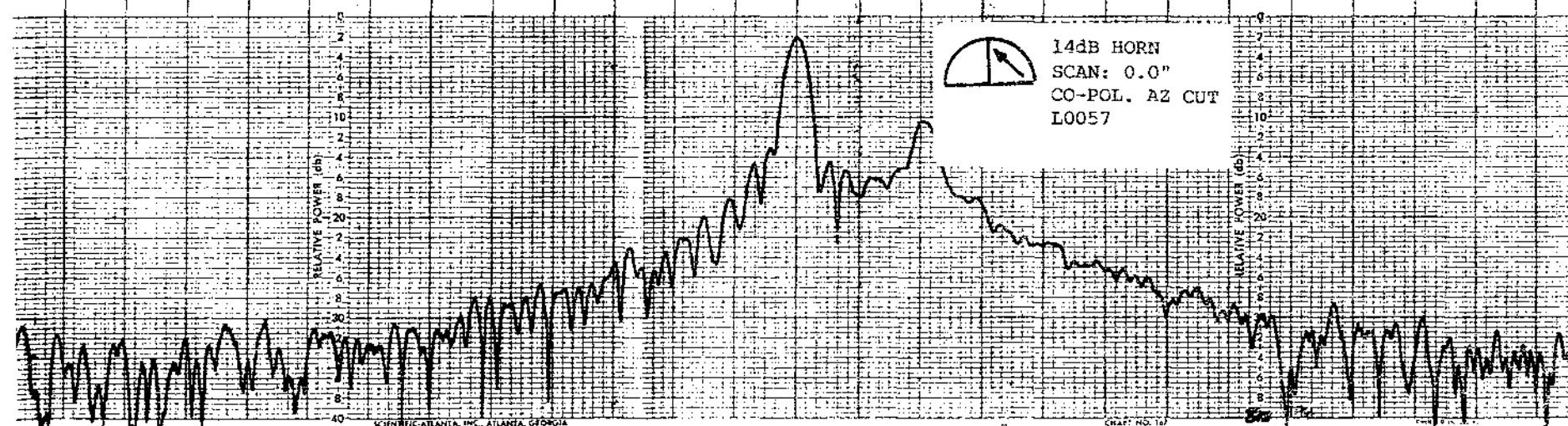
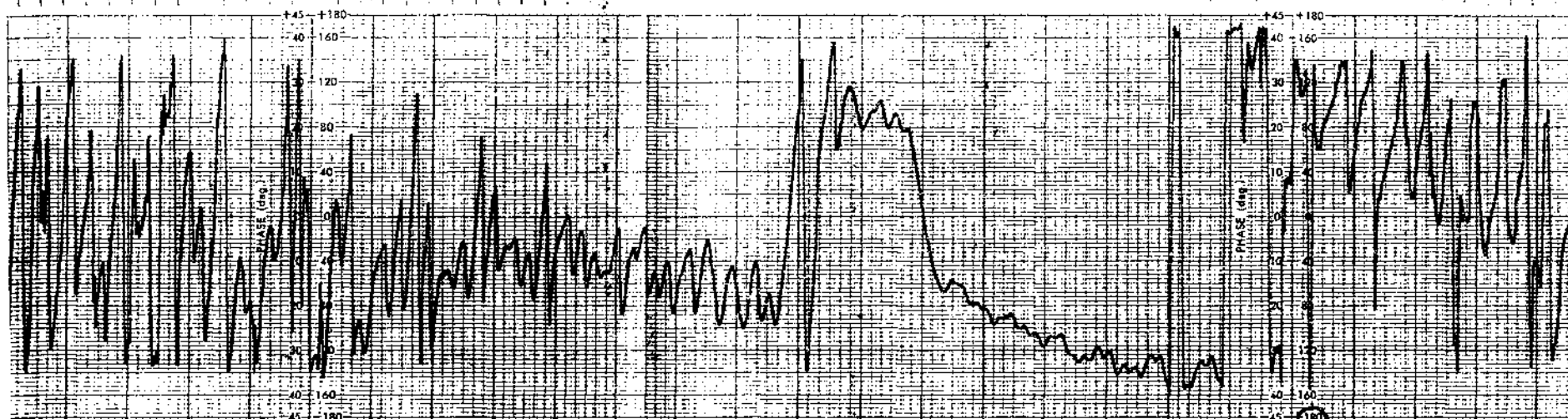








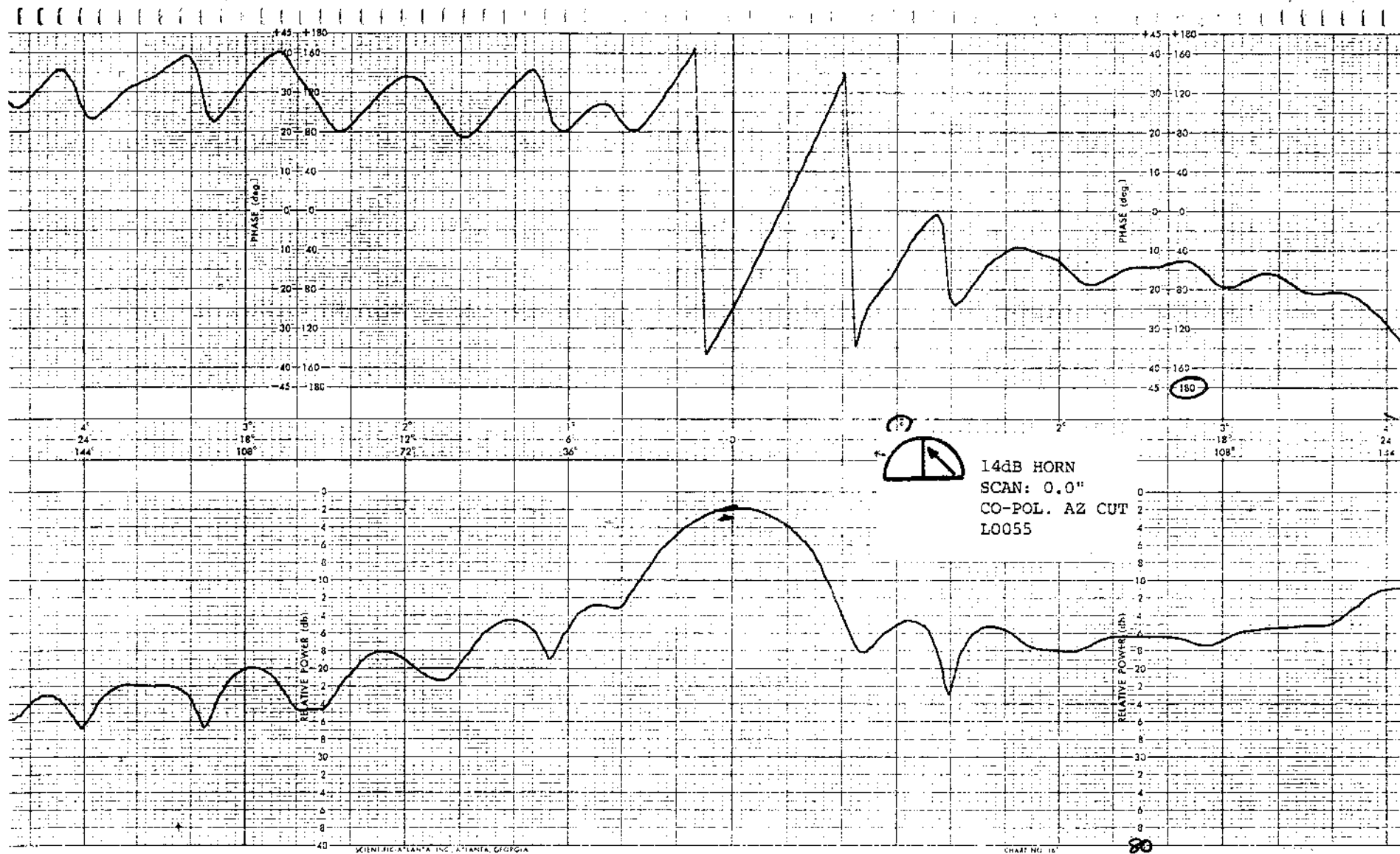


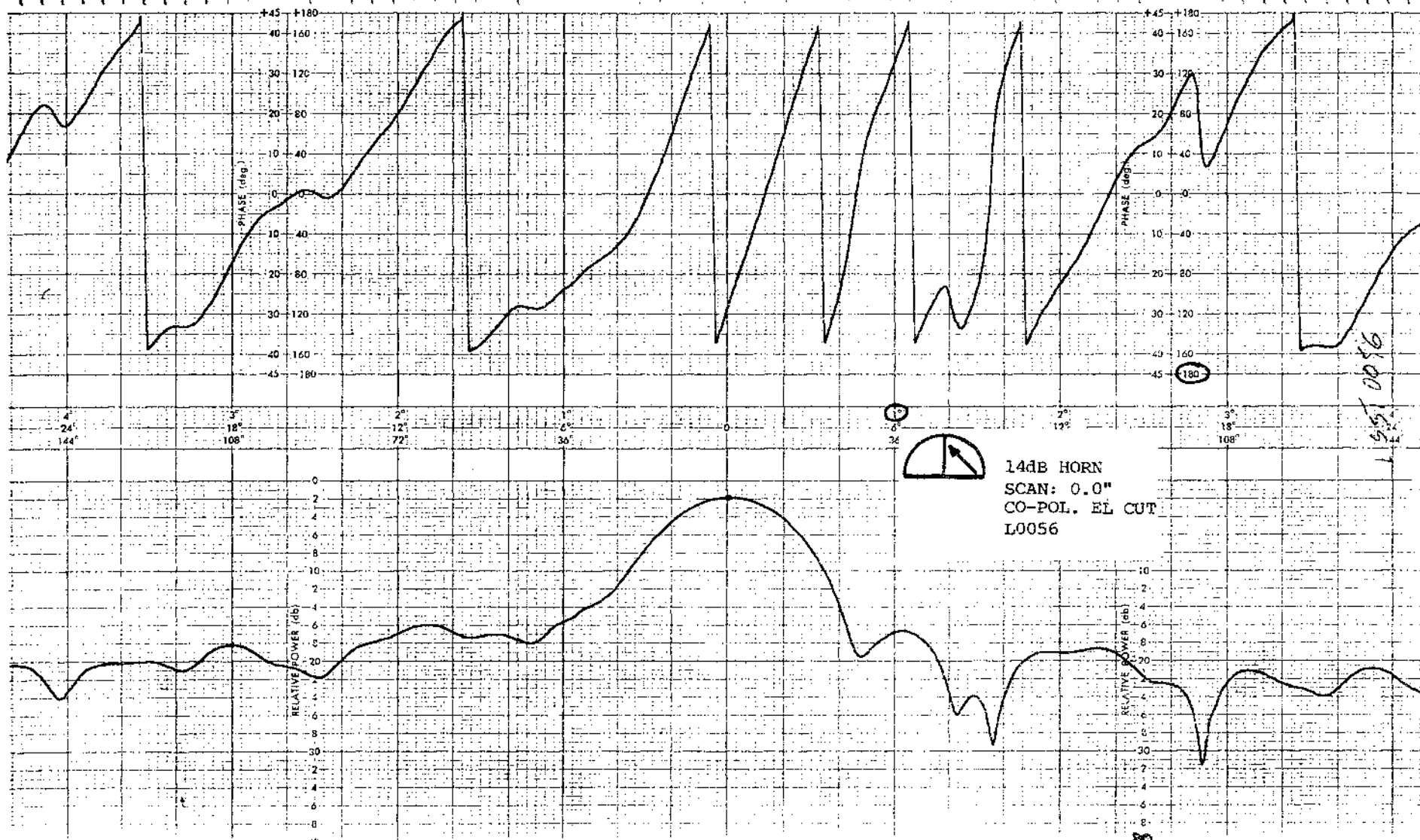


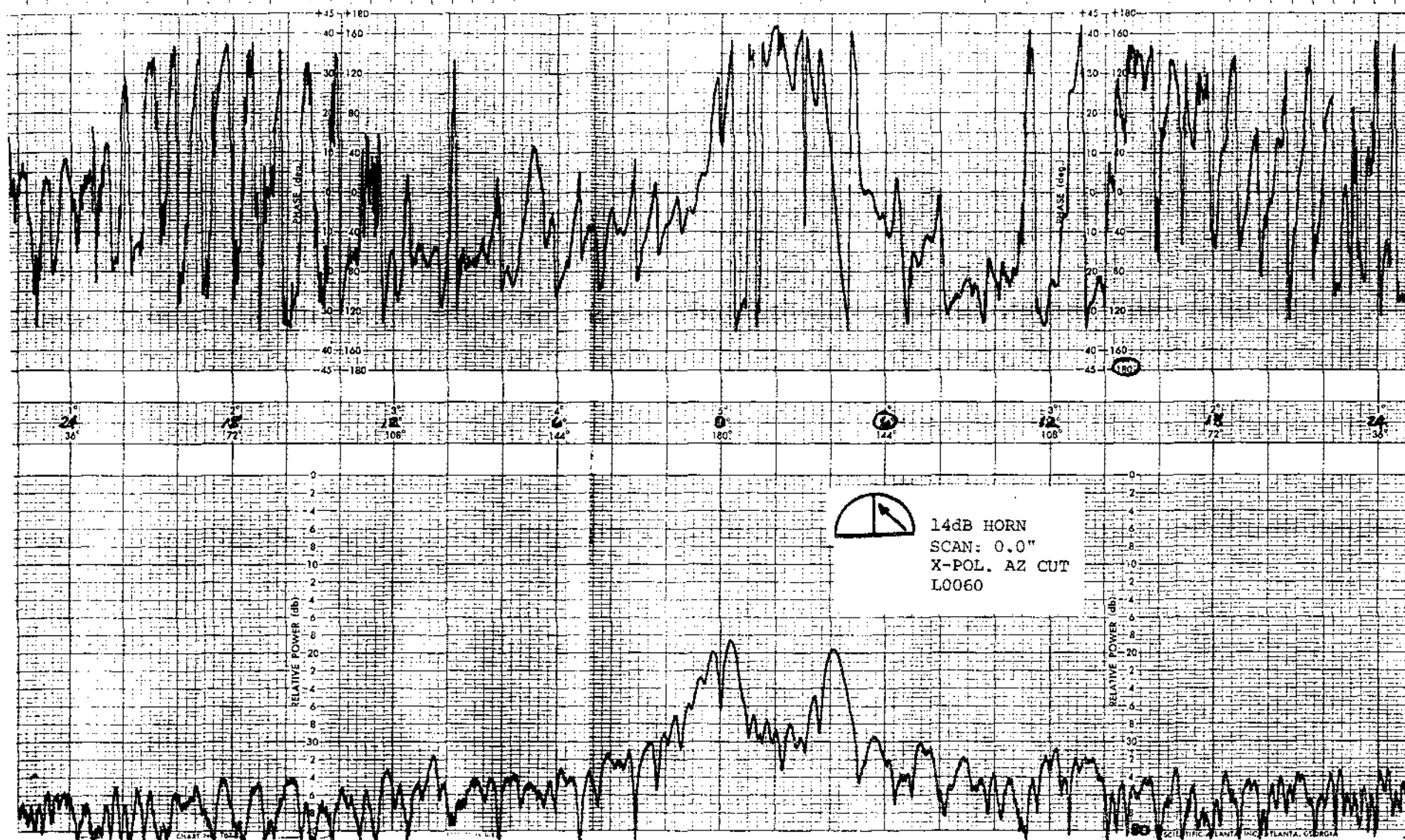
14dB HORN  
SCAN: 0.0"  
CO-POL. AZ CUT  
L0057

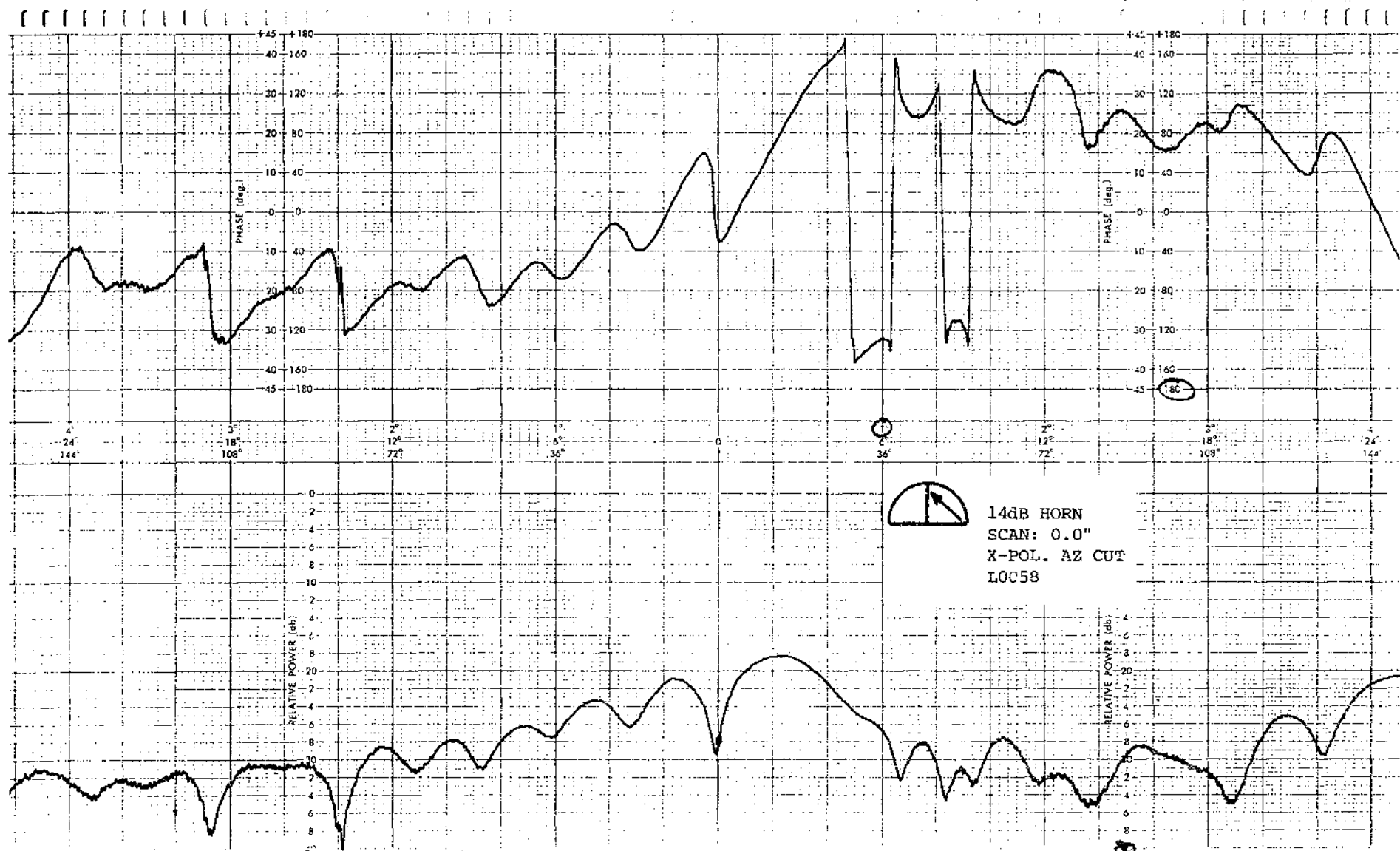
KIDNITE/ATLANTA, INC. ATLANTA, GEORGIA

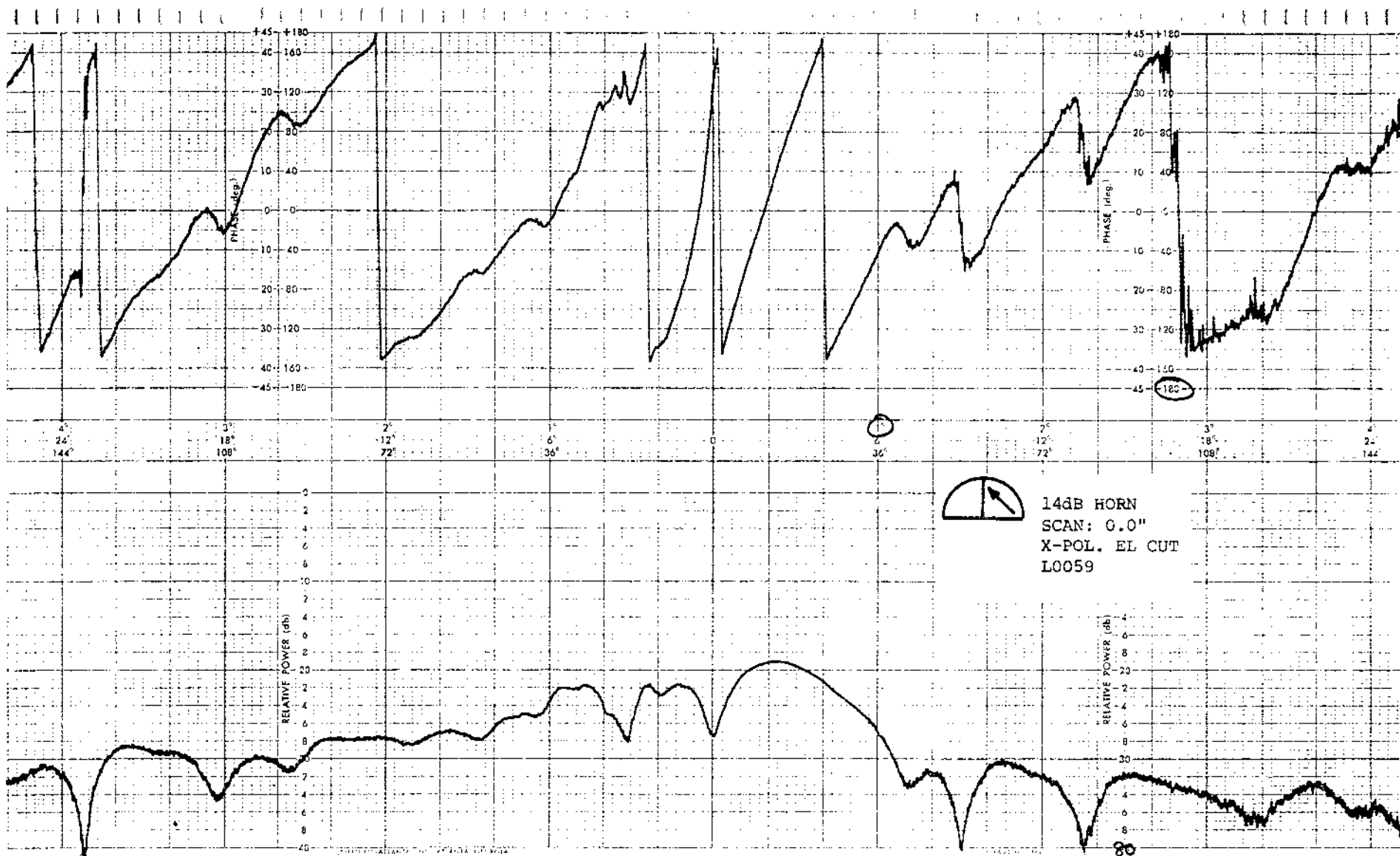
CHART NO. 16





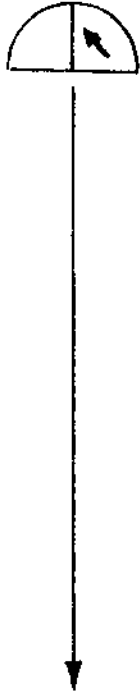
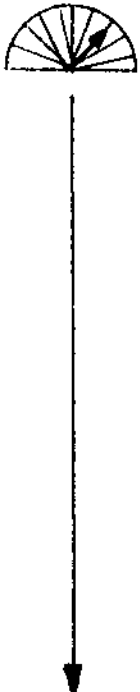


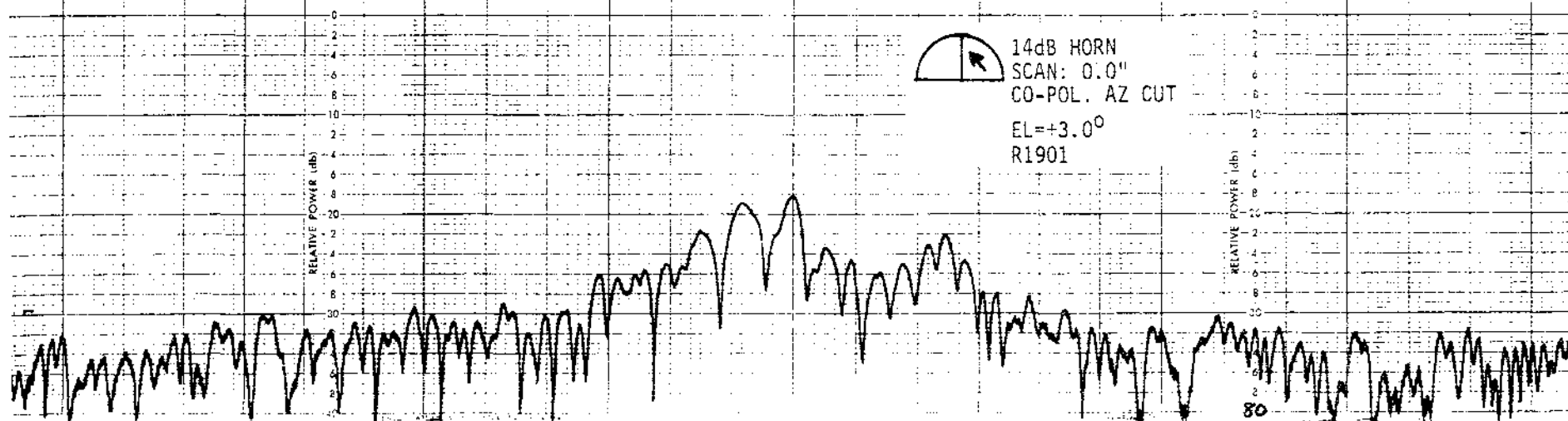
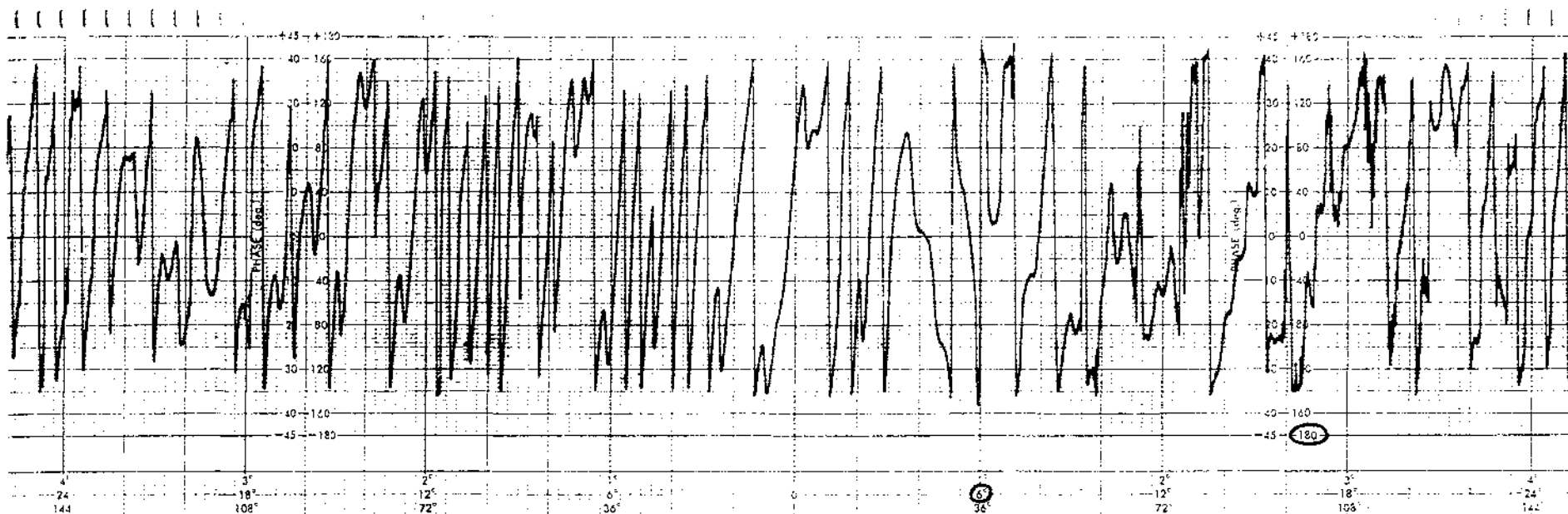




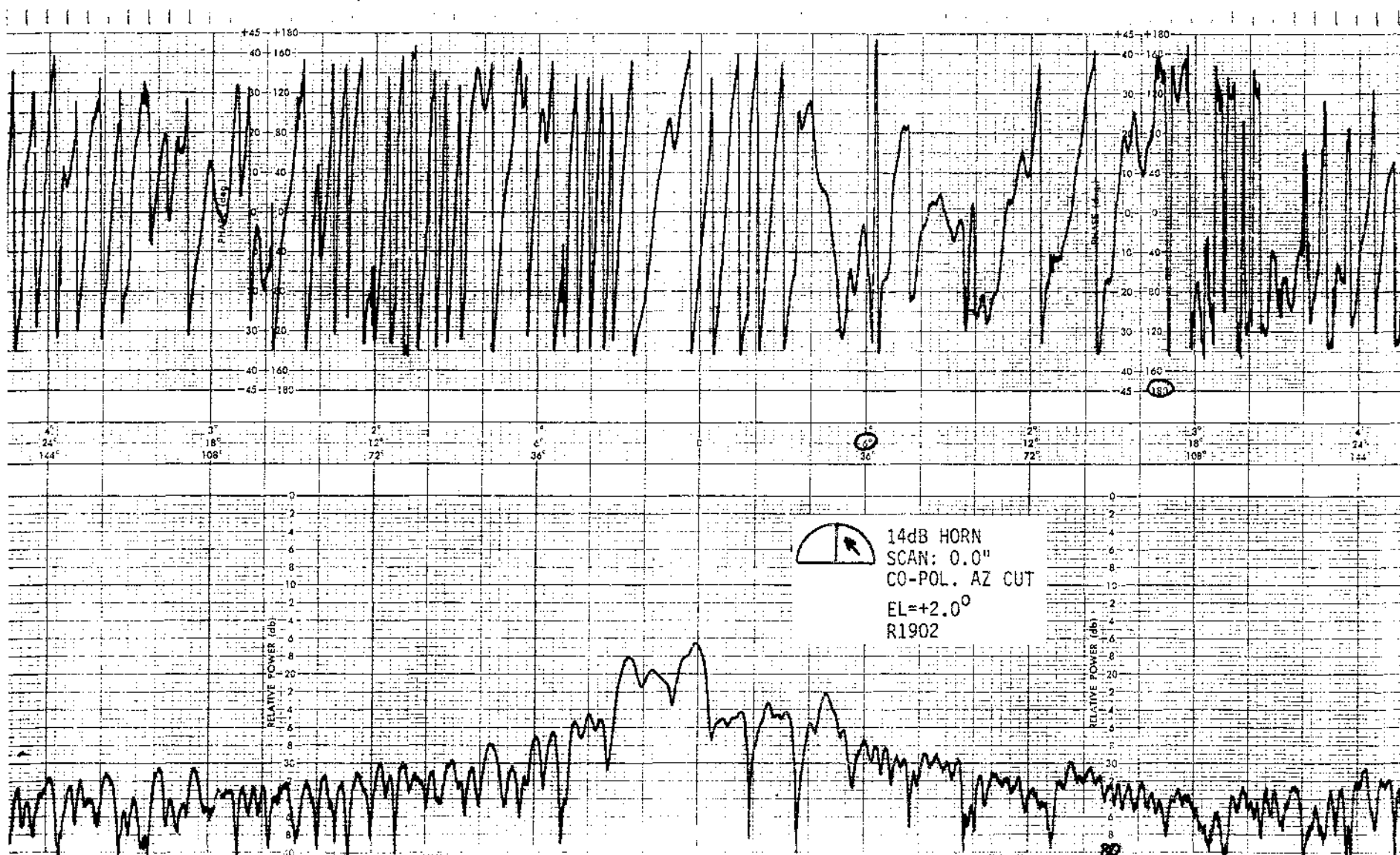


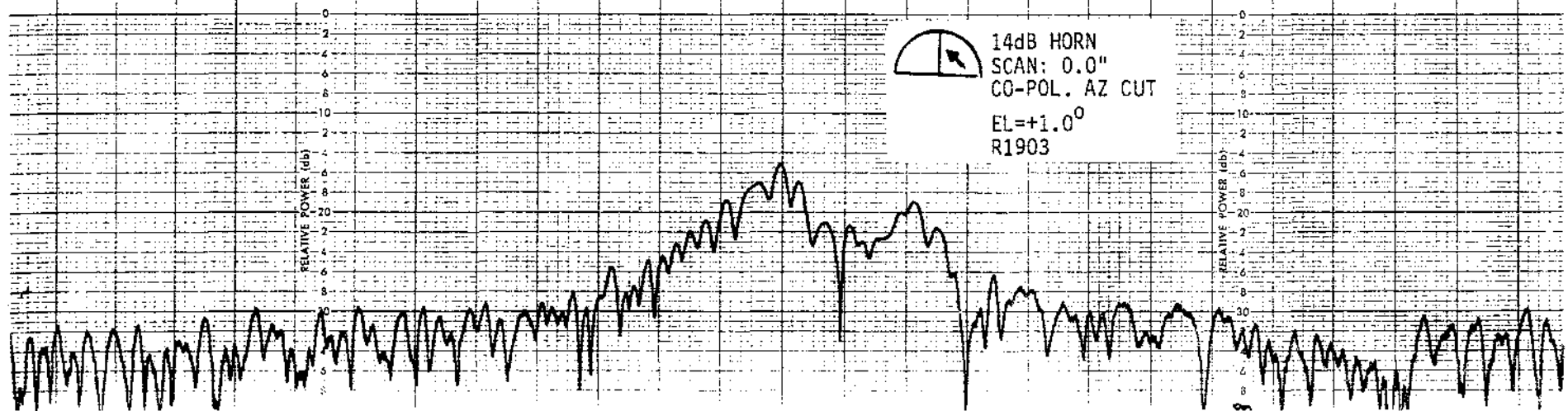
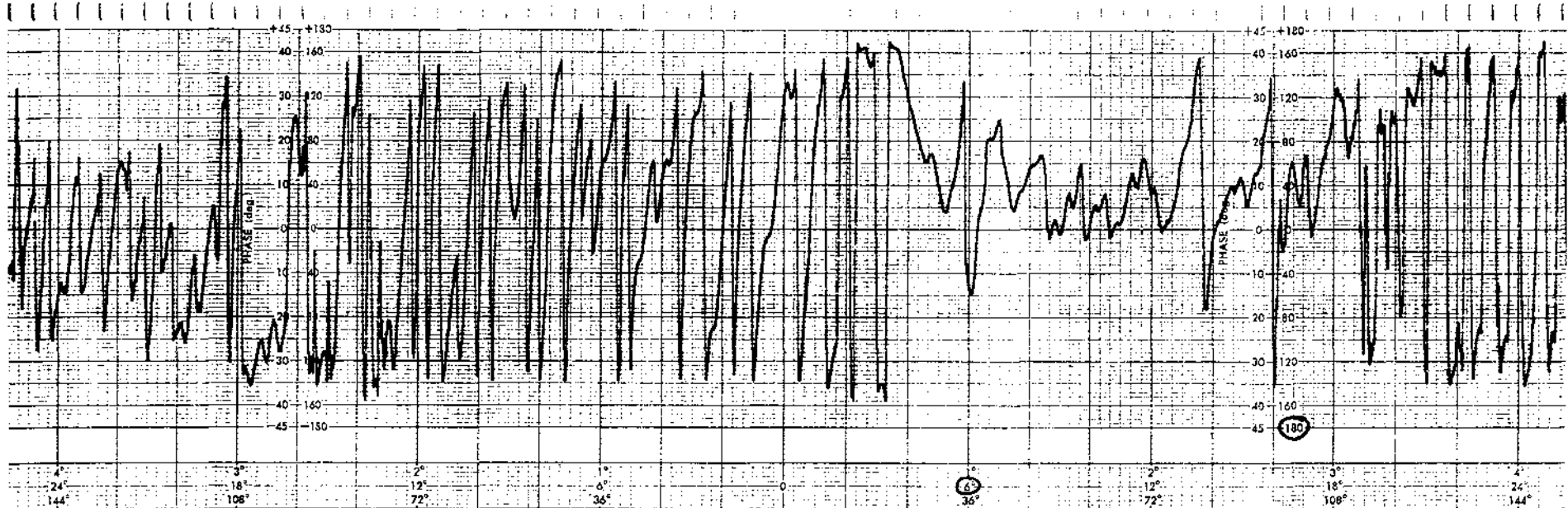
LSST - IXSECONDARY PATTERN LOG

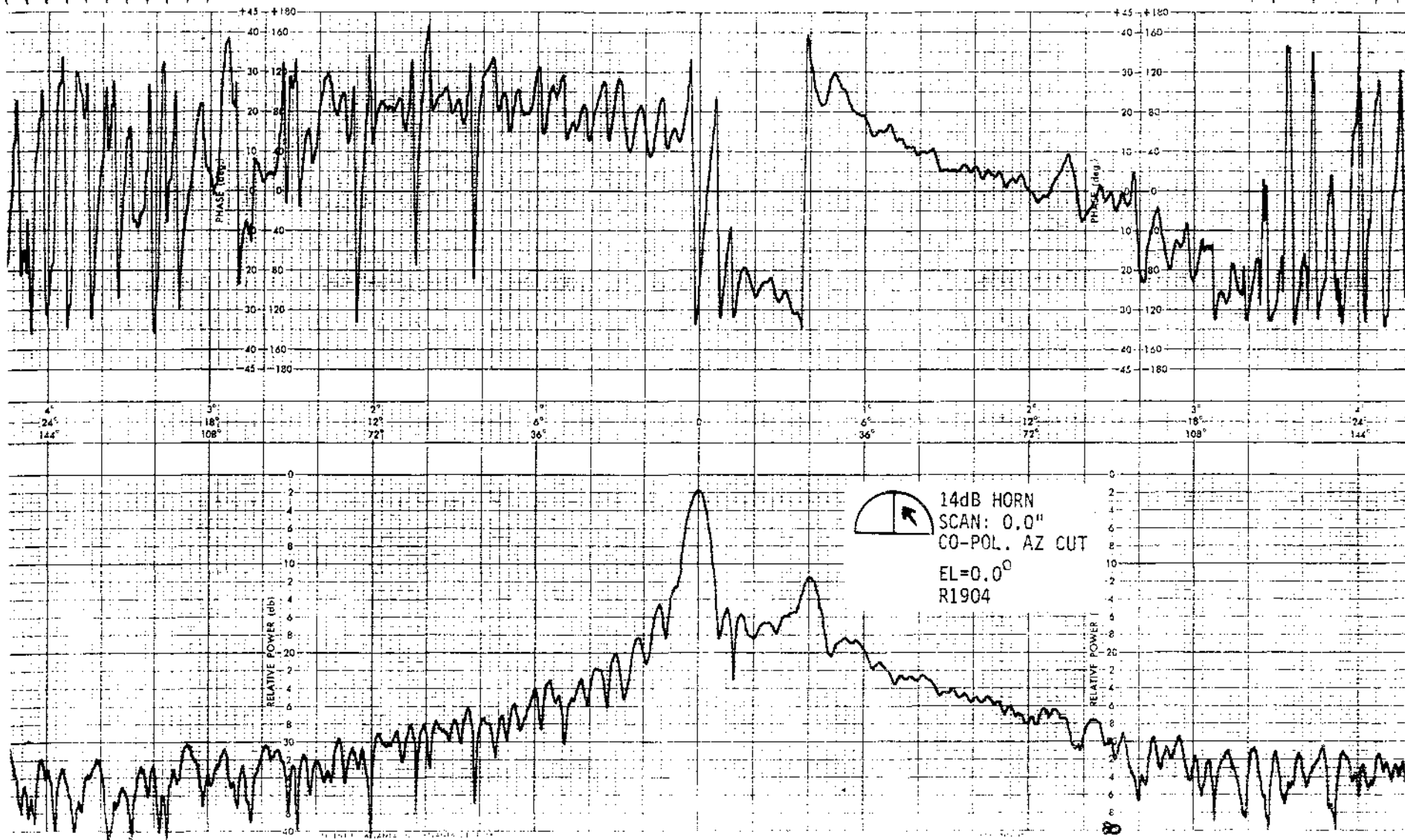
<u>CONFIGURATION</u>	<u>HORN</u>	<u>SCAN</u>	<u>POL.</u>	<u>PK. GAIN</u>	<u>PATTERN</u>	<u>FILE NAME</u>	<u>PAGE NUMBER</u>
	14 dB	0.0"	CO	-	+3°EL ± 45°AZ	R1901	279
	"	"	"	-	+2°EL "	R1902	280
	"	"	"	-	+1°EL "	R1903	281
	"	"	"	50.55	0°EL "	R1904	282
	"	"	"	-	-1°EL "	R1905	283
	"	"	"	-	-2°EL "	R1906	284
	"	"	"	-	-3°EL "	R1907	285
	14 dB	0.0"	X	-	+3°EL ± 45°AZ	R2001	286
	"	"	"	-	+2°EL "	R2002	287
	"	"	"	-	+1°EL "	R2003	288
	"	"	"	-	0°EL "	R2004	289
	"	"	"	-	-1°EL "	R2005	290
	"	"	"	-	-2°EL "	R2006	291
	"	"	"	-	-3°EL "	R2007	292
	14 dB	0.0"	CO	-	+3°EL ± 45°AZ	R2501	293
	"	"	"	-	+2°EL "	R2502	294
	"	"	"	-	+1°EL "	R2503	295
	"	"	"	50.35	0°EL "	R2504	296
	"	"	"	-	-1°EL "	R2505	297
	"	"	"	-	-2°EL "	R2506	298
	"	"	"	-	-3°EL "	R2507	299
	14 dB	0.0"	X	-	+3°EL ± 45°AZ	R2601	300
	"	"	"	-	+2°EL "	R2602	301
	"	"	"	-	+1°EL "	R2603	302
	"	"	"	-	0°EL "	R2604	303
	"	"	"	-	-1°EL "	R2605	304
	"	"	"	-	-2°EL "	R2606	305
	"	"	"	-	-3°EL "	R2607	306

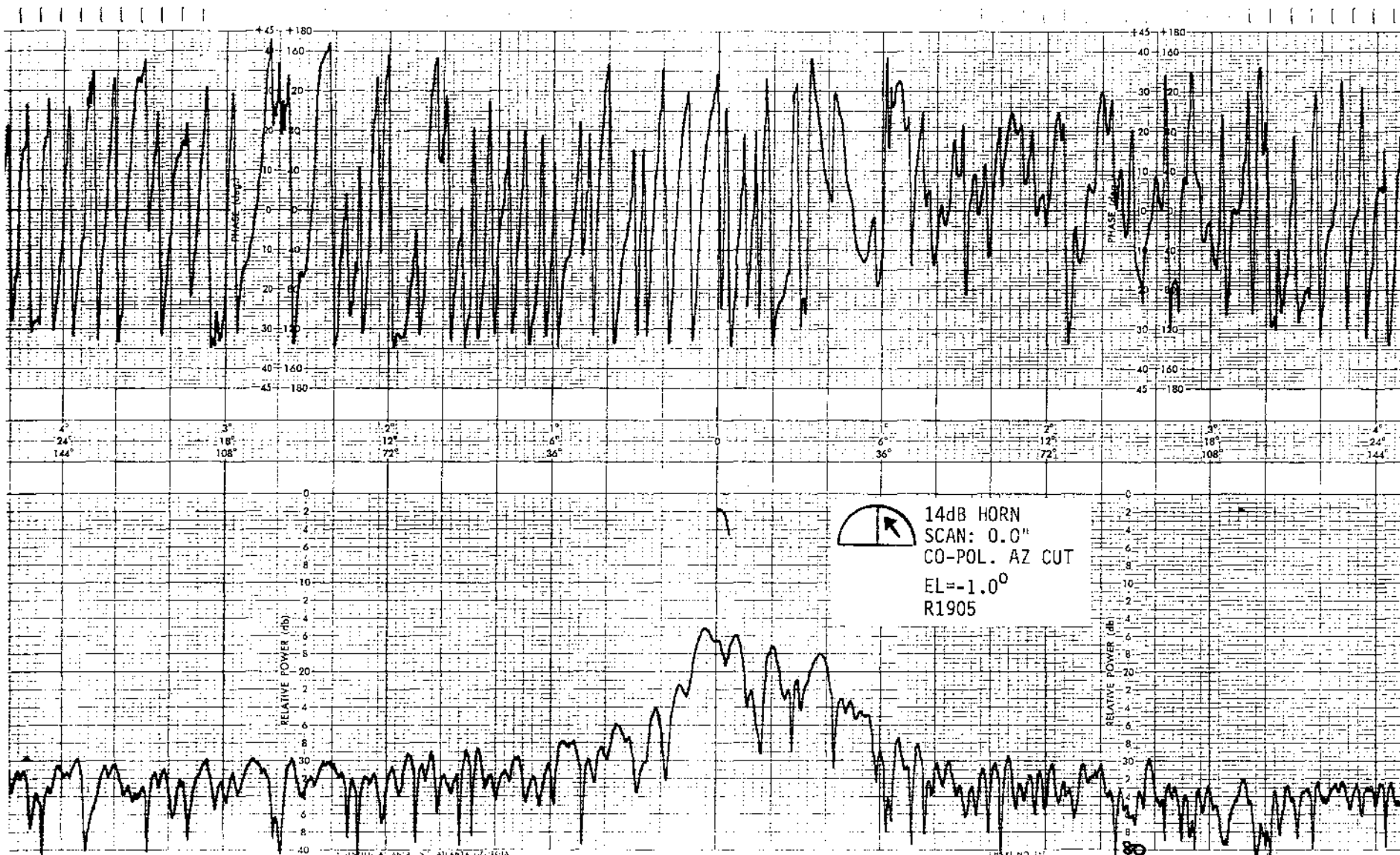


14dB HORN  
 SCAN: 0.0"  
 CO-POL. AZ CUT  
 EL=+3.0°  
 R1901

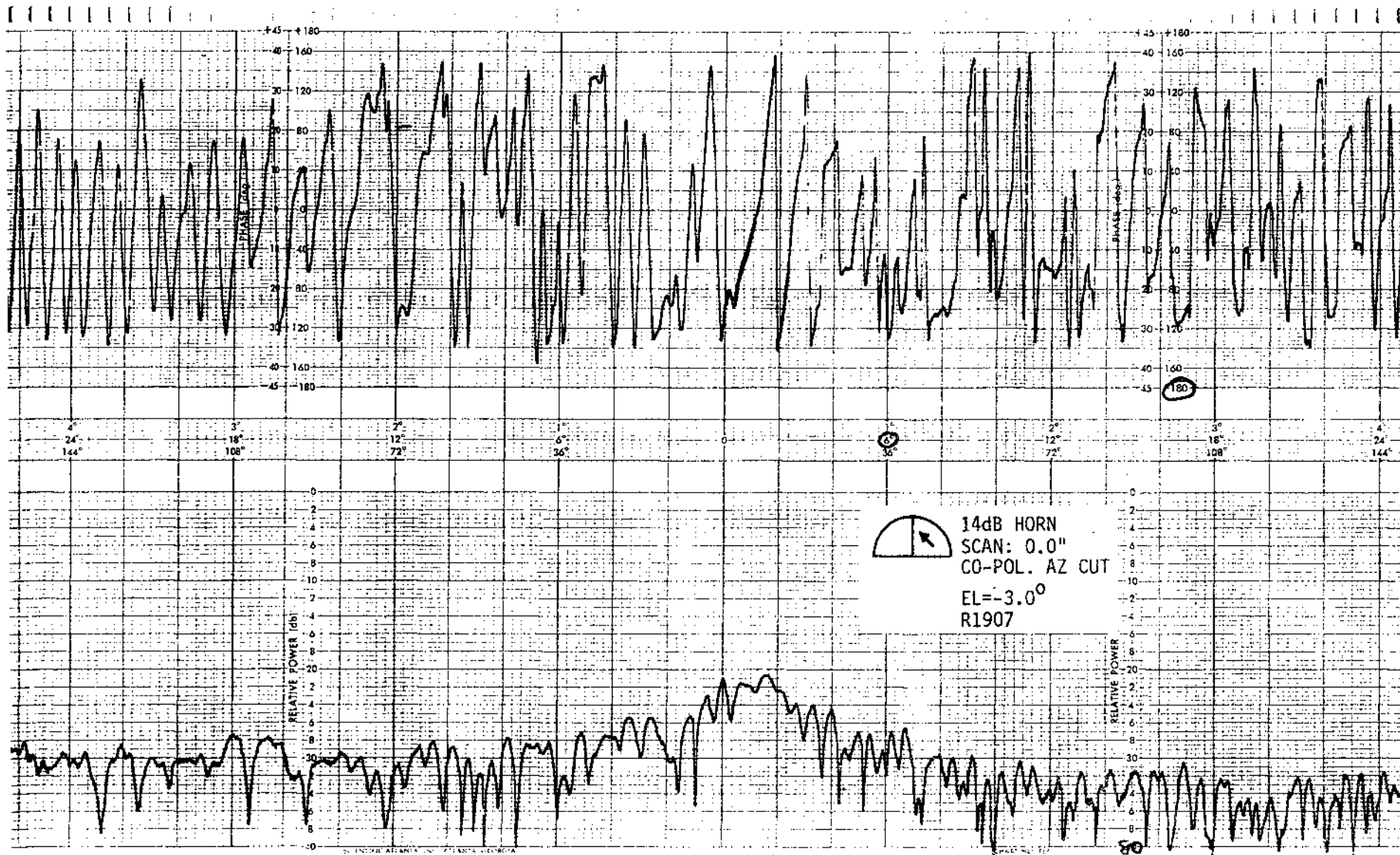




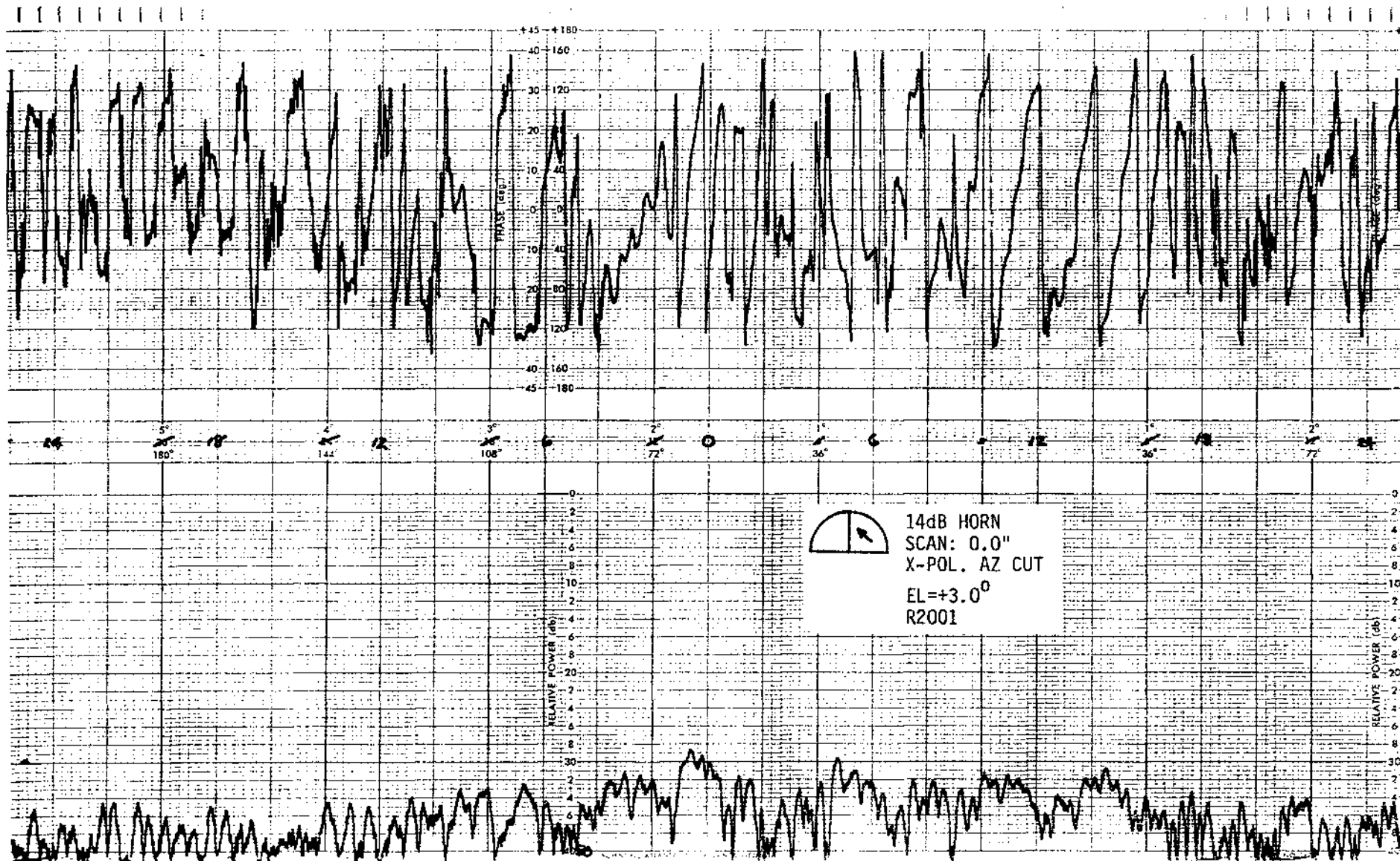


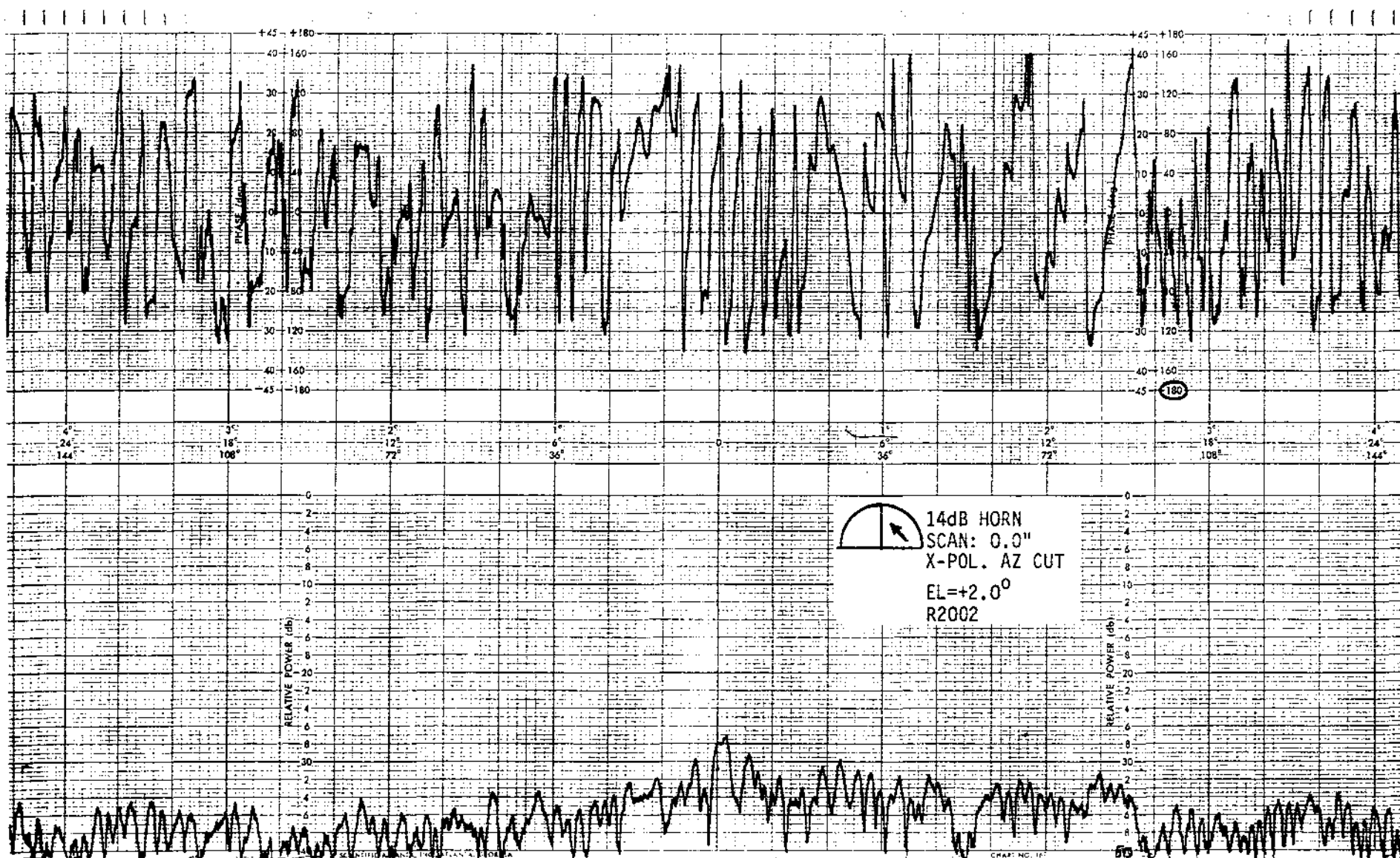


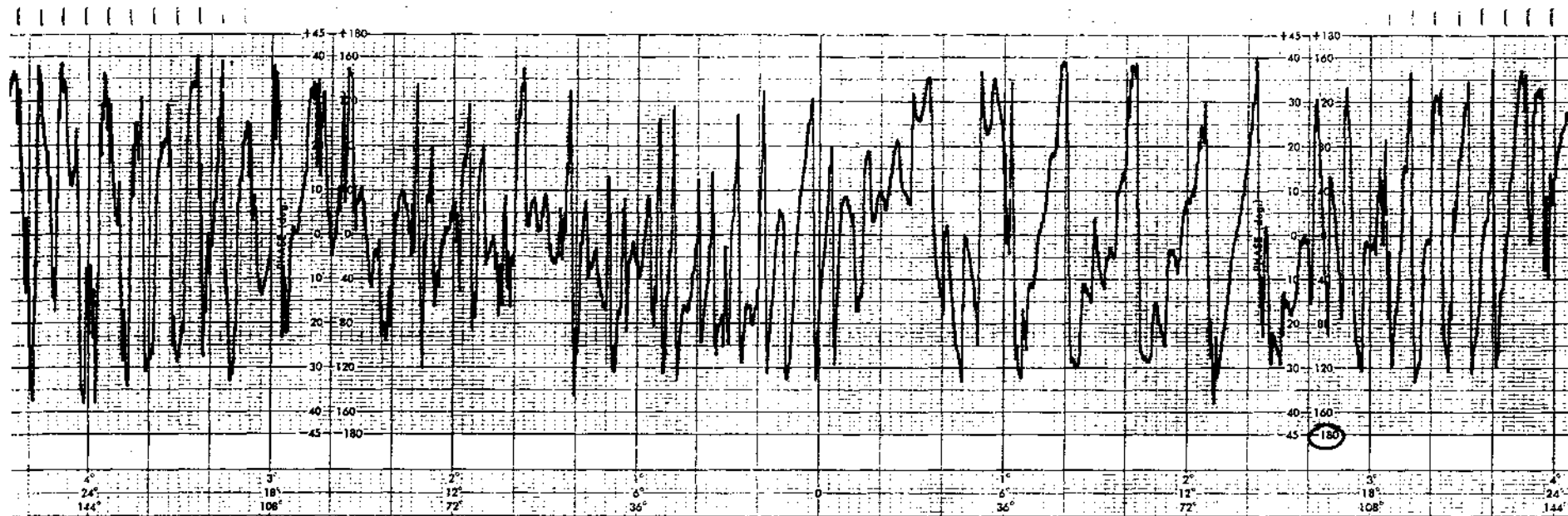




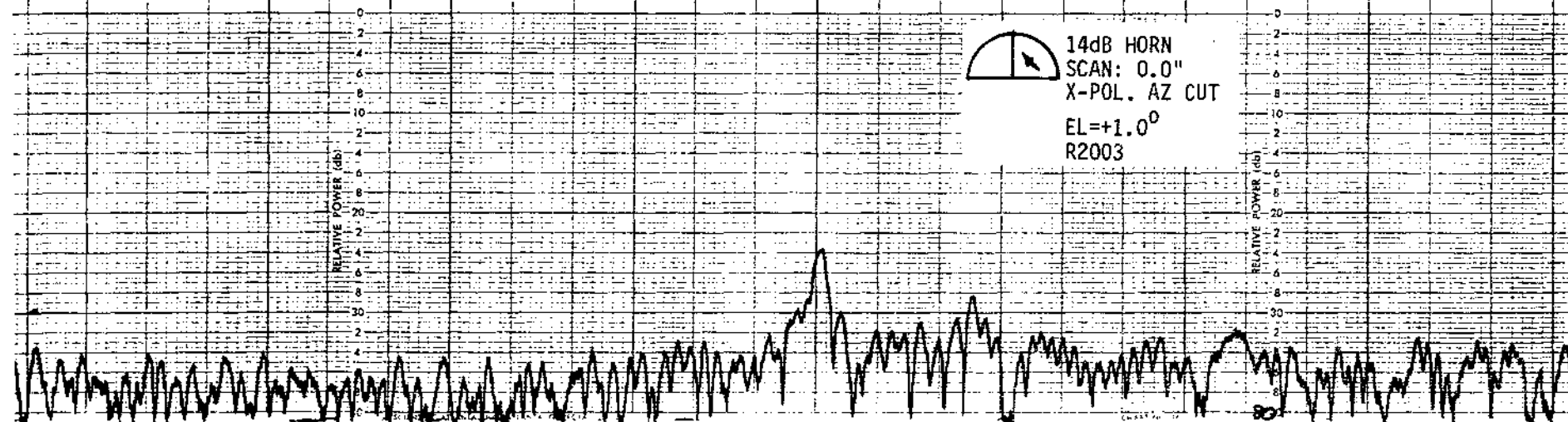




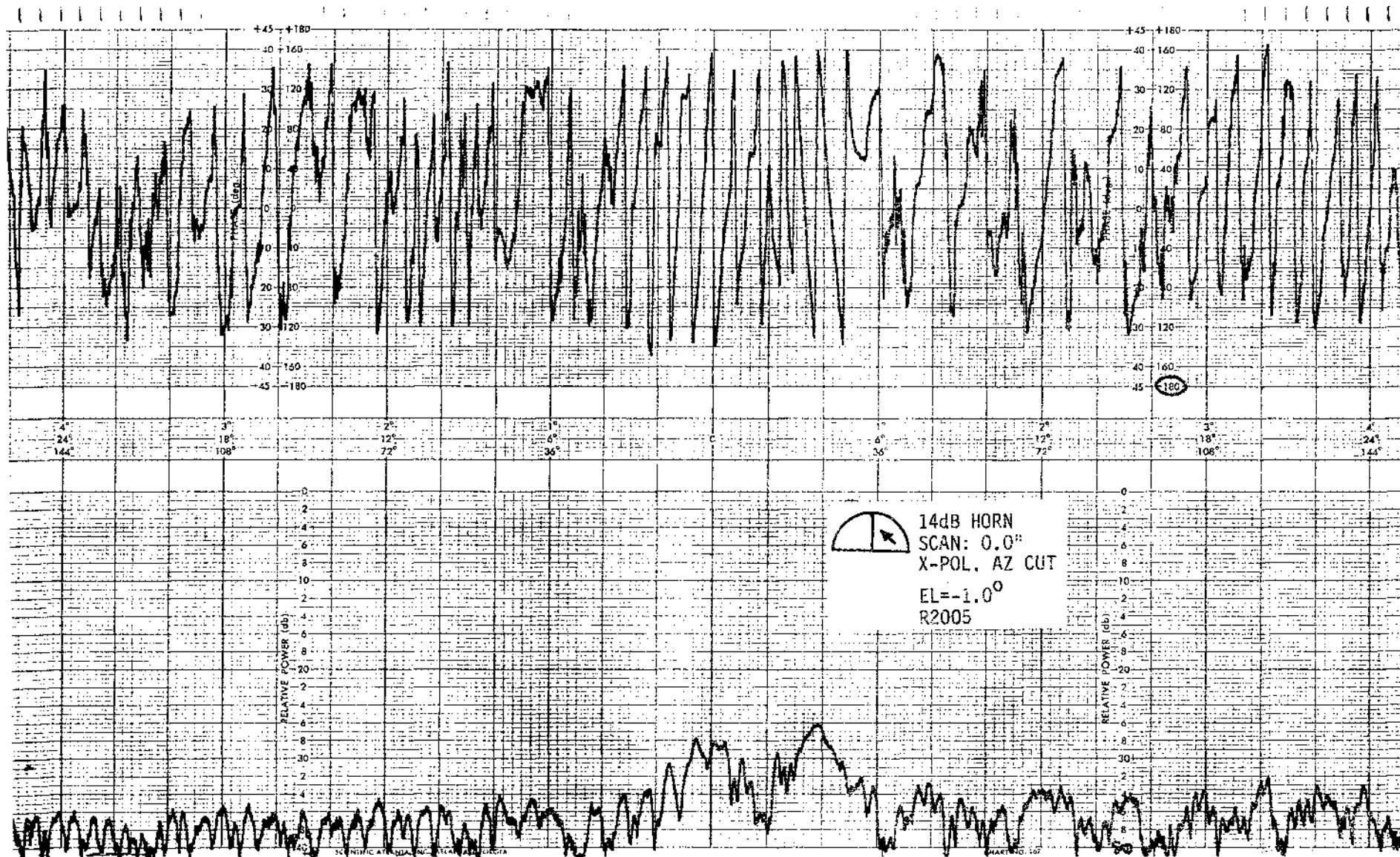


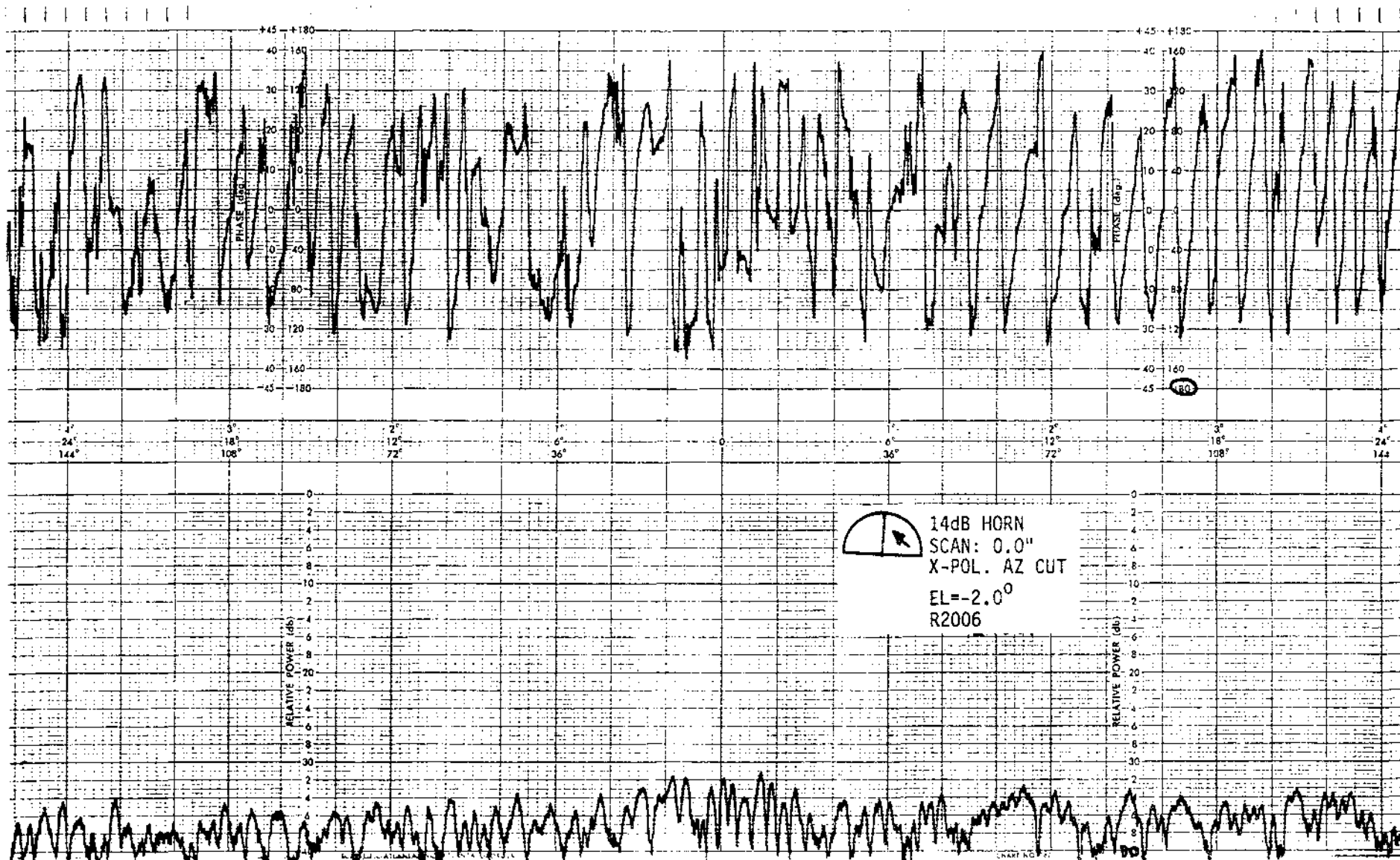


14dB HORN  
SCAN: 0.0"  
X-POL. AZ CUT  
EL=+1.0°  
R2003

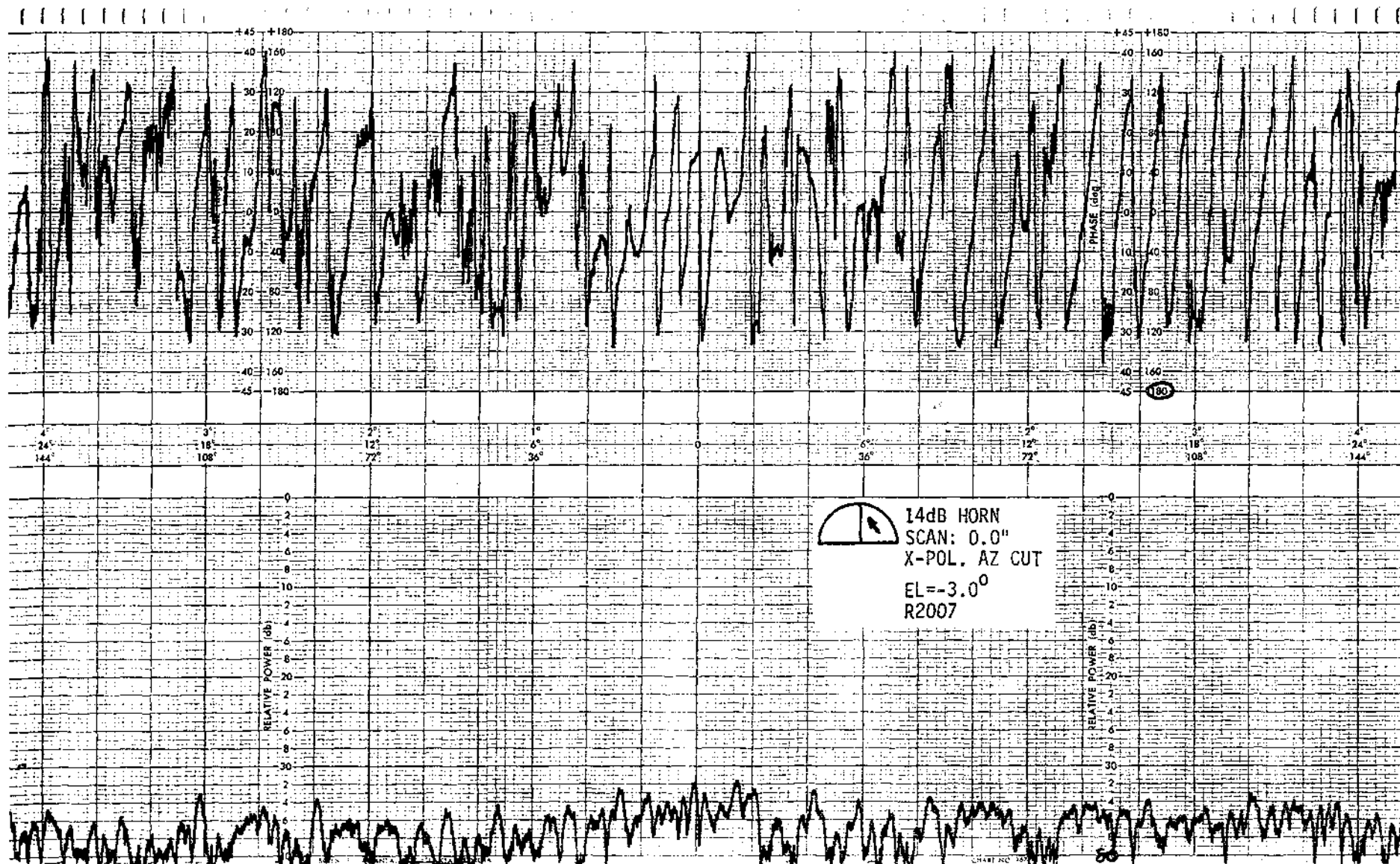






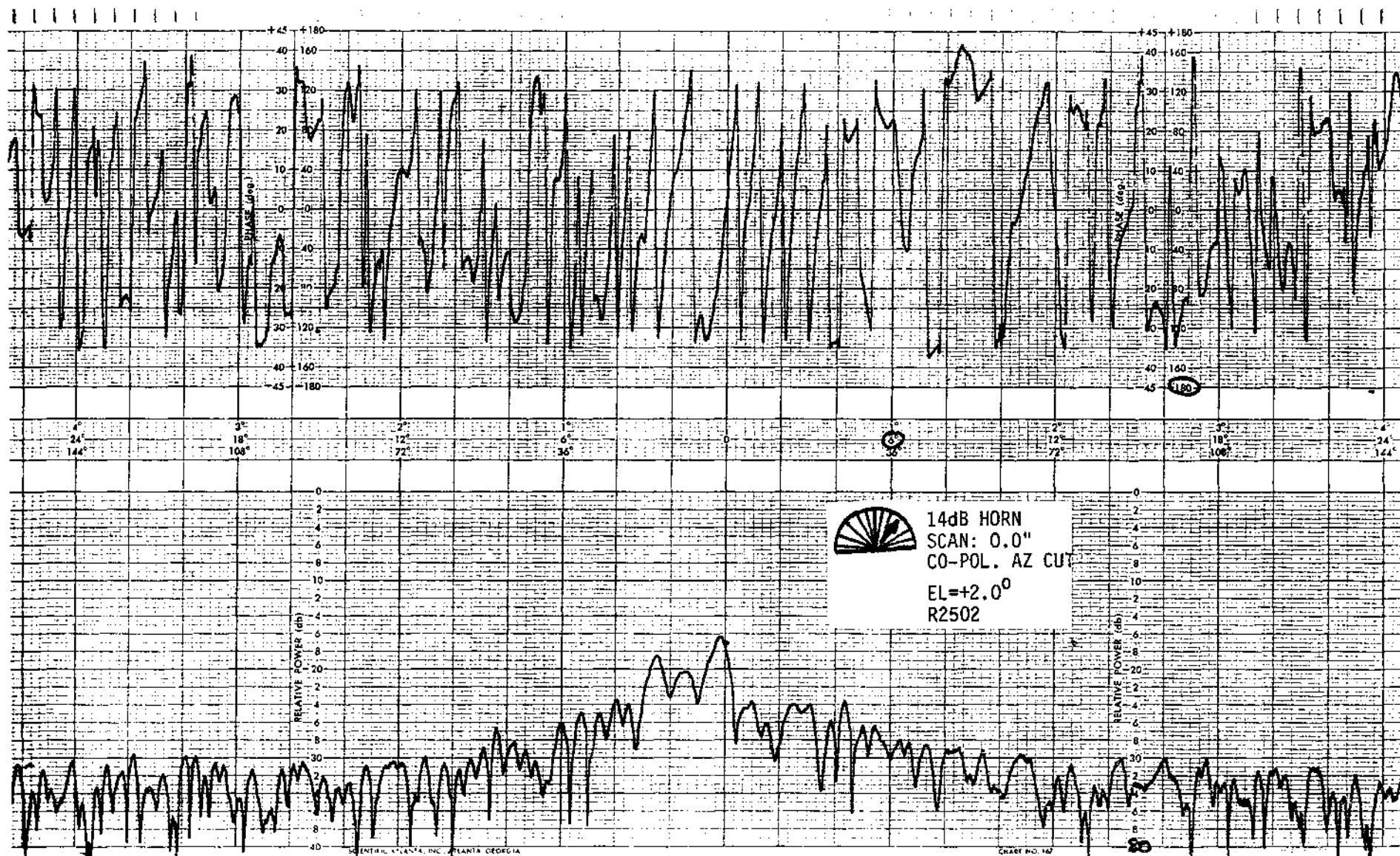


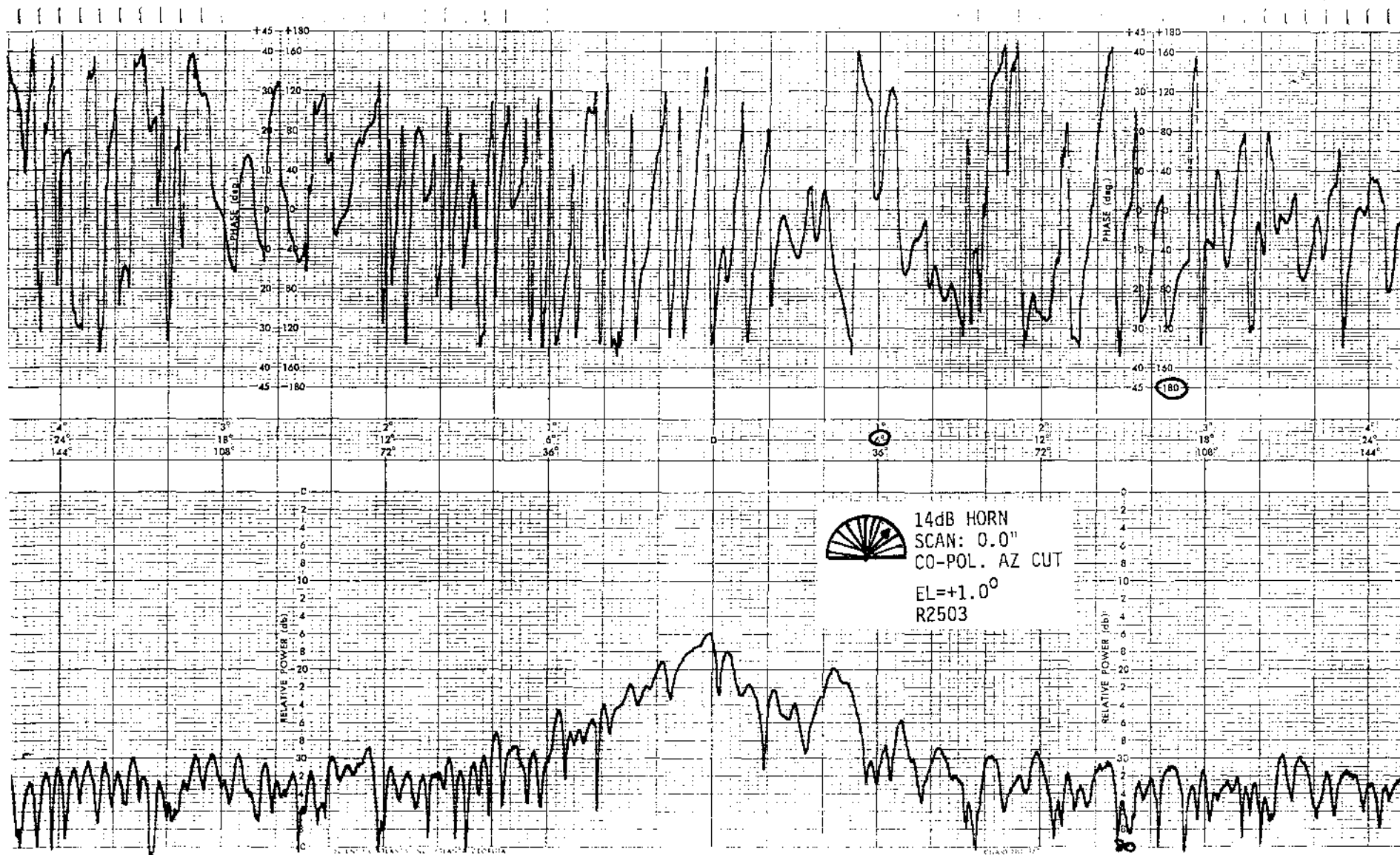


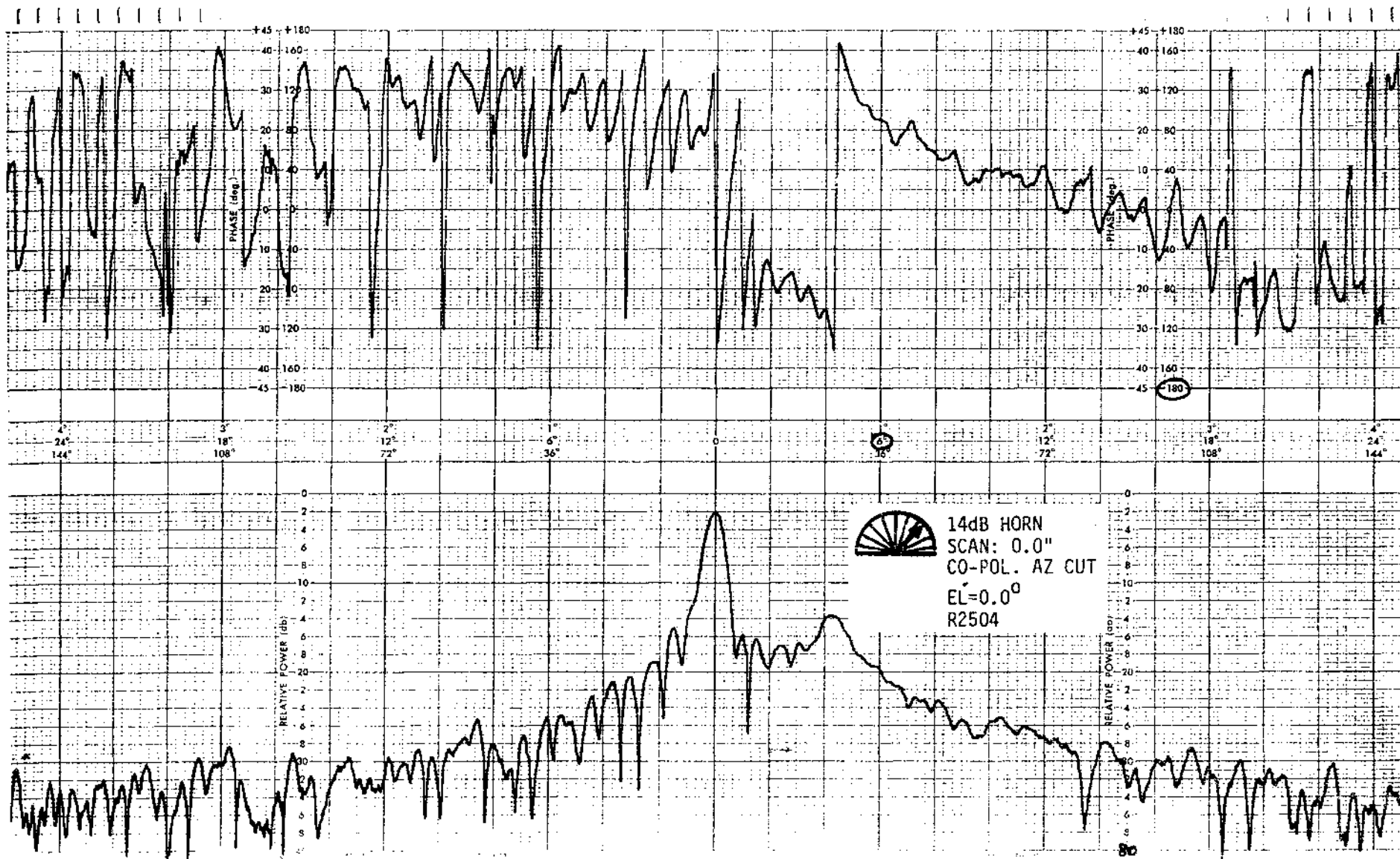


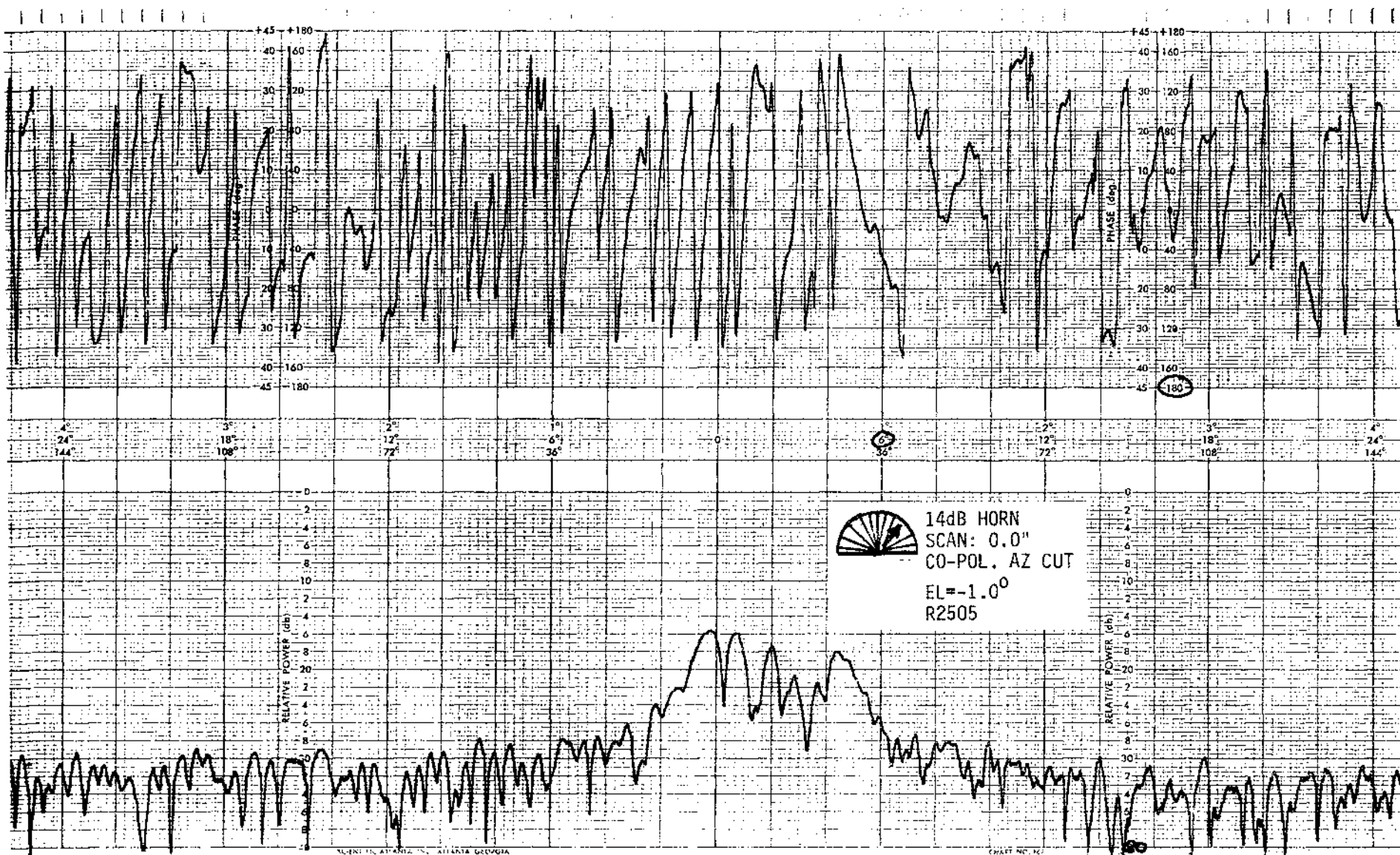


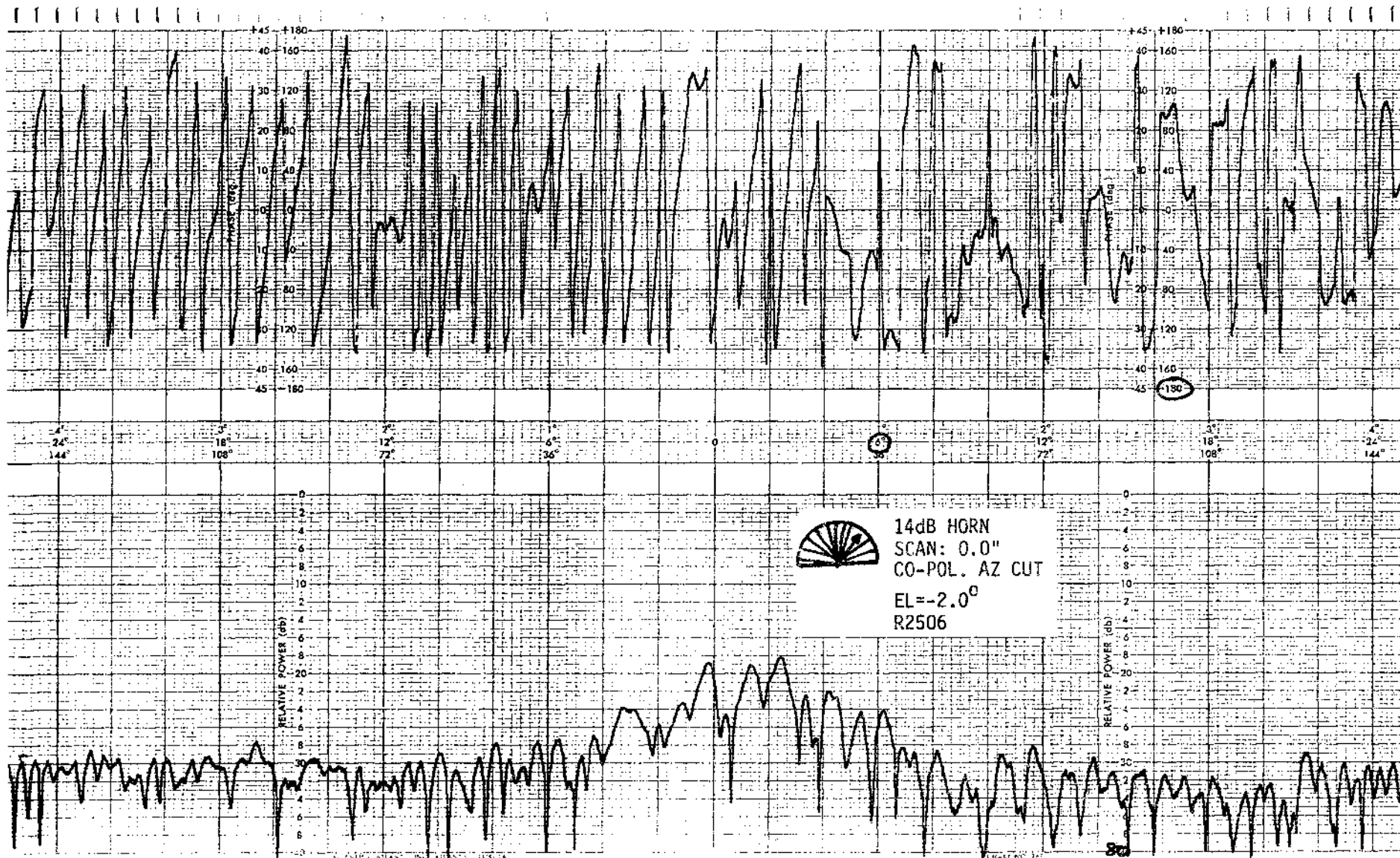


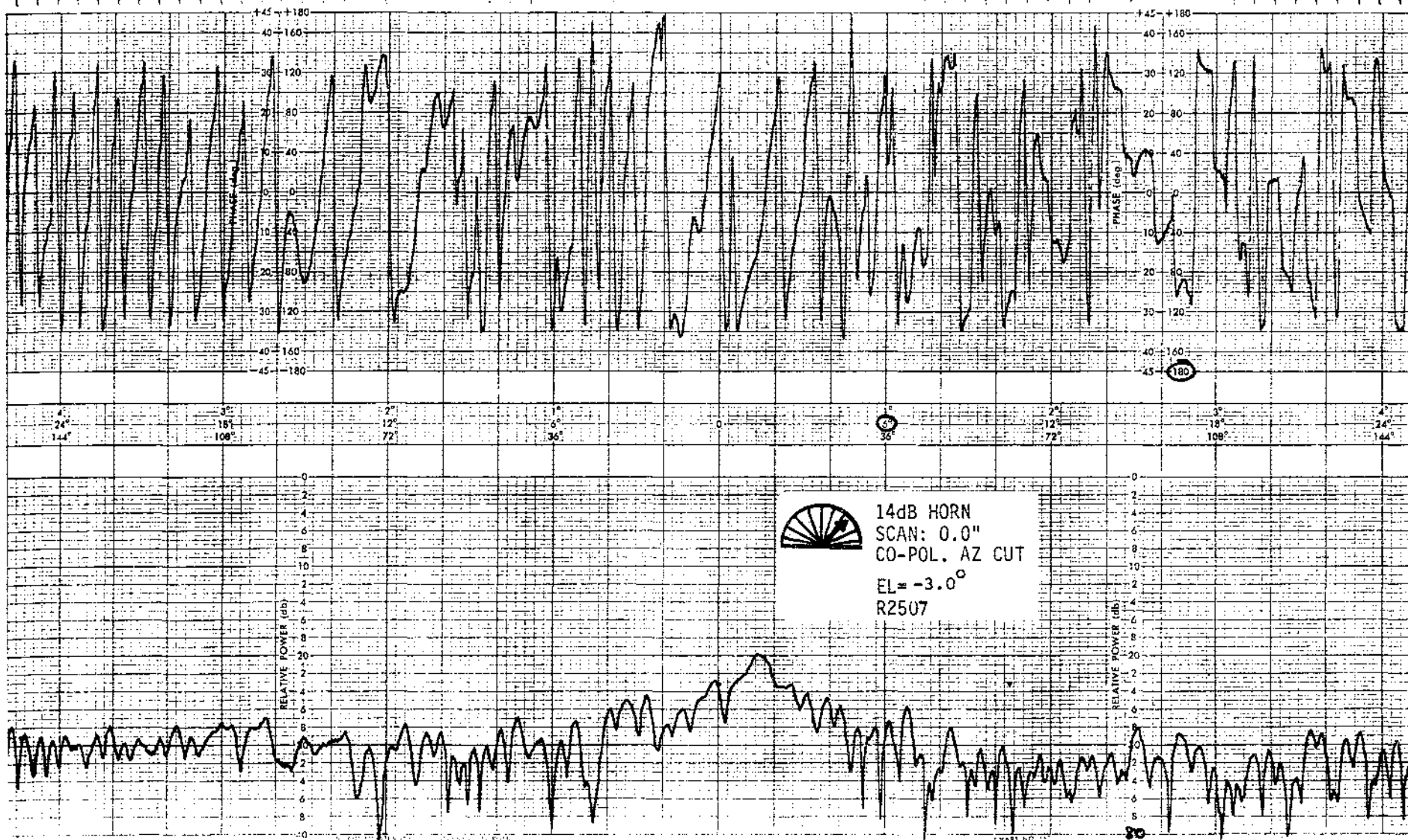






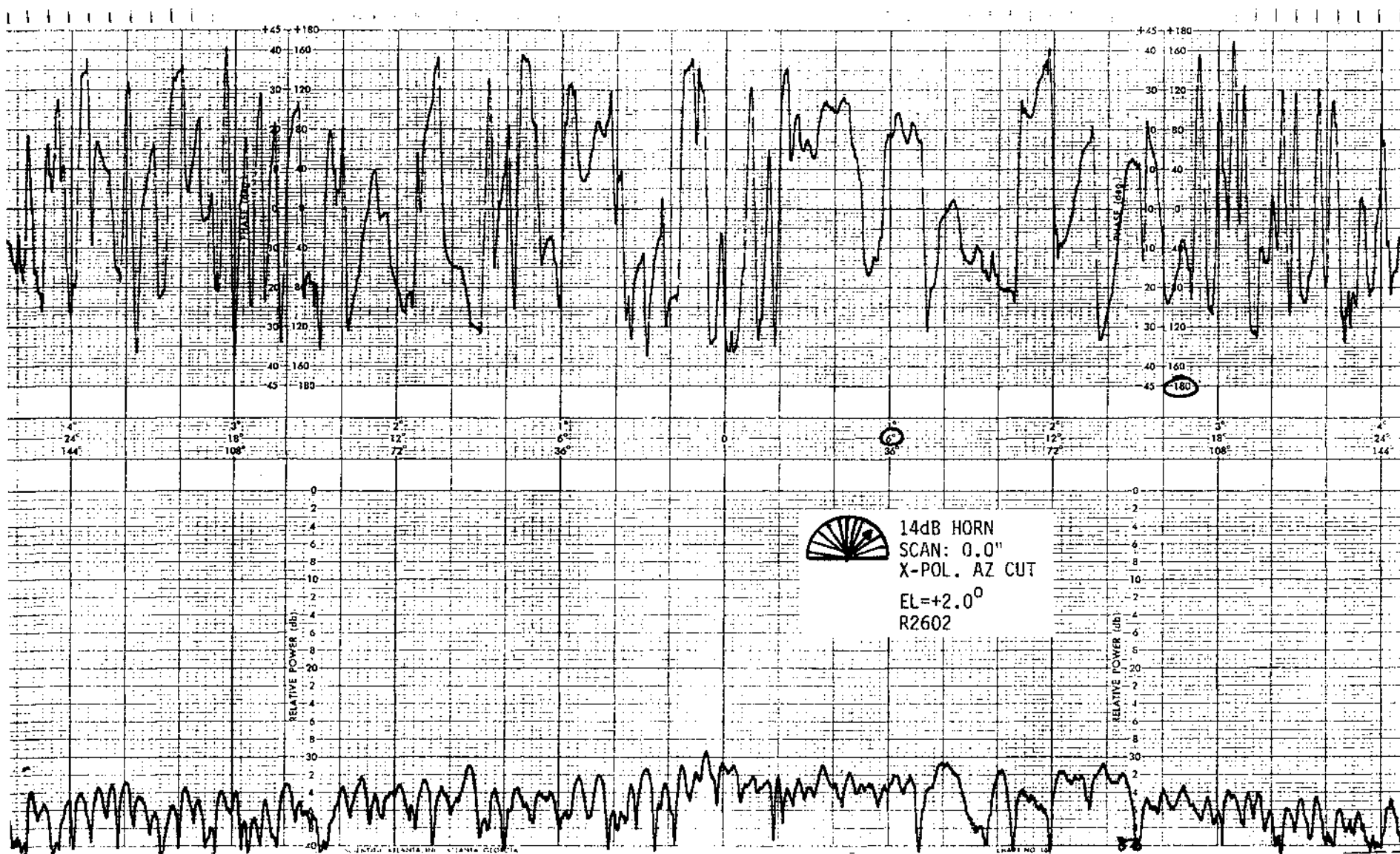




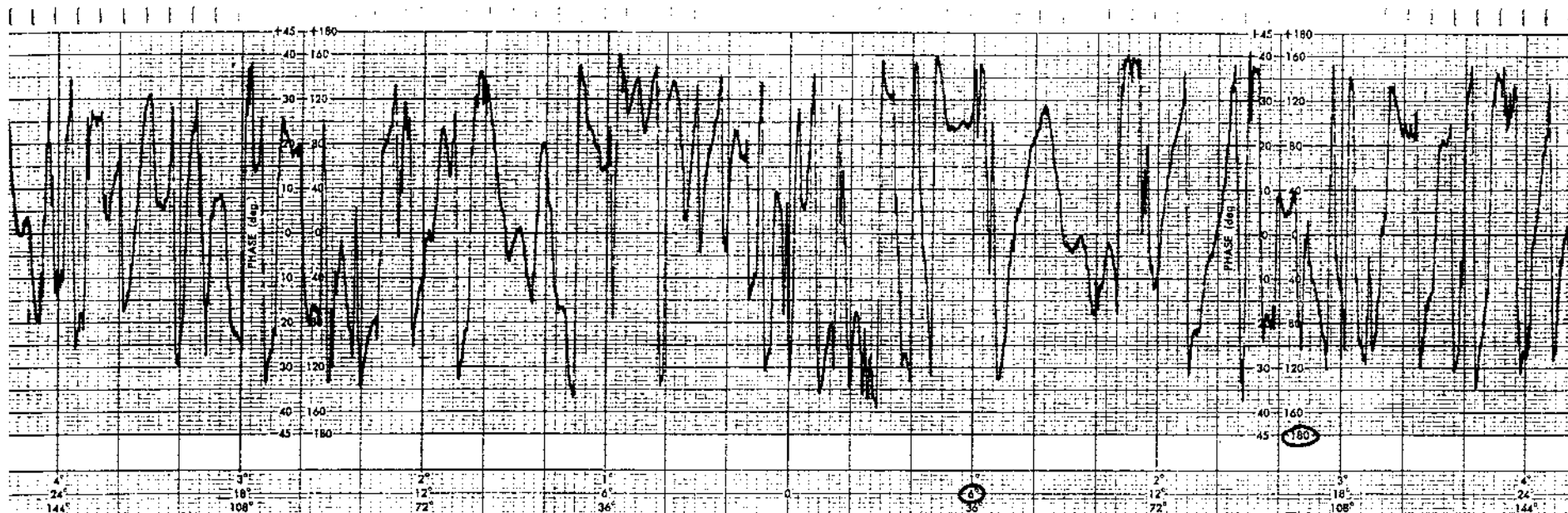




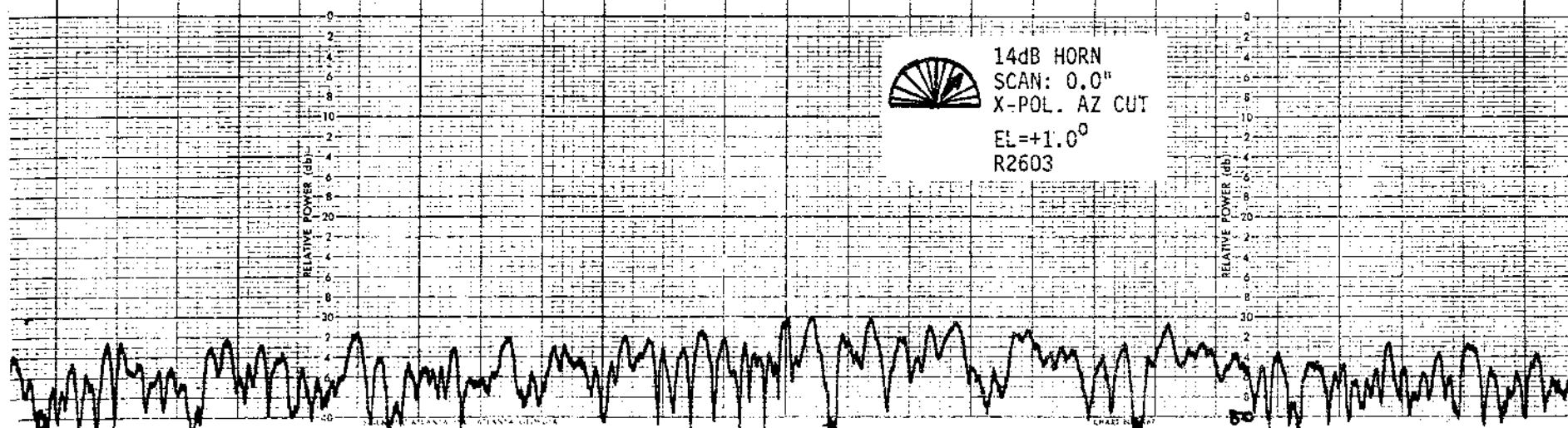


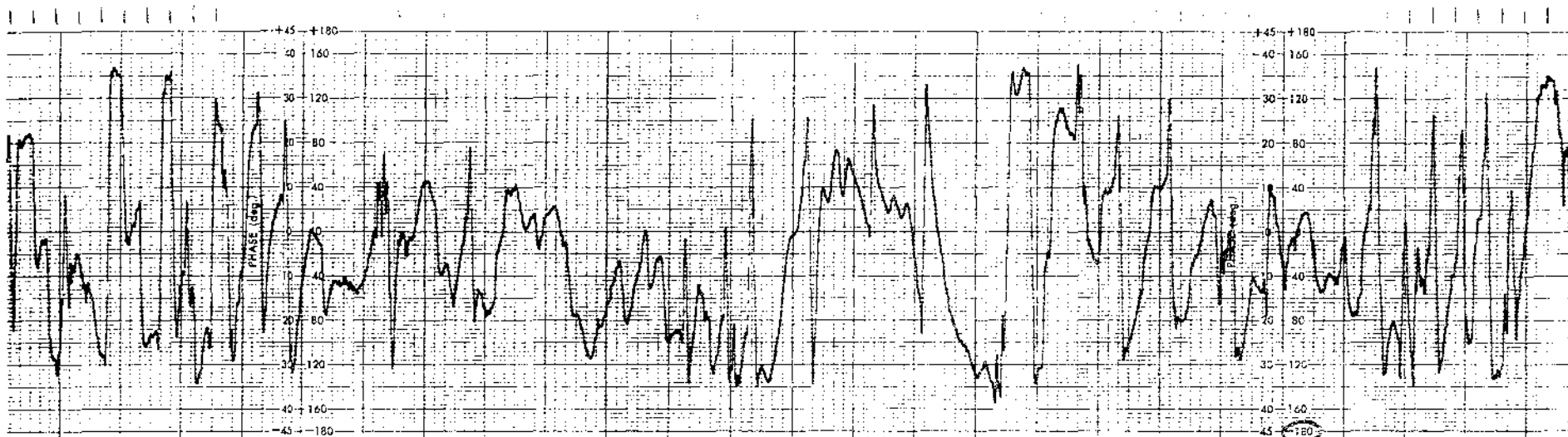




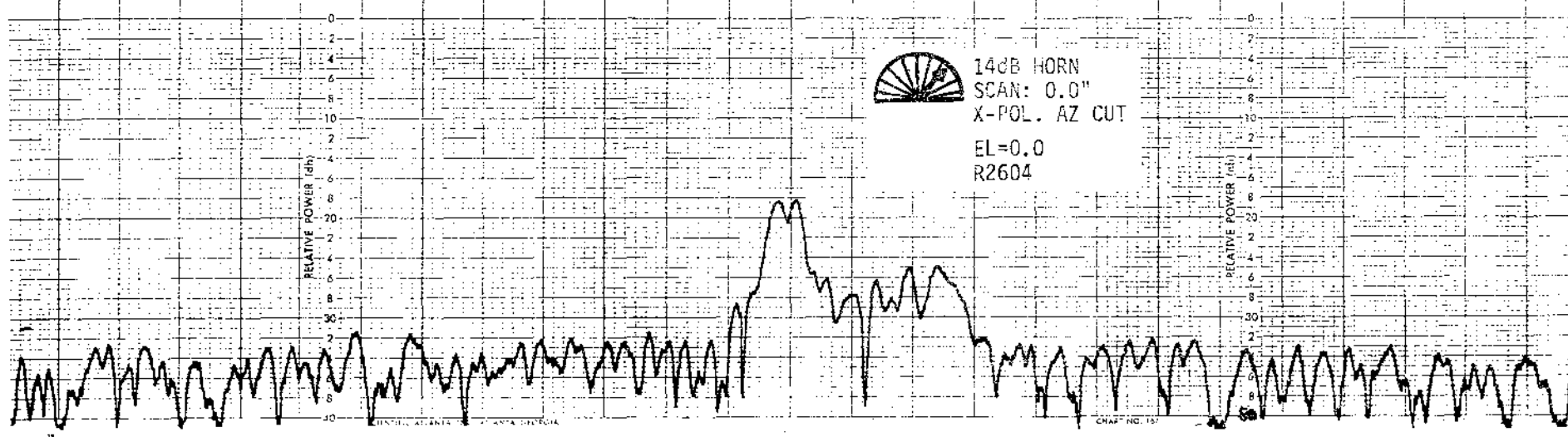


14dB HORN  
SCAN: 0.0°  
X-POL. AZ CUT  
EL=+1.0°  
R2603

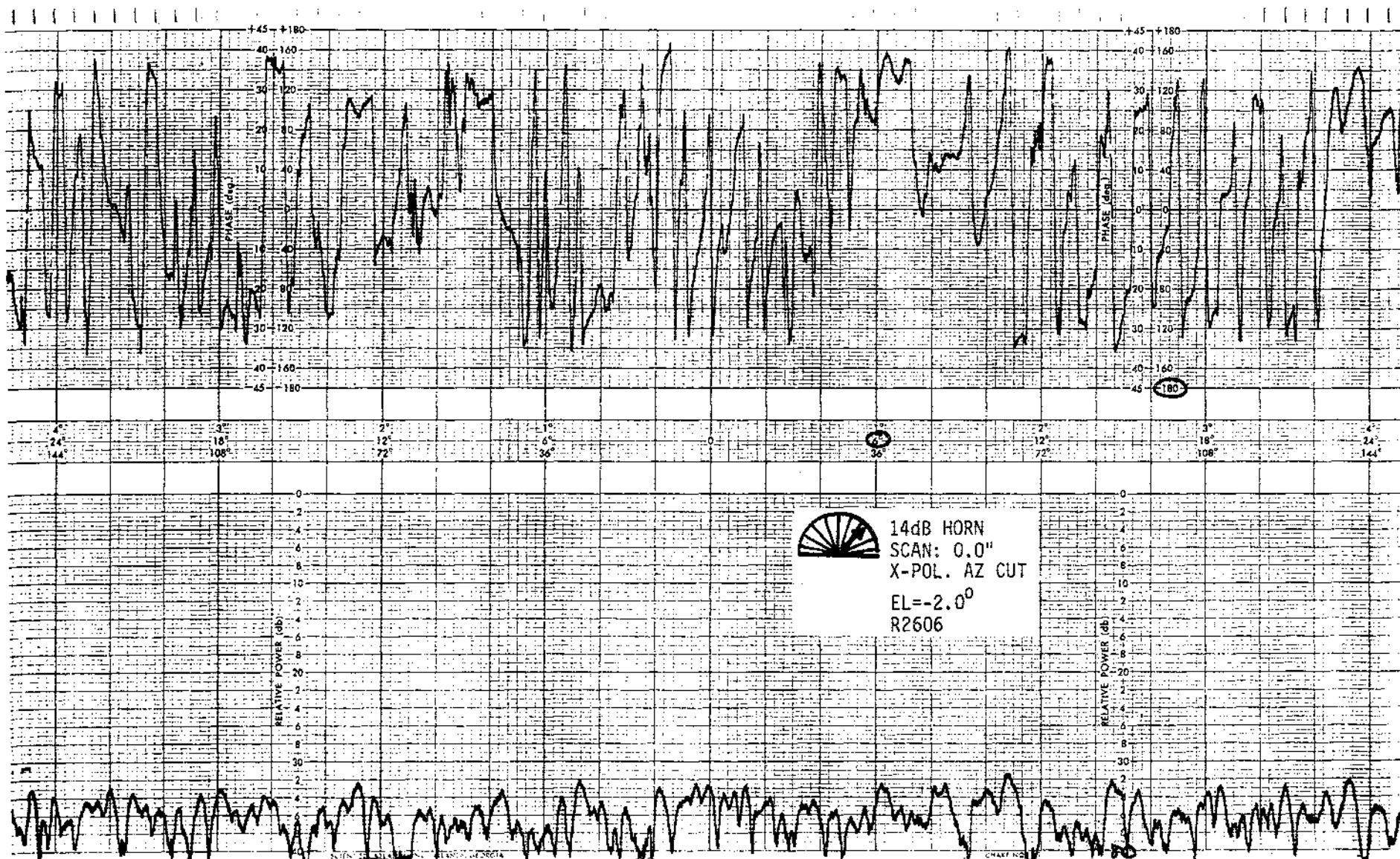


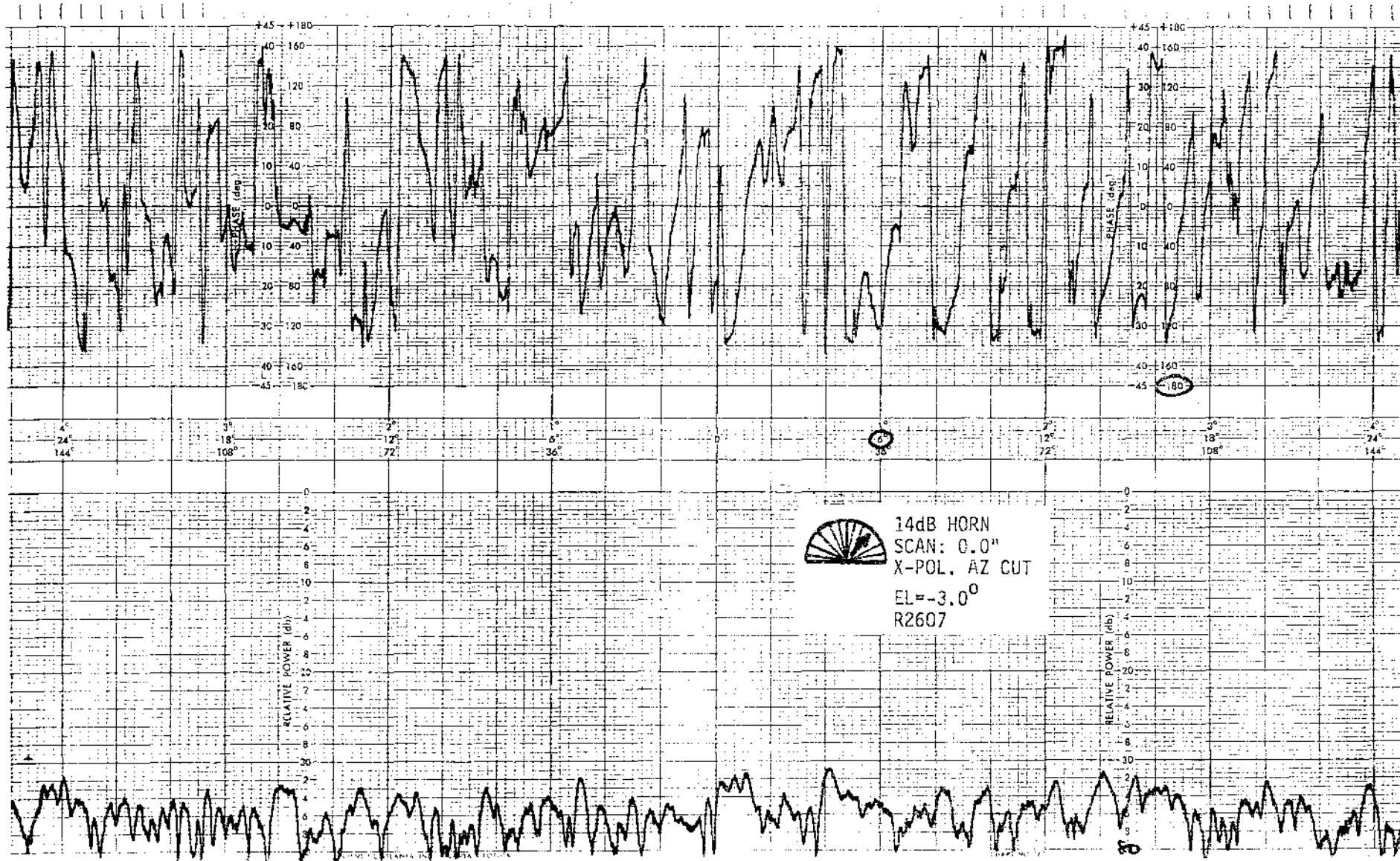


4° 3° 2° 1° 0° 1° 2° 3° 4°  
 -24° 18° 12° 6° 0° 6° 12° 18° 24°  
 144° 108° 72° 36° 0° 36° 72° 108° 144°




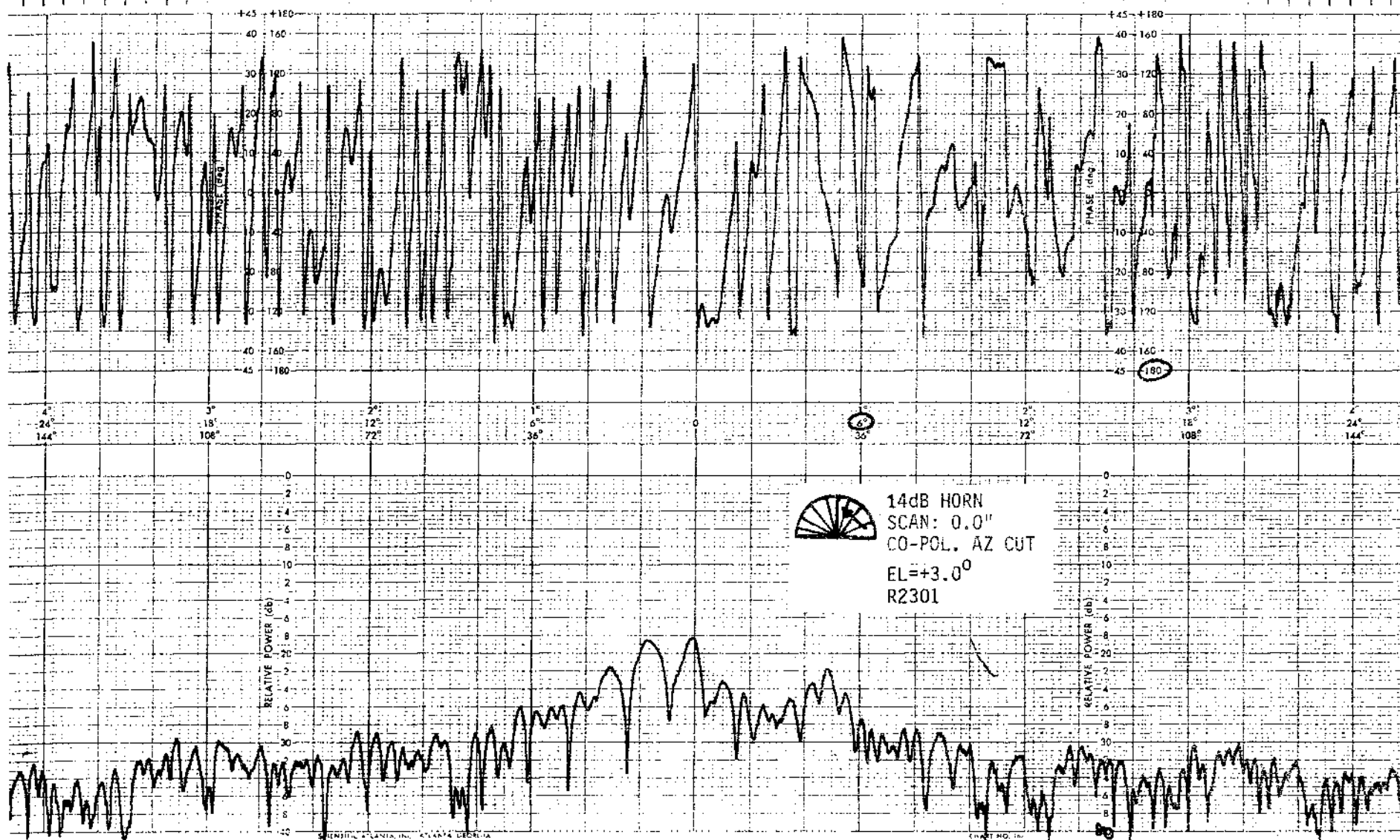




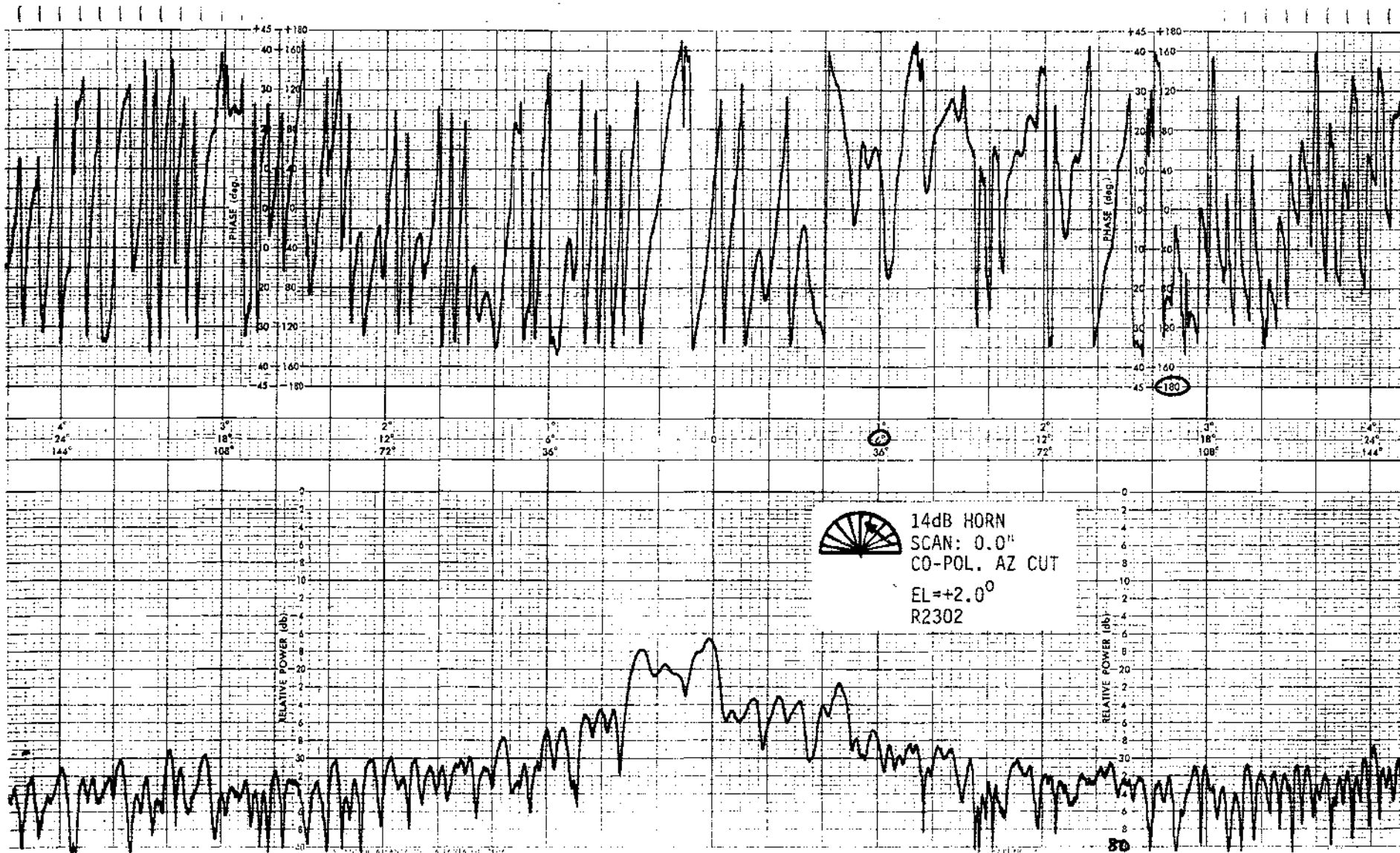


LSST - XSECONDARY PATTERN LOG

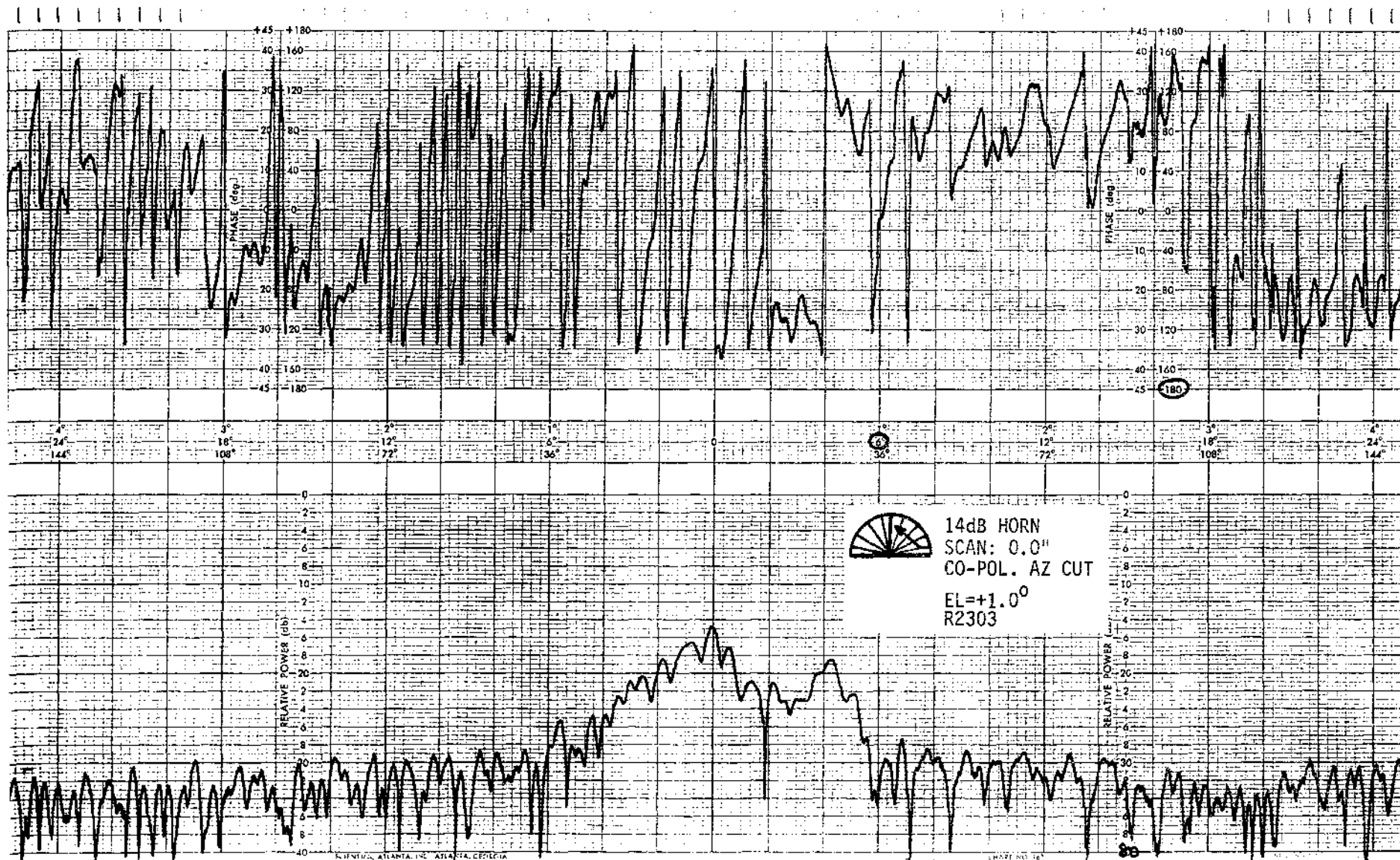
<u>CONFIGURATION</u>	<u>HORN</u>	<u>SCAN</u>	<u>POL.</u>	<u>PK. GAIN</u>	<u>PATTERN</u>	<u>FILE NAME</u>	<u>PAGE NUMBER</u>
	14 dB	0.0"	CO	-	+3°EL + 45°AZ	R2301	308
	"	"	"	-	+2°EL "	R2302	309
	"	"	"	-	+1°EL "	R2303	310
	"	"	"	50.50	0°EL "	R2304	311
	"	"	"	-	-1°EL "	R2305	312
	"	"	"	-	-2°EL "	R2306	313
	"	"	"	-	-3°EL "	R2307	314
	14 dB	0.0"	X	-	+3°EL "	R2401	315
	"	"	"	-	+2°EL "	R2402	316
	"	"	"	-	+1°EL "	R2403	317
	"	"	"	-	0°EL "	R2404	318
	"	"	"	-	-1°EL "	R2405	319
	"	"	"	-	-2°EL "	R2406	320
	"	"	"	-	-3°EL "	R2407	321

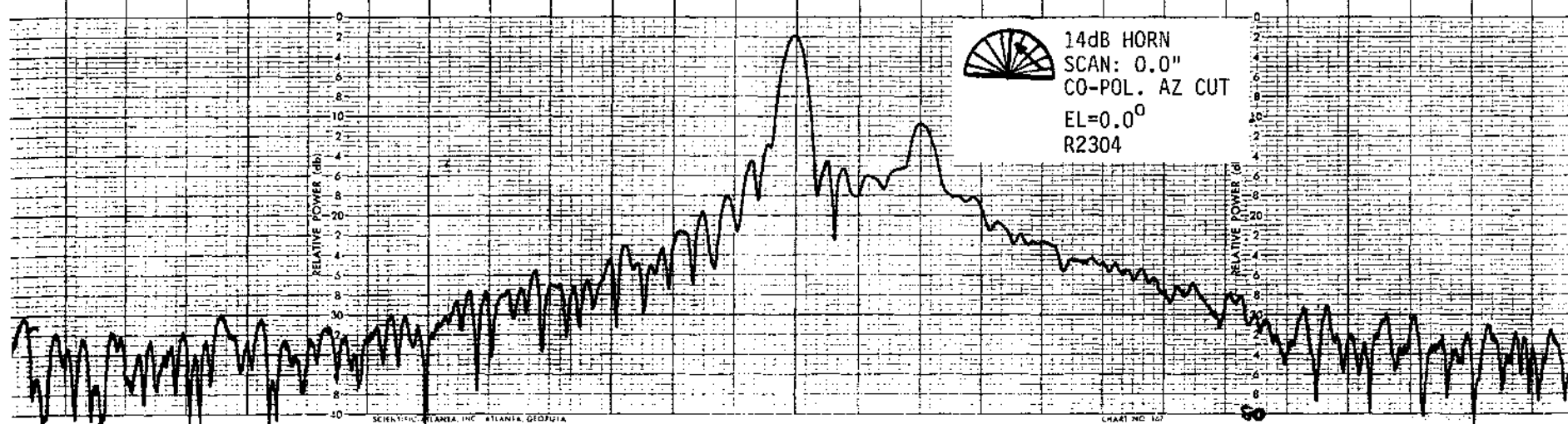
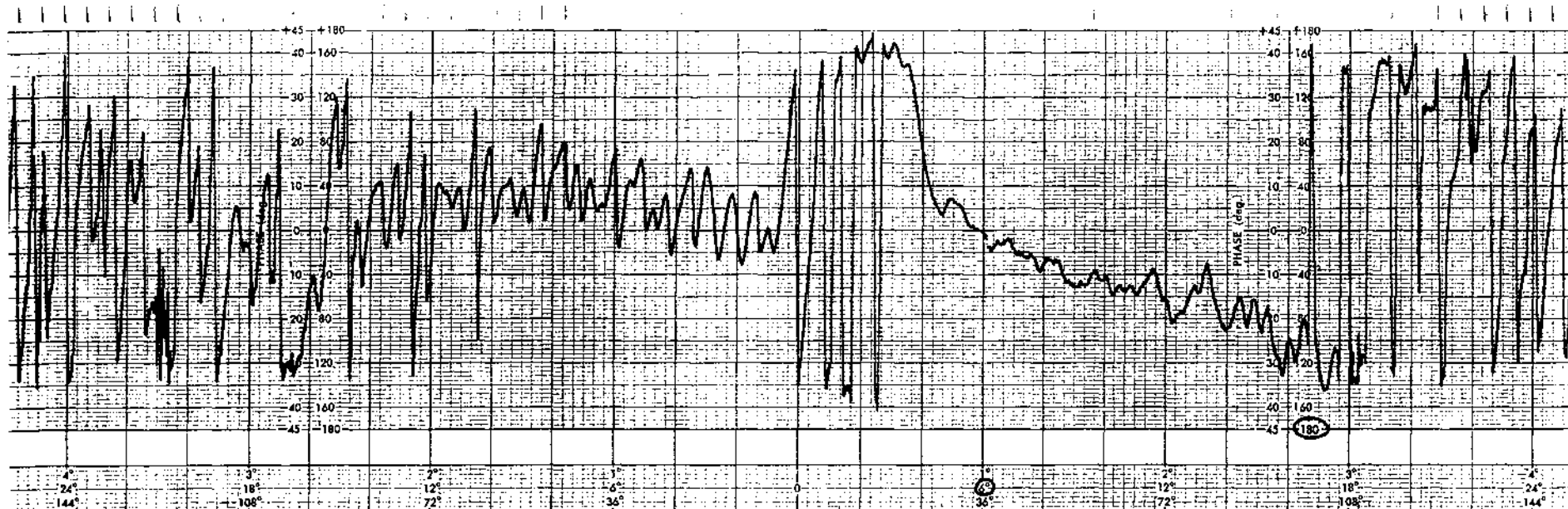


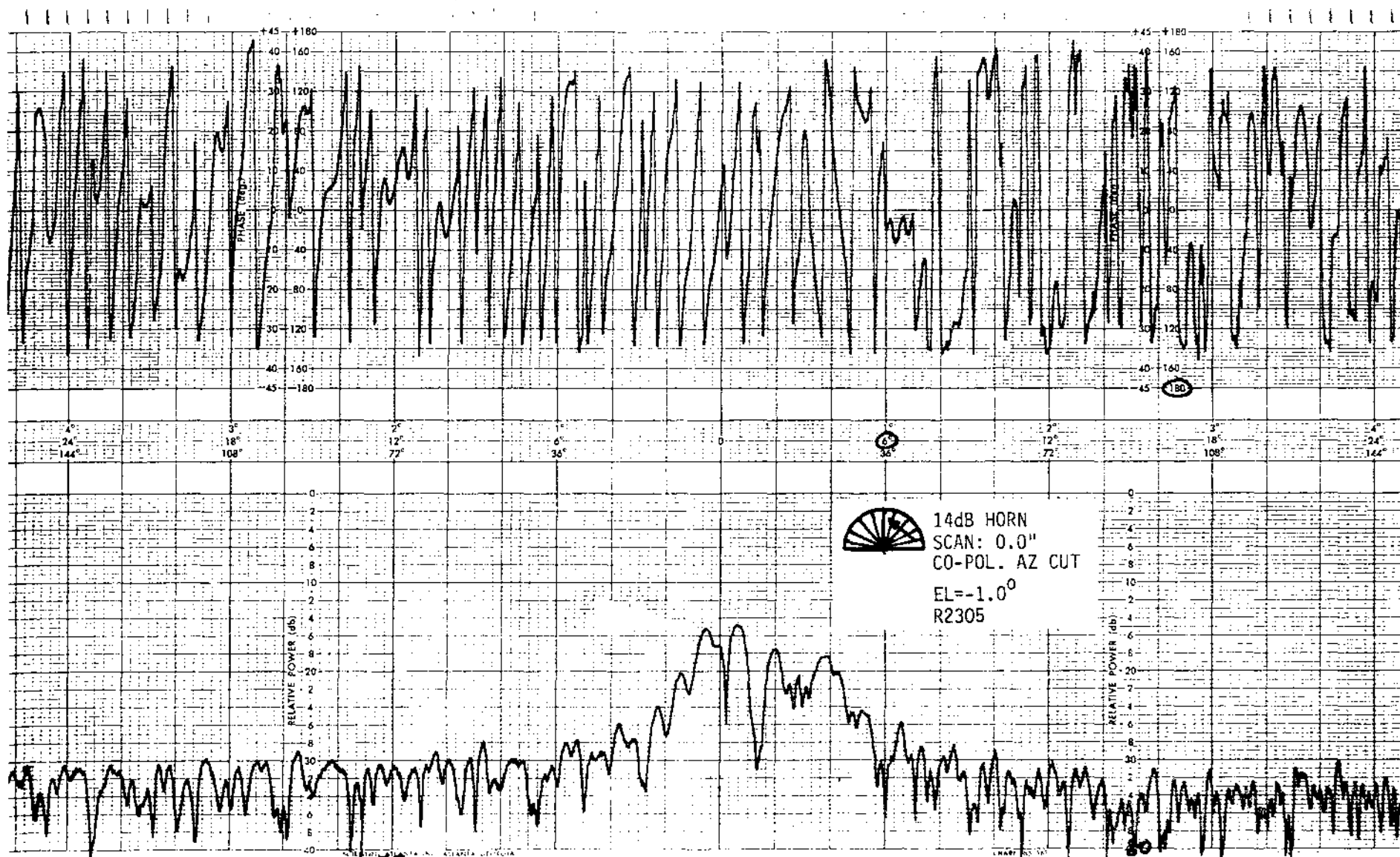


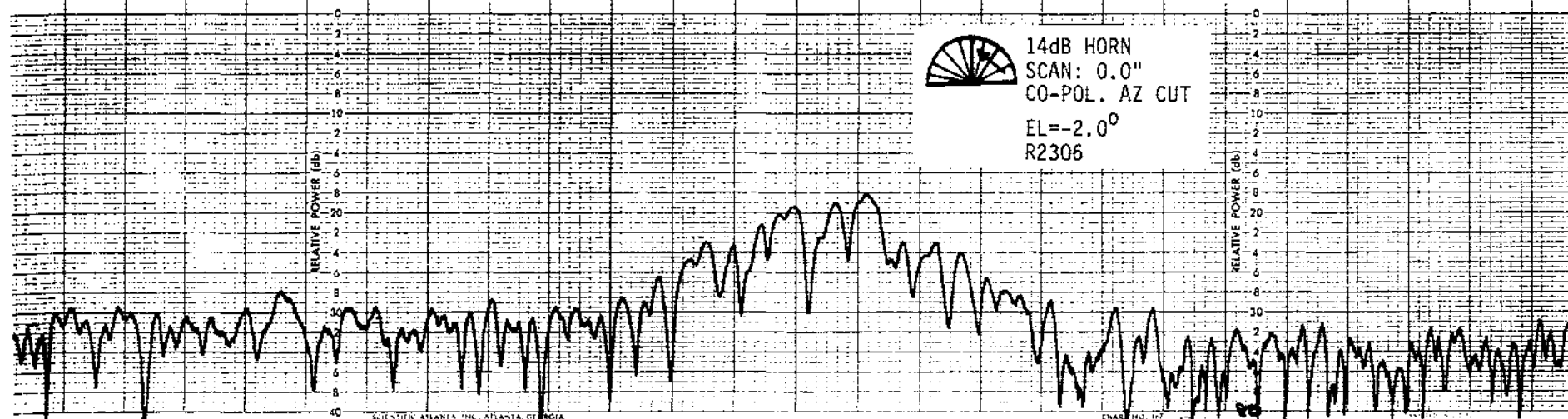
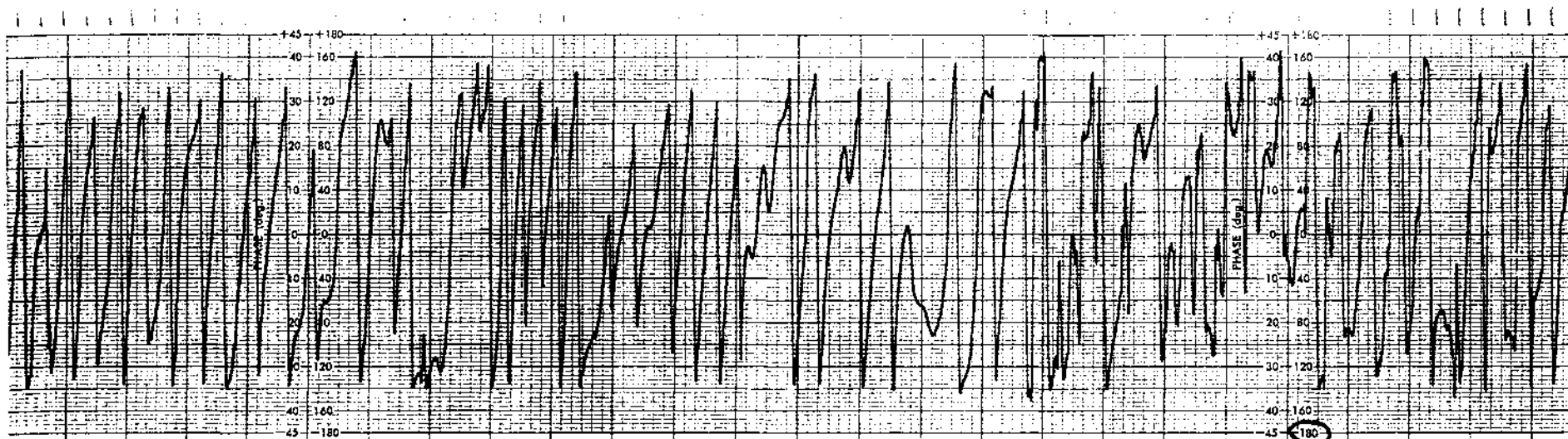








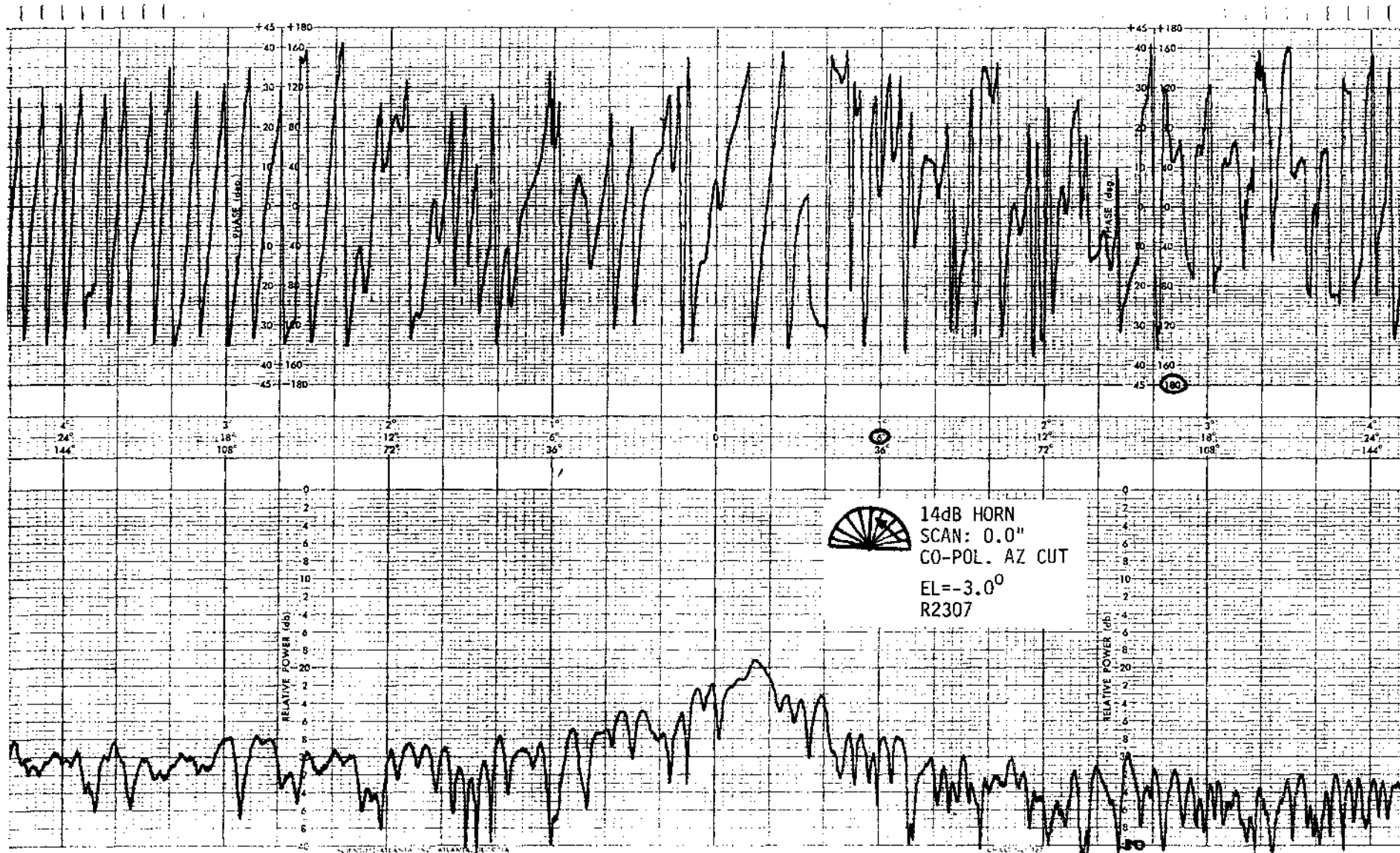


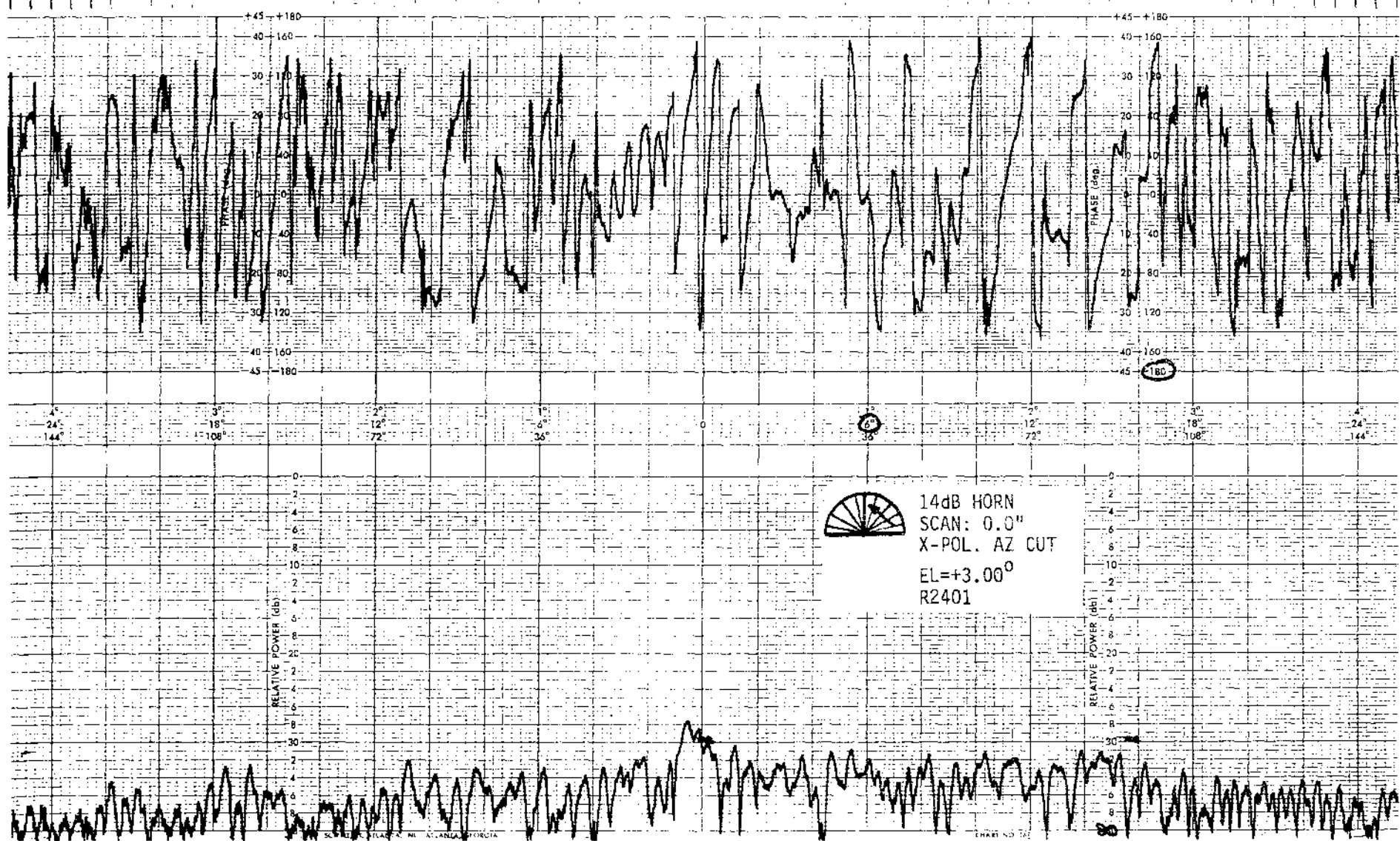


14dB HORN  
SCAN: 0.0"  
CO-POL. AZ CUT  
EL=-2.0°  
R2306

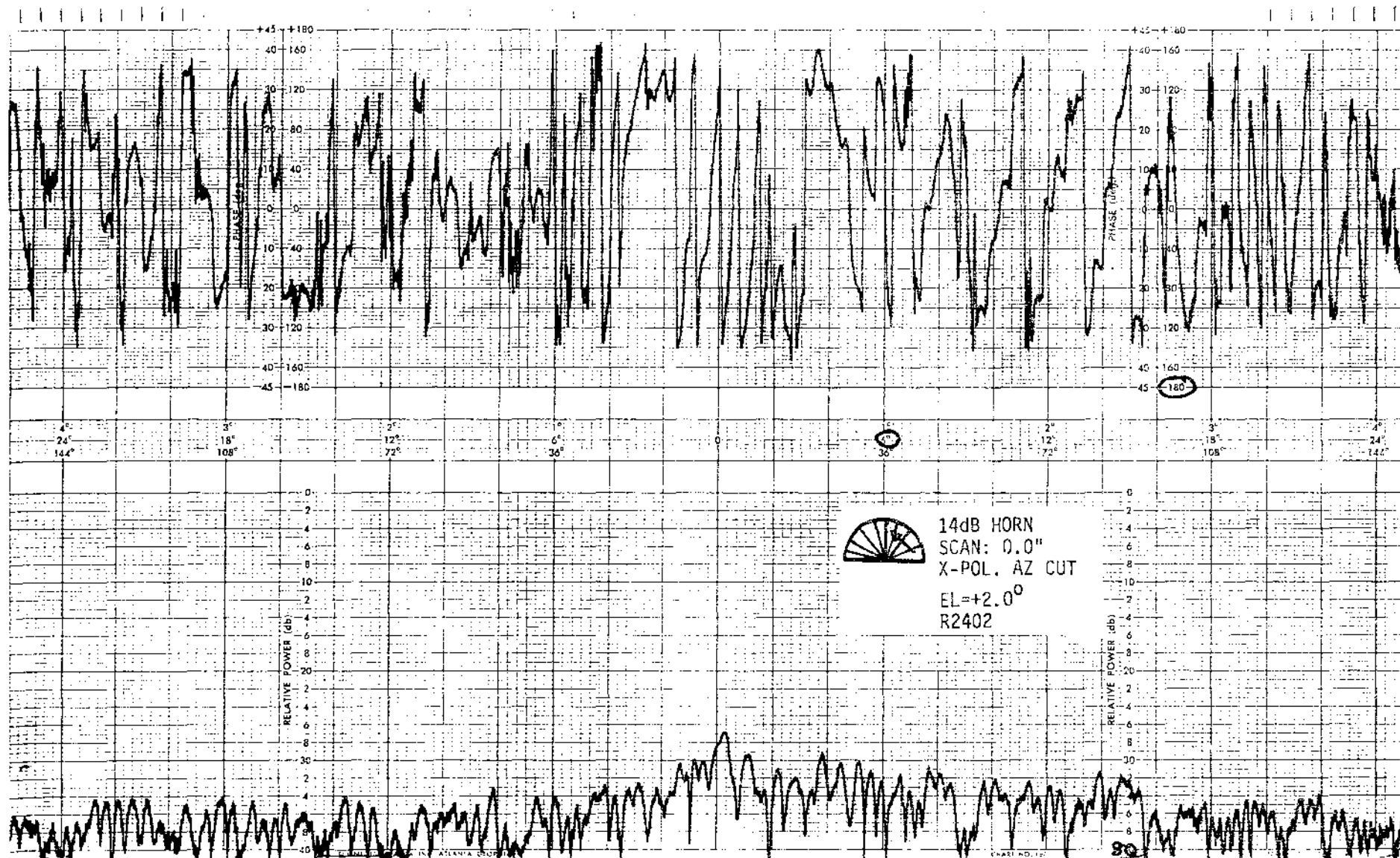
SCIENTIFIC ATLANTA, INC., ATLANTA, GEORGIA

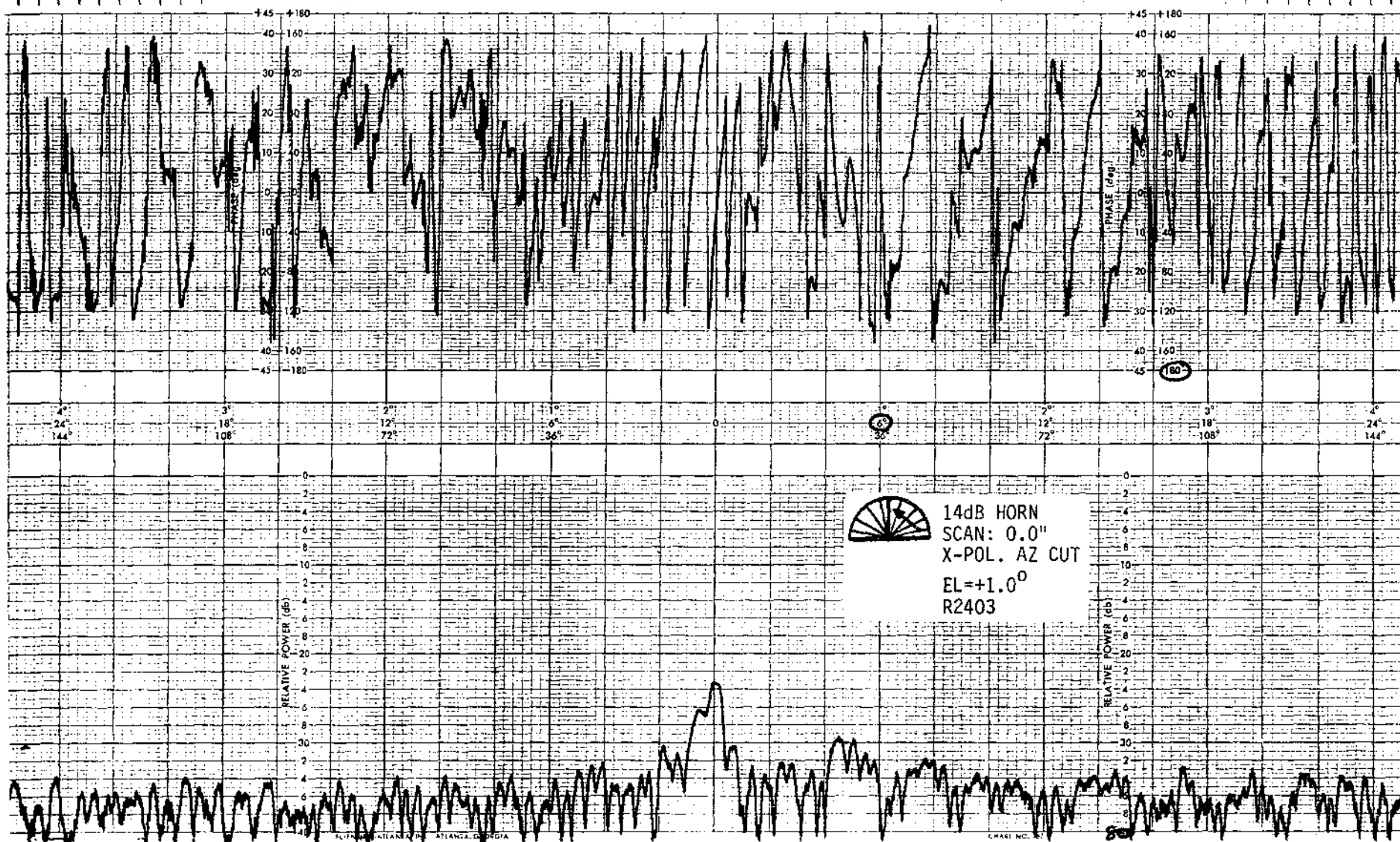
CHART NO. 167



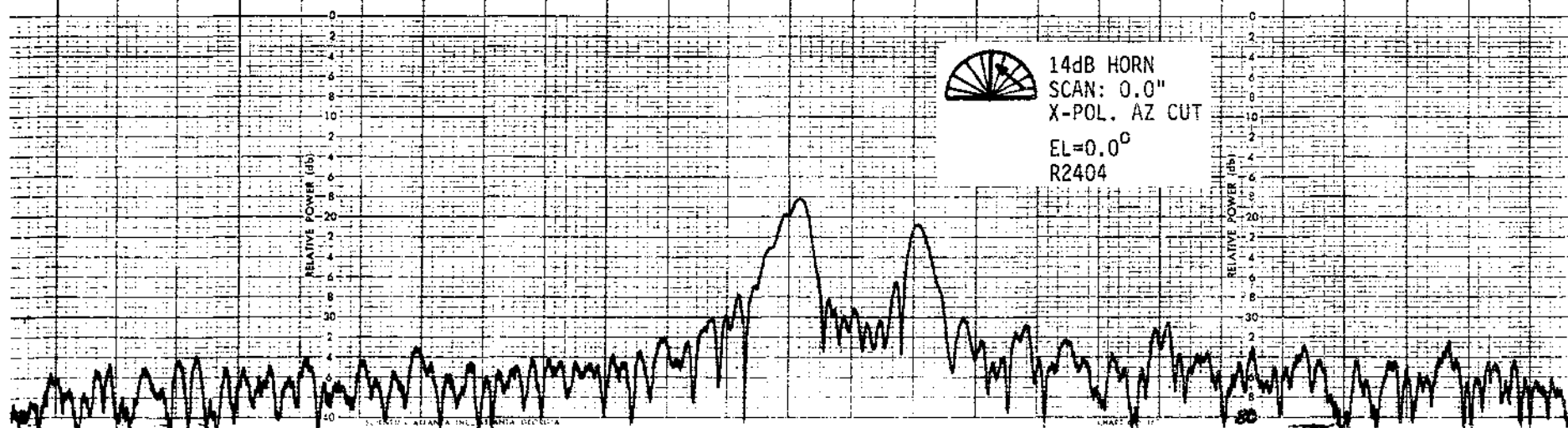
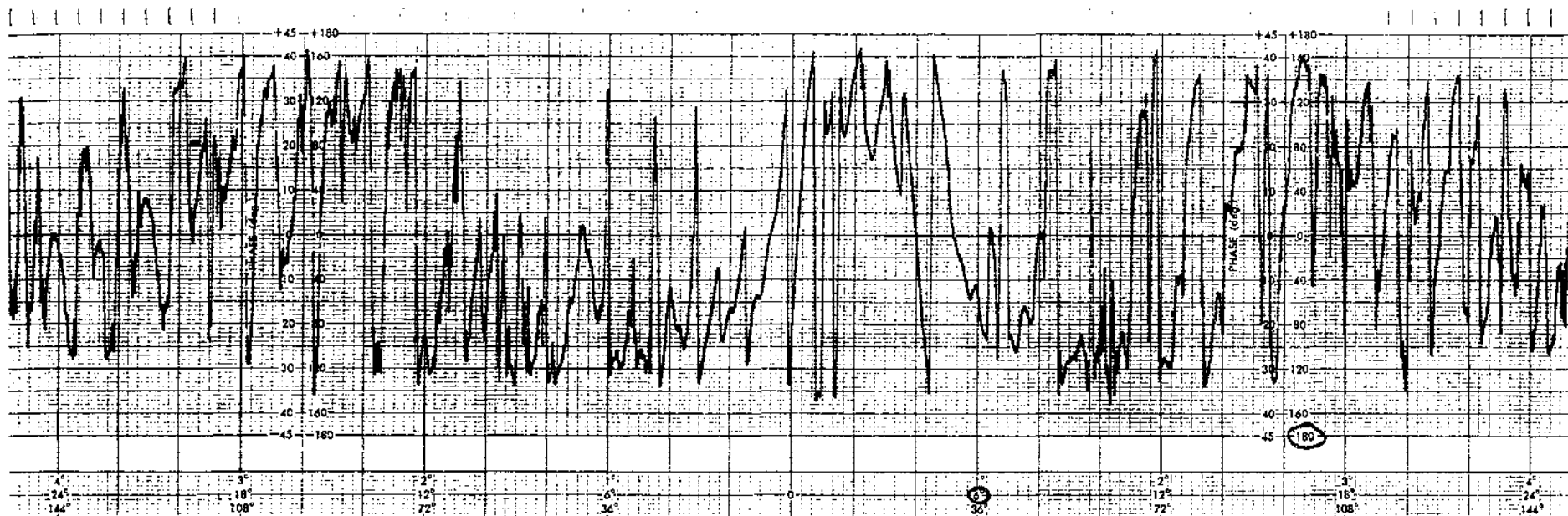


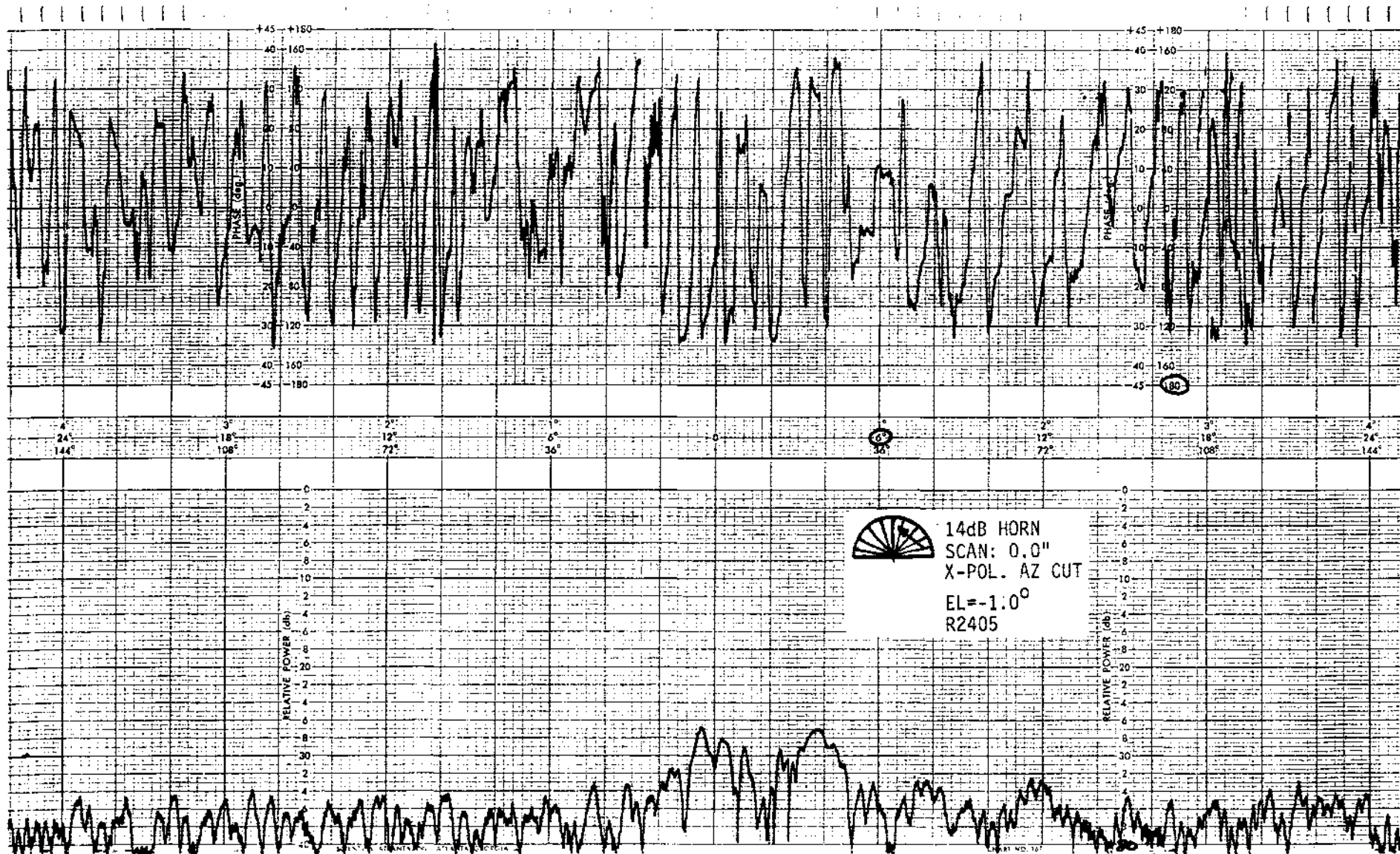


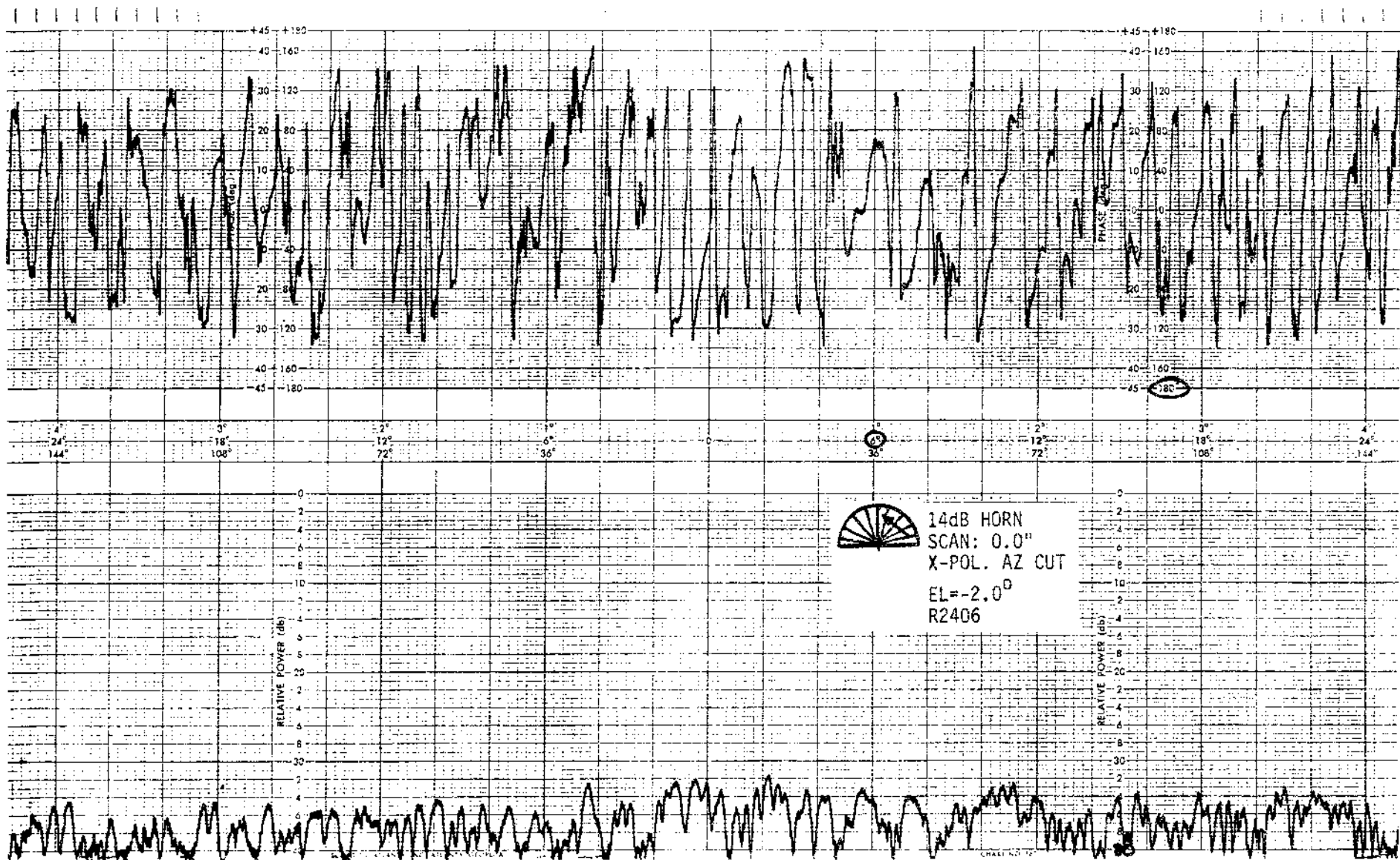


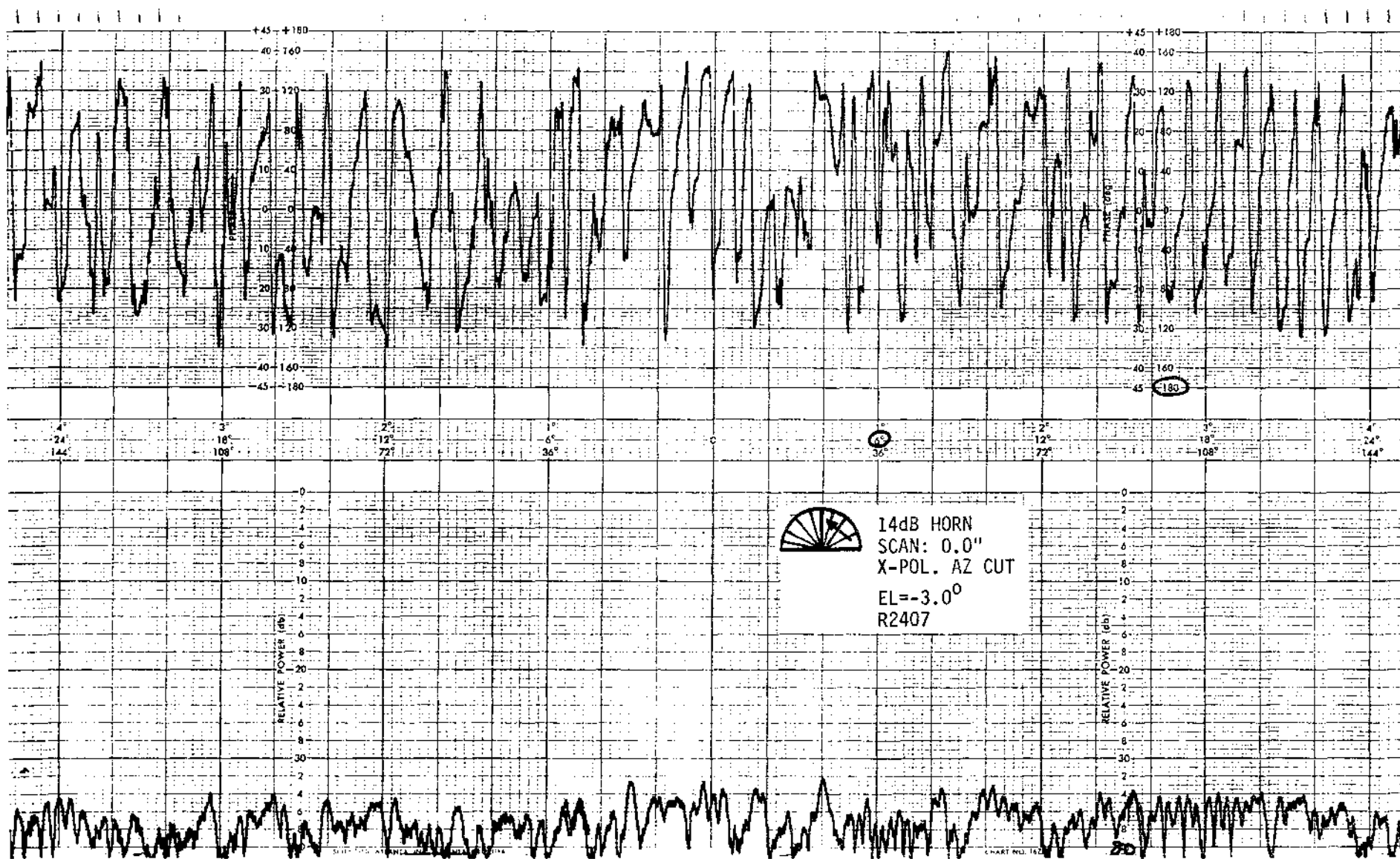












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16. Abstract  As part of the Large Space System Technology Program, this report, in two volumes, presents the theoretical and experimental results of the RF characteristic of a hoop/column, quad aperture antenna using an RF verification model.  To satisfy the primary purposes of the model it provides experimental pattern data for the quad aperture configuration at different reflector edge illumination levels, from which the geometry and edge effects can be assessed, and provides experimental data which can be compared with calculations using various theoretical reflector scattering formulae. It also experimentally determines the effects upon secondary patterns of scale model quartz cables, as used in the hoop/column design, upon secondary patterns in order to assess the importance of developing a scattering theory to predict such effects. In addition, this report contains a comprehensive theoretical study and the experimental pattern results of quad aperture antenna feeds, a discussion of the fundamental affect of parasitic side lobes, their amplitude, and location in space.					
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